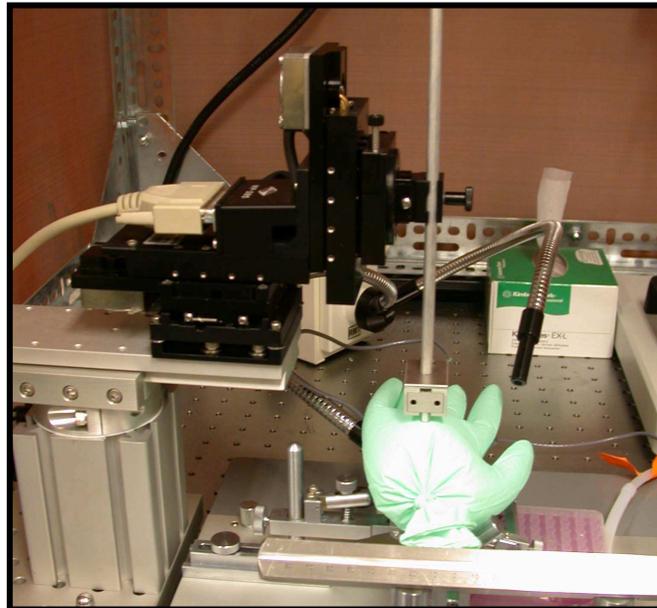


Penetration Mechanics and Mechanical Properties of Mouse Brain Tissue



CMM Brain Neuromechanics Workshop
Field's Institute, University of Toronto
July 26-28, 2010



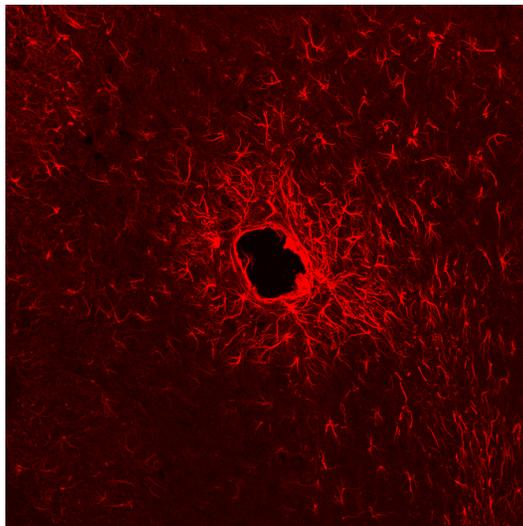
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Motivation:

- Insertion of foreign objects into the brain gives rise to neuronal necrosis and apoptosis, inflammatory processes and gliosis

Goal:

- Design more biocompatible implants and implantation processes to minimize deleterious tissue responses



Astrocytosis caused by
implantation of silicon in OB
after 1 month.

Sharp et al. (2006) J. Neural Eng.

