

# Design Optimization of a Supersonic Natural Laminar Flow Business Jet

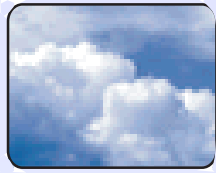
Peter Sturdza  
Desktop Aeronautics, Inc.  
4 December 2007



# Outline

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- ✦ Quick explanation of laminar flow and transition prediction
- ✦ Design of various laminar flow experiments
  - small blade under F-15
  - airfoils for lengthened blade
  - rocket-propelled sled test
- ✦ Full aircraft configuration aerodynamic optimization



# Natural Laminar Flow Supersonic Business Jet

- ◆ Conventional supersonic designs minimize wave drag
  - wing/body shaping (traditional “area ruling”)
  - propulsion integration
- ◆ Alternately can minimize skin friction
  - natural laminar flow
  - Aerion Corporation (Richard Tracy)



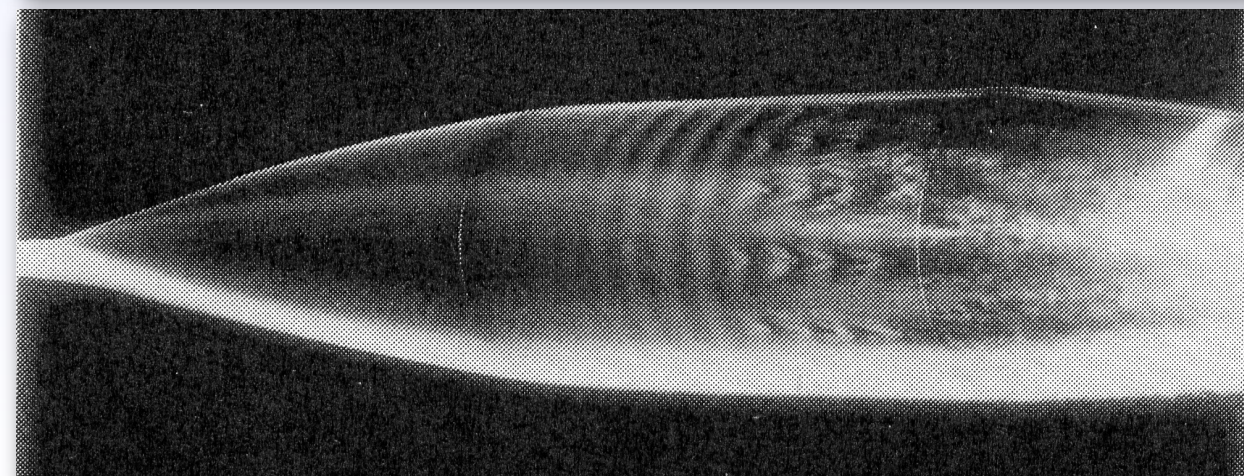
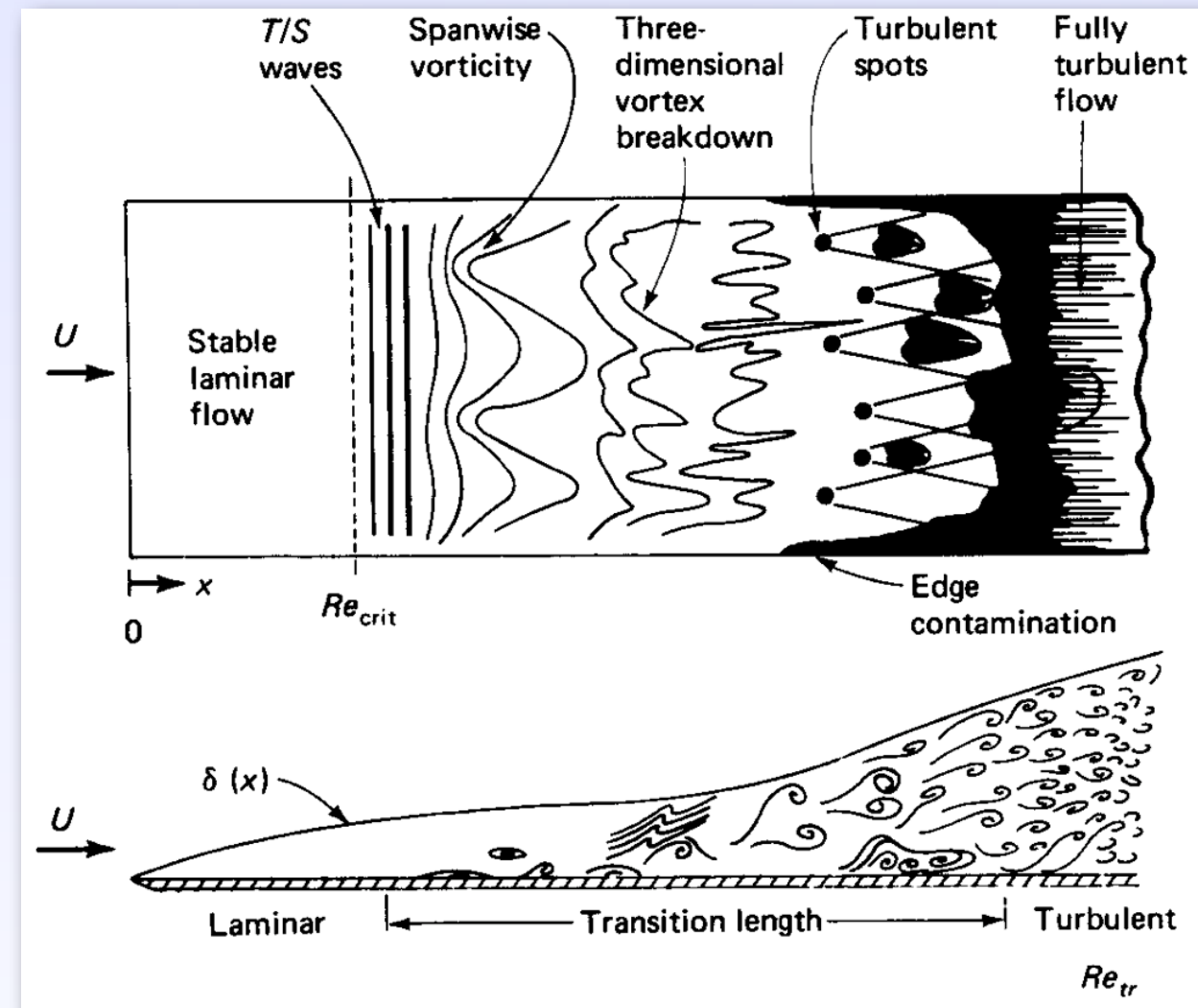
[www.aerioncorp.com](http://www.aerioncorp.com)