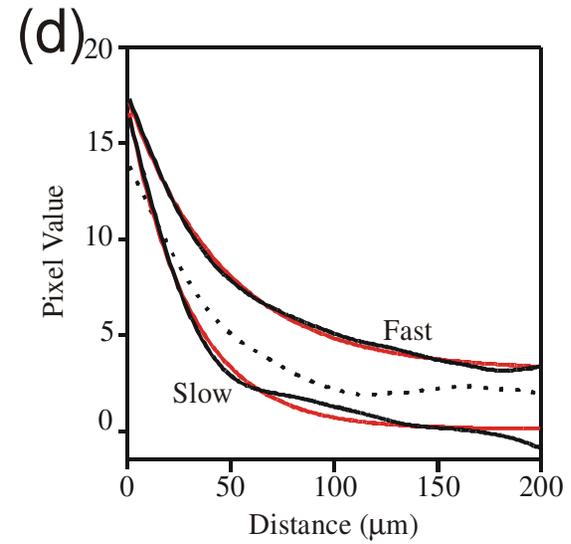
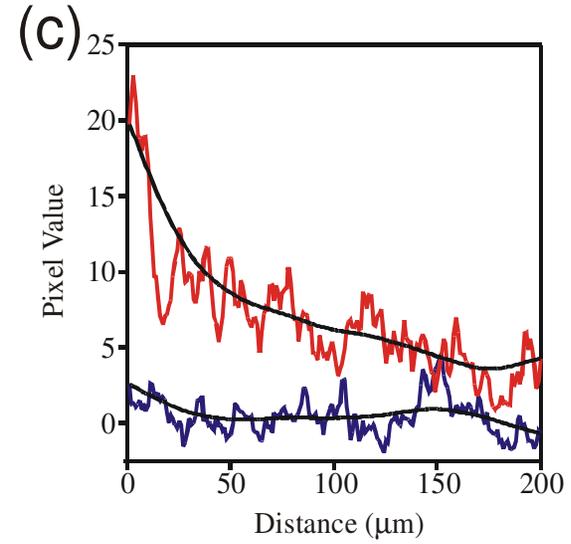
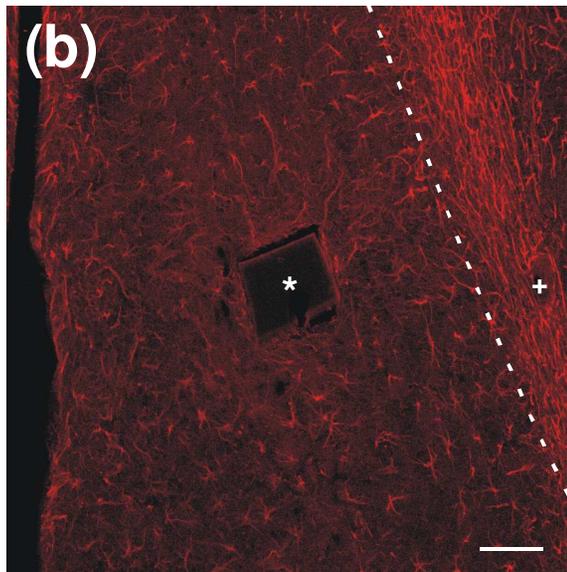
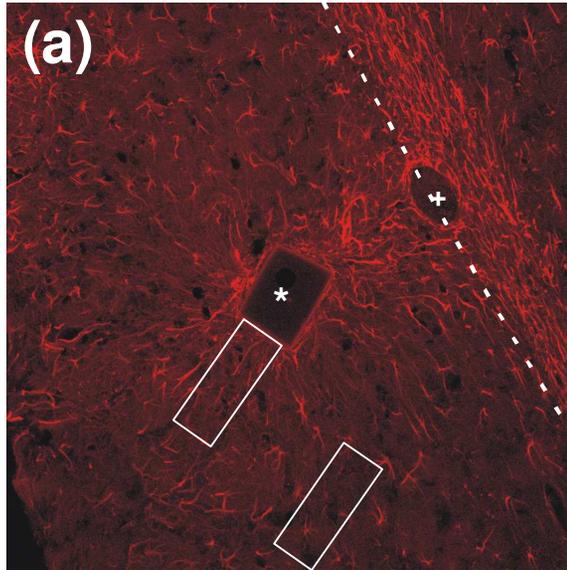


Things known to affect biocompatibility of implant:

- size
- shape
- material
- compliance
- shear from tether
- rate of insertion



Insertion Rate affects Biocompatibility

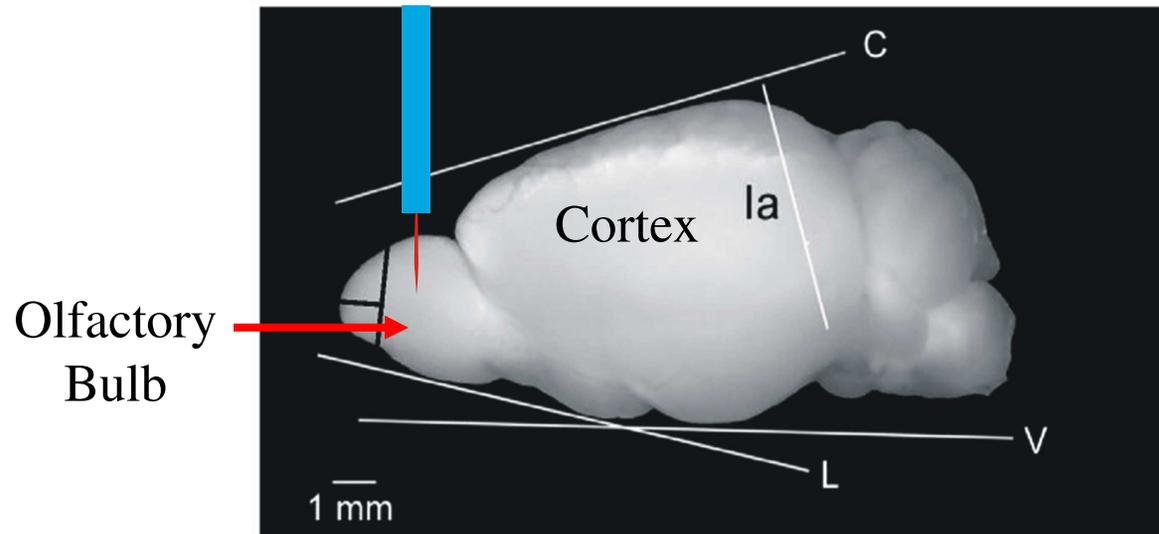


Sharp et al. (2006) J. Neural Eng.

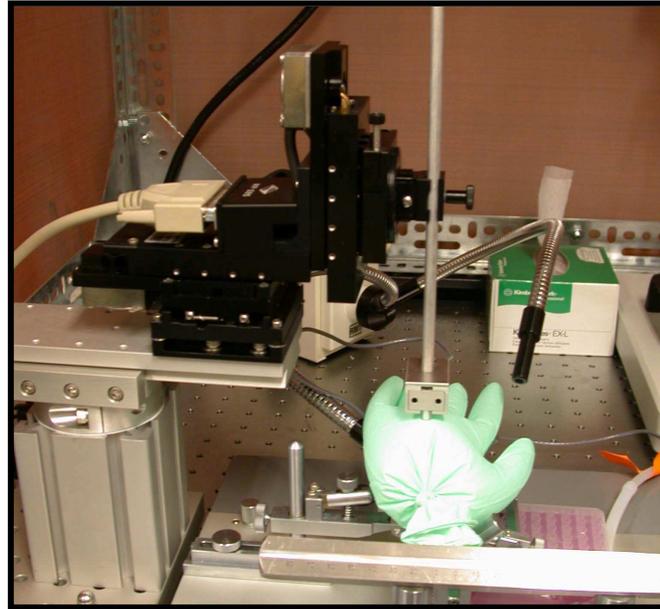


Objective: Use compliant materials (polymers?) to engineer more “compatible/effective” implants.

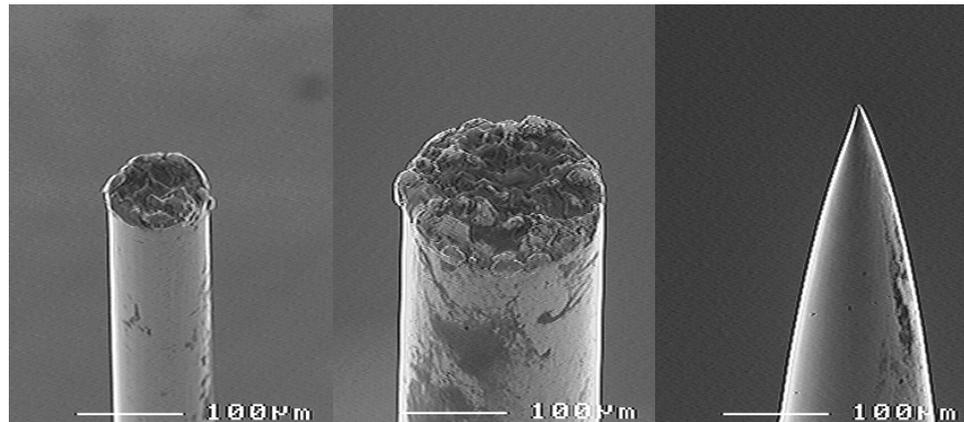
Design Issue: How stiff does the implant need to be or how much force does it need to withstand during insertion?



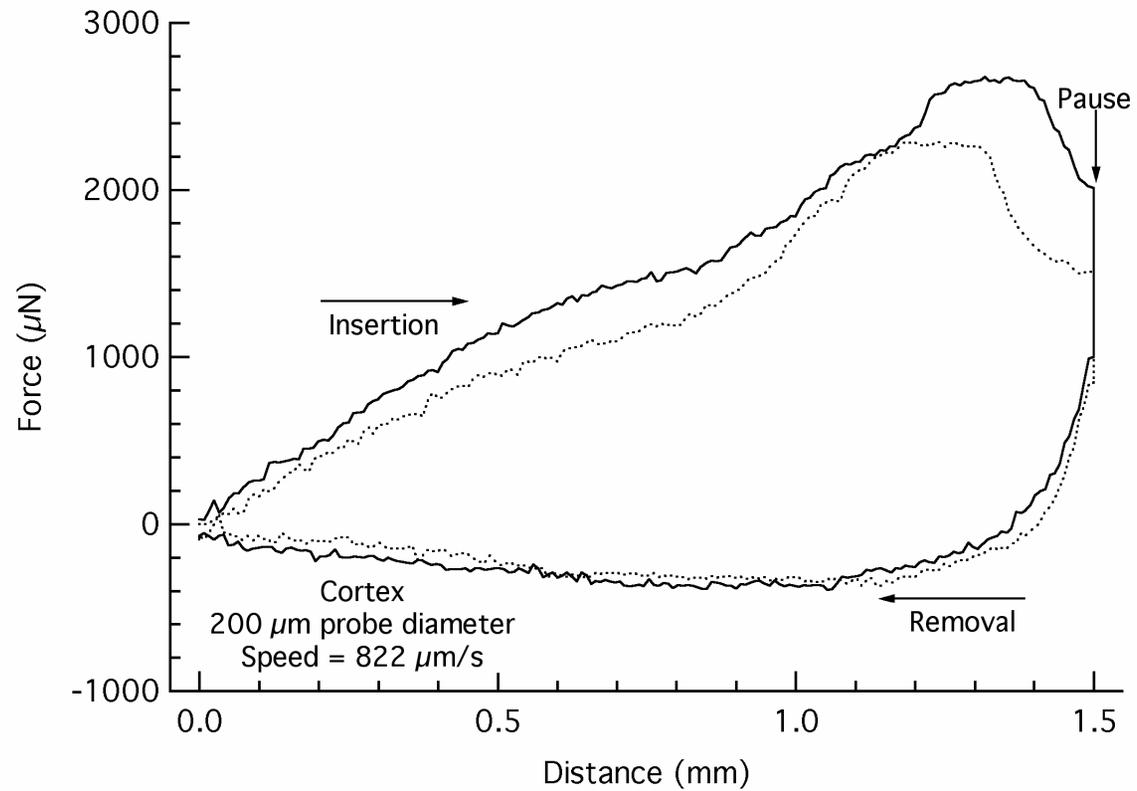
Measure Force during Controlled Insertion



Sharp et al. (2009) IEEE
Trans. Biomed. Eng.



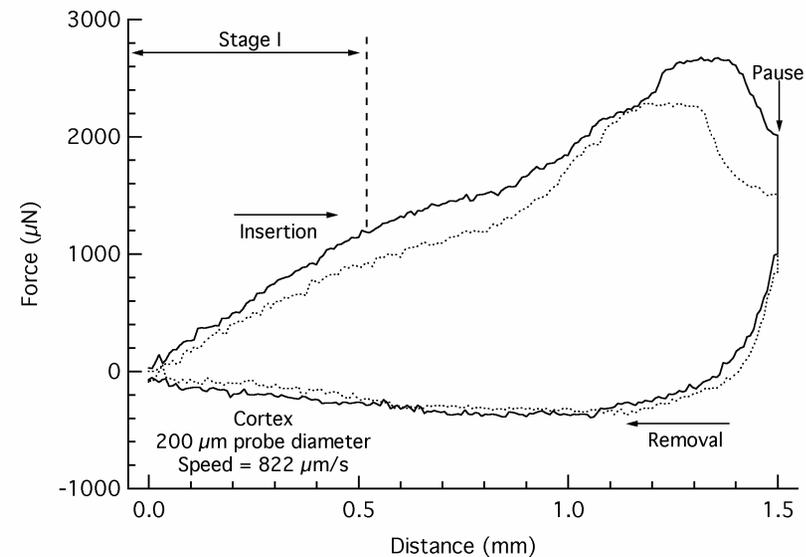
Forces during Probe Insertion and Removal



Young's Modulus of Tissue

$$E = \frac{\Delta F(1 - \nu^2)}{\Delta u 2a} = \frac{K_1(1 - \nu^2)}{d}$$

where E = Young's Modulus
 K_1 = slope
 F = applied force
 ν = Poisson's ratio = 0.5
 a = radius of punch
 d = diameter of punch
 u = indentation depth



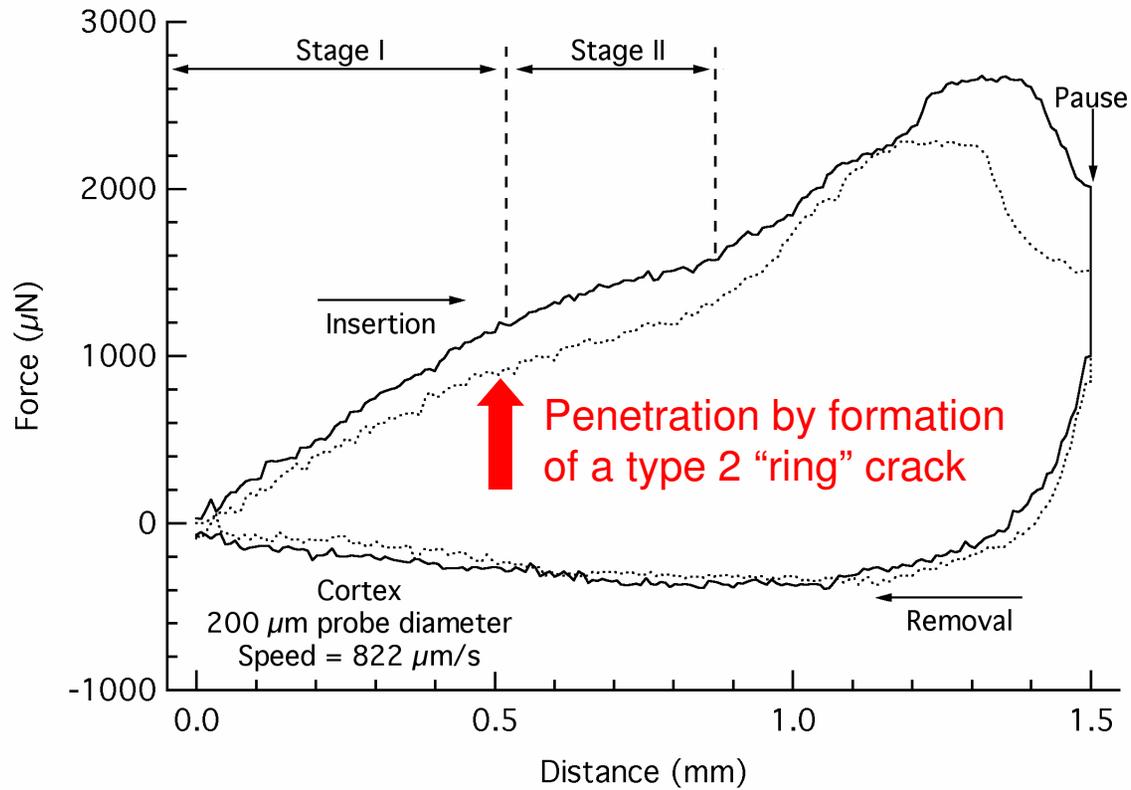
$$E = 7.4 \pm 0.7 \text{ kPa}$$

Assumptions:

- 1) the brain is a linear, elastic and incompressible material (really non-linear and viscoelastic)
- 2) K_1 is linear with indentation depth



Penetration Force



$$F_{crit} = 1092.6 \pm 166.2 \mu\text{N}$$



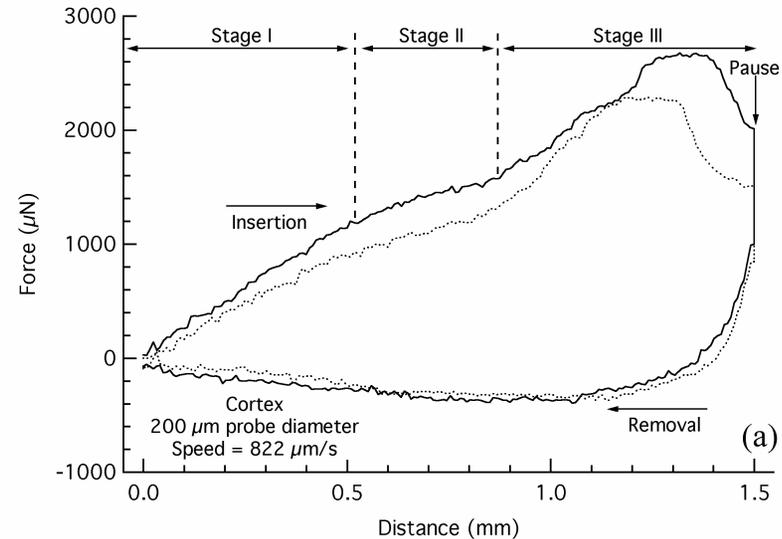
Frictional Forces

-ideally, the linear unloading path is a function of tissue modulus, probe diameter, and the coefficient of friction

-unfortunately, there are various confounds than led us to consider the rate of change in frictional forces as a whole

$$\frac{\Delta F_f}{\Delta \delta} = |K_2|$$

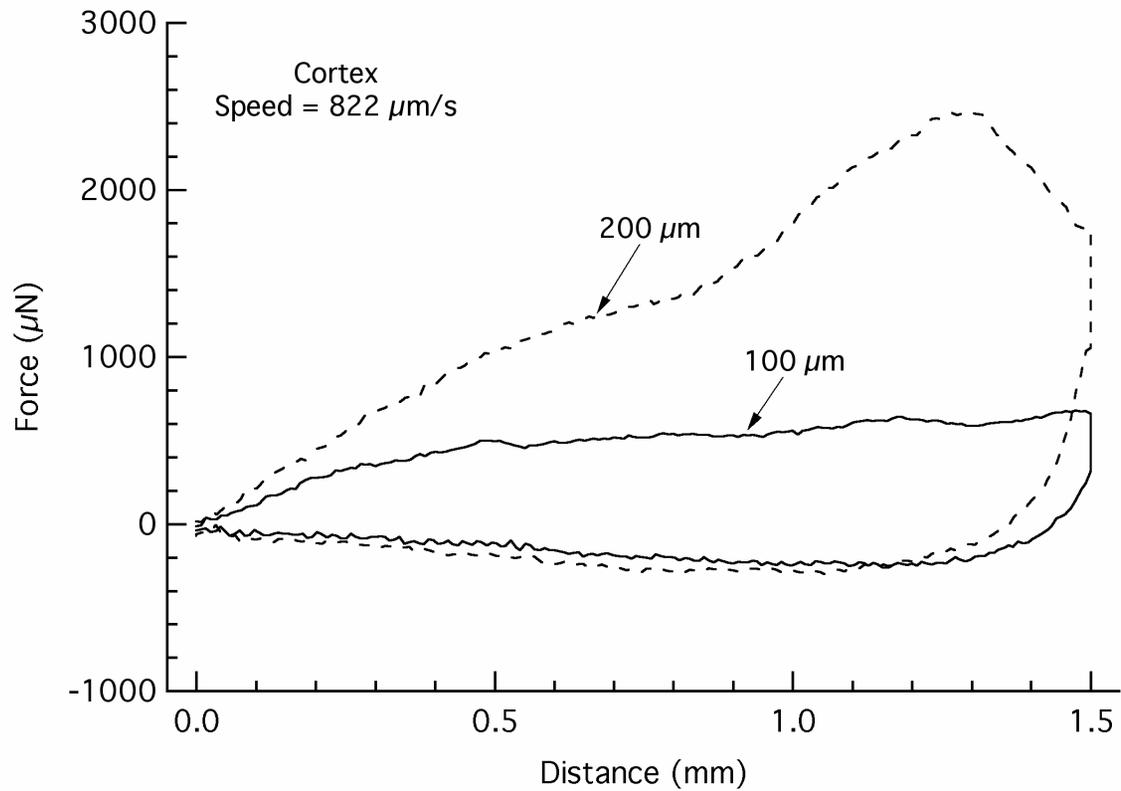
where F_f = frictional force
 δ = penetration depth
 K_2 = slope



$$\Delta F_f / \Delta \delta = 269.7 \pm 65.4 \text{ } \mu\text{N/mm}$$



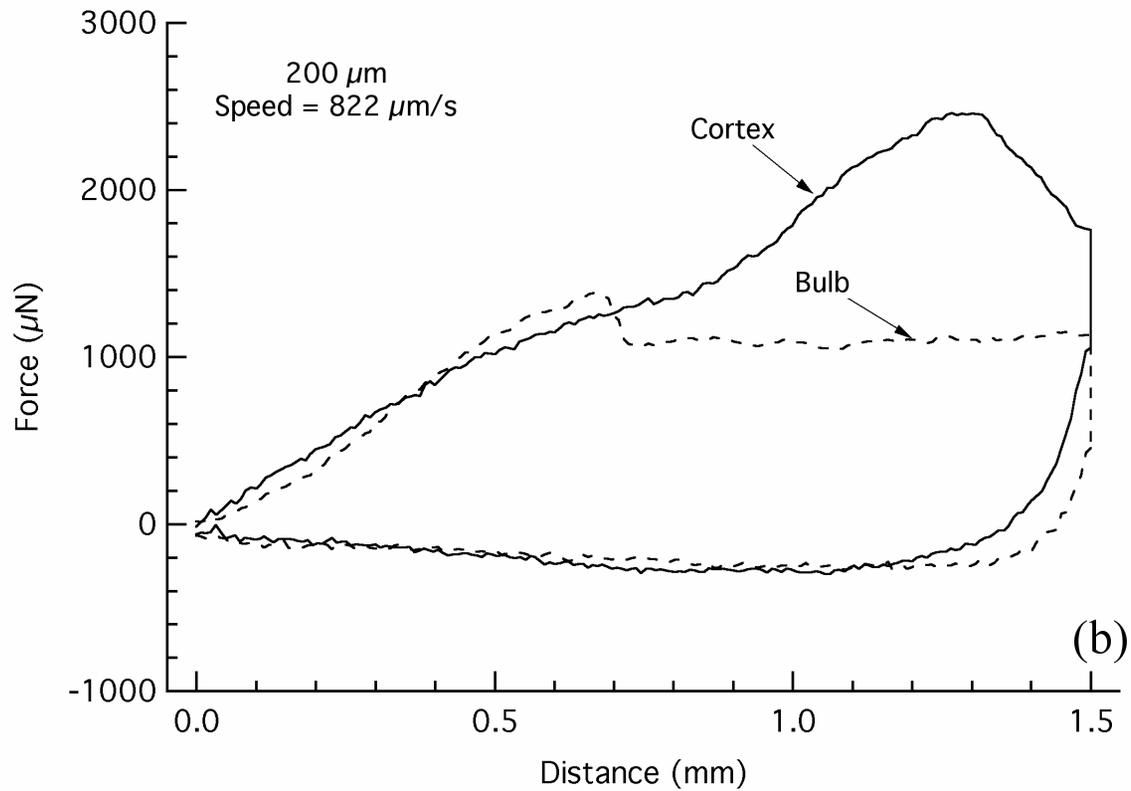
Decrease in Probe Diameter



Decrease in maximum force, load/displacement hysteresis, penetration force and frictional force.



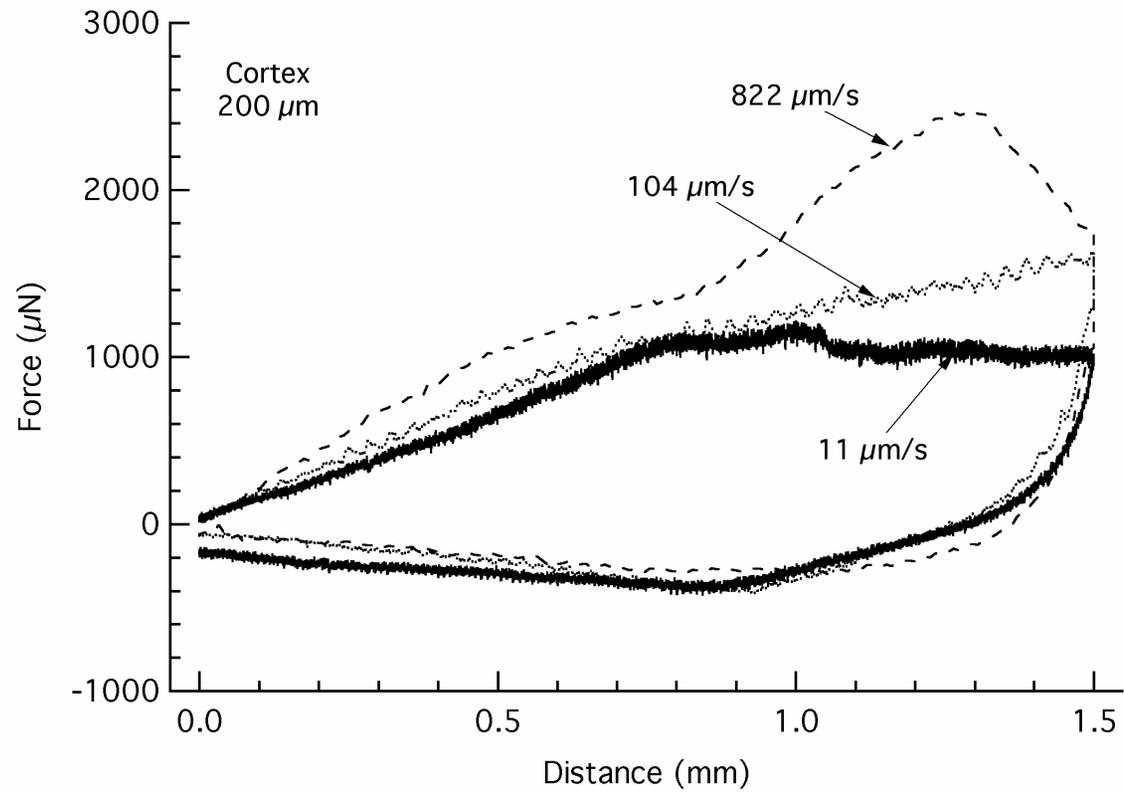
Tissue Specific Effects



Modulus was not significantly different between tissues, but frictional forces were lower in the OB.



Rate of Probe Insertion

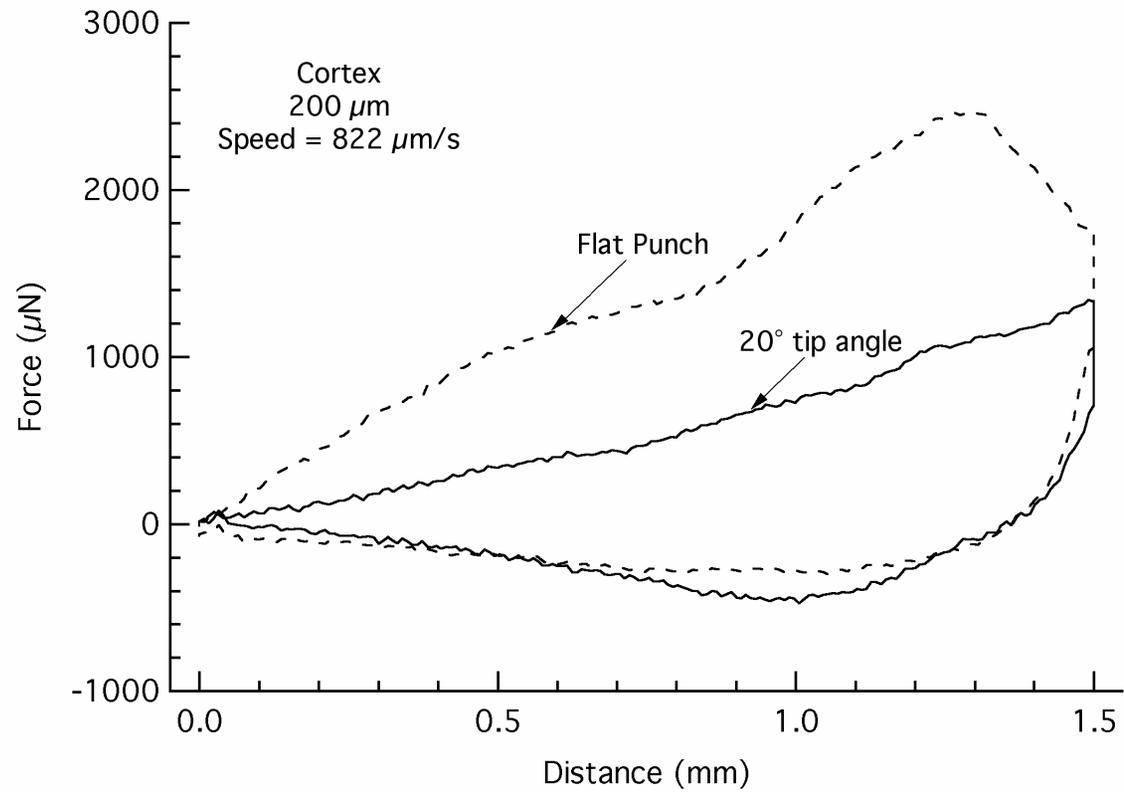


Significant Effects of decreasing the Insertion Rate

- 1) Modulus: decreased
- 2) Maximum Force: decreased
- 3) Load Displacement Hysteresis: decreased
- 4) Frictional Force: increase for slowest rate - adhesions



Sharpened (200 μm) Probe



Formation and opening of mode I crack.



Sharpened Probe:

- Decrease in maximum force
- No change in frictional forces during retraction given the same base diameter

Cutting Force:

$$\frac{\Delta F_{cut}}{\Delta \delta} = \frac{\Delta F_{total}}{\Delta \delta} - \frac{\Delta F_f}{\Delta \delta} = K_3 - |K_2|$$

where F_{cut} = cutting force

K_3 = loading slope

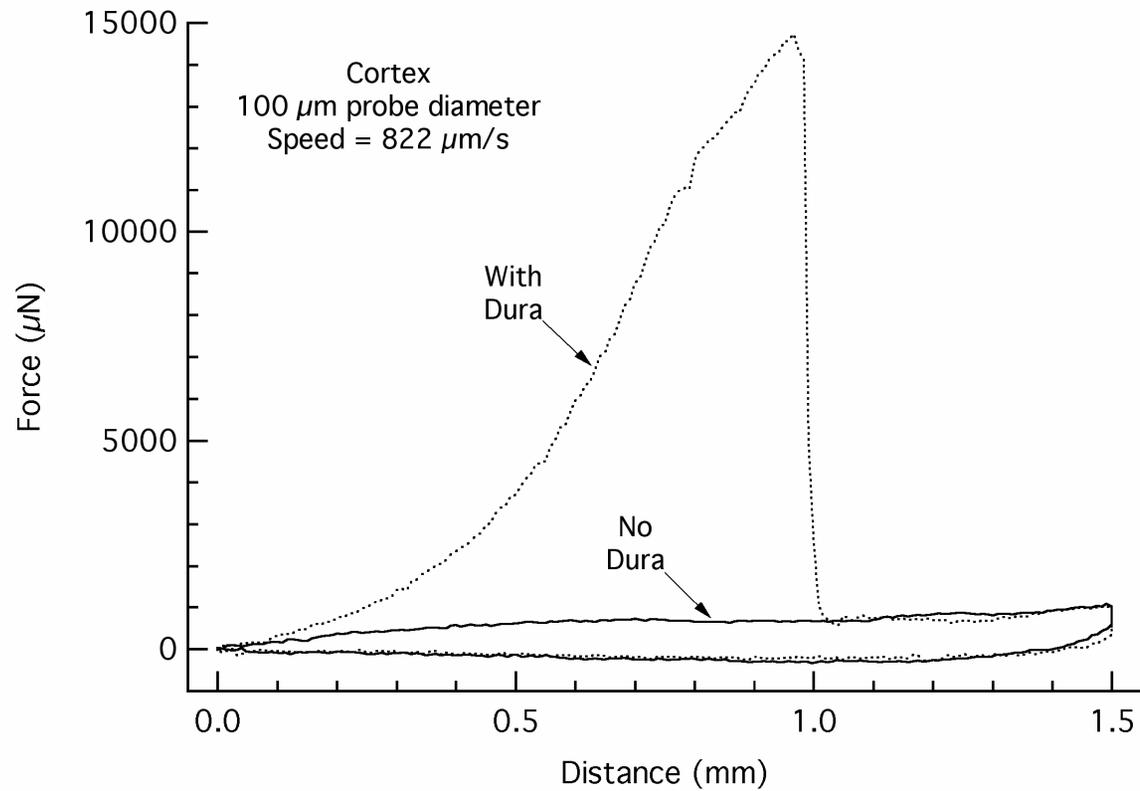
$\Delta F_{total}/\Delta \delta$ = the rate of change of the force read from the load cell

$\Delta F_f/\Delta \delta$ = the rate of change of frictional force

No significant change with rate, but interesting...



Dura and Pia Intact



Massive increase in insertion/maximum force!



Considerations for Future Implant Designs:

- 1) Points are useful – reduced forces, gradual build-up (shape)
- 2) Reduce insertion forces (force = energy = tissue damage?)
- 3) Balance implant diameter (shape) against implant stability
- 4) Relationship between insertion rate and adhesion – low frictional coefficient for insertion then modify to sticky?
- 5) What happens at fast insertion rates (pneumatic)?
- 6) Post-implantation modification?



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Supported by:

NSF # HRD-0086551, The Coleman Institute for Cognitive Disabilities,
NIDCD (DC00566) and NINDS (NS054161)