# Laminar to Turbulent Transition

- ◆ Viscous boundary layer near surface begins in laminar state
- ◆ Laminar flow becomes unstable
  - initially instabilities behave as linear waves
  - various types of instabilities exist
- ◆ Turbulent flow bad for drag
  - skin friction increases 5 to 10-fold (depending on flight conditions)
  - very little laminar flow in today's jet aircraft







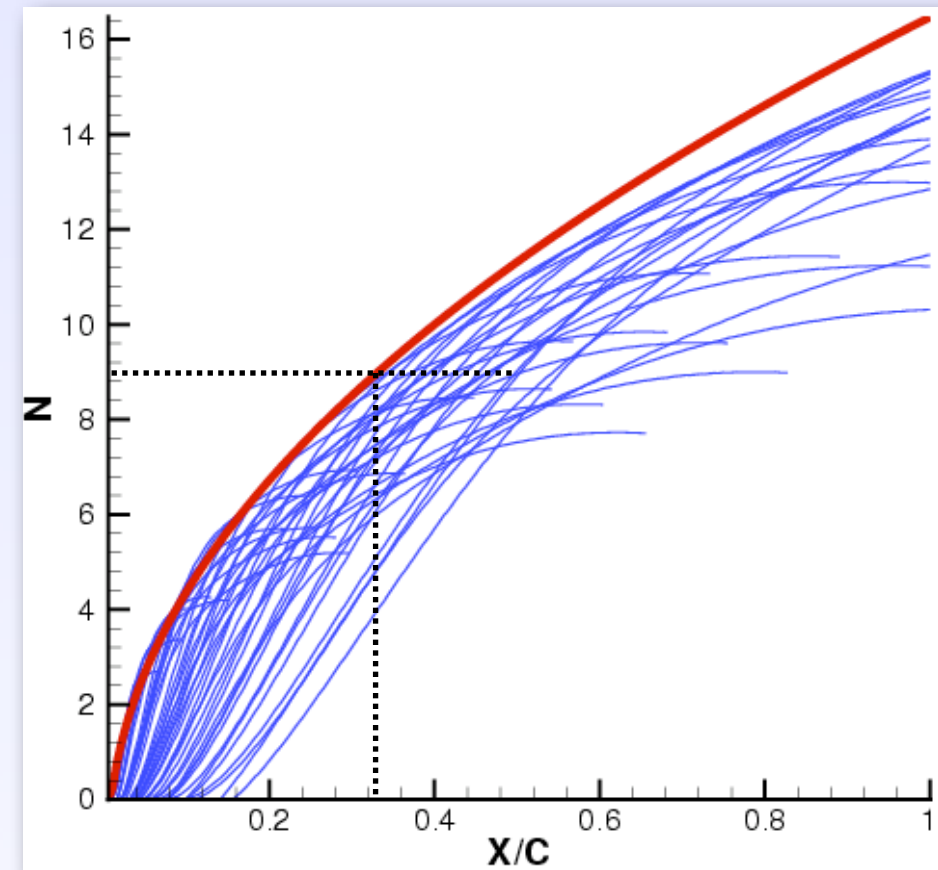
# Design for Laminar Flow

- ◆ Current aviation industry practice very limited
  - 2-D airfoil section design based on pressure distribution
  - Beech did 3-D inverse design to a specified pressure distribution (Alonso & Reuther SYN-107)
  - interest in laminar flow increasing for transonic aircraft
- ◆ For Aerion, laminar flow drives entire configuration
  - strong coupling between supersonic wave drag and laminar flow
  - need transition modeling for conceptual design



# Modeling Transition

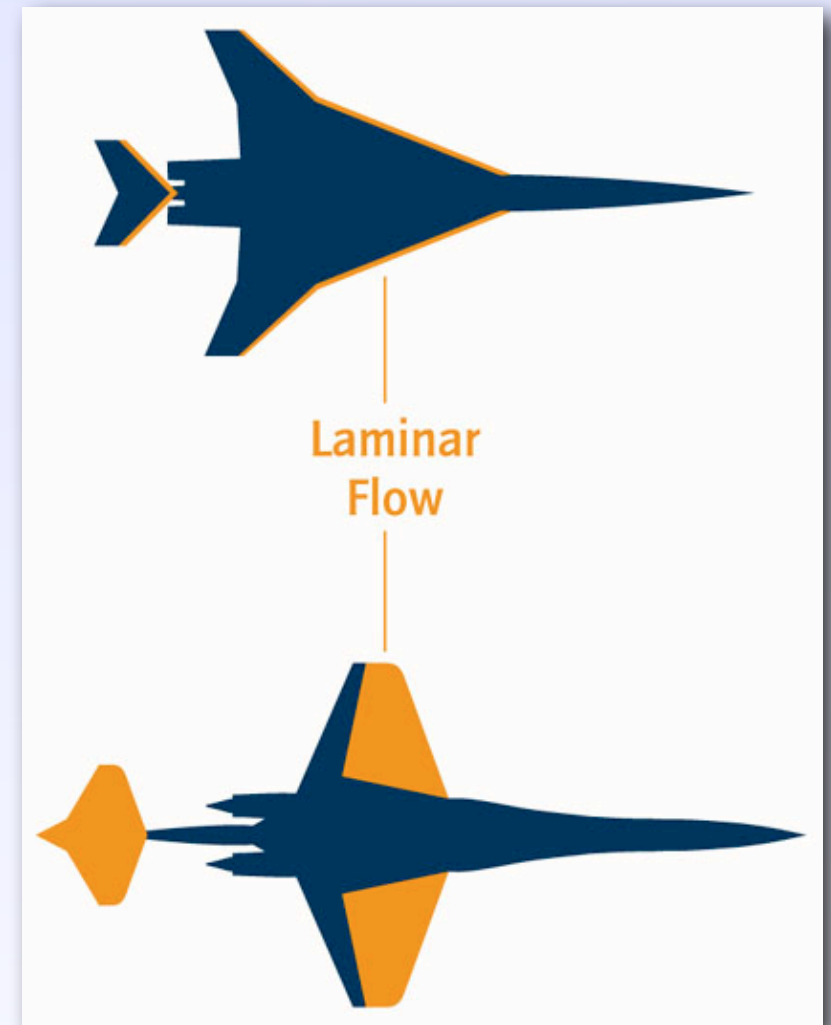
- ✦ Direct computation of transition still not practical
- ✦ Relatively high-fidelity transition prediction available since the '80s
  - computationally intensive, even the semi-empirical “ $e^N$ ” method
  - human intervention required: “massaging” and “baby sitting”
  - not suited for numerical optimization
- ✦ Database or parametric models used instead
  - very fast
  - less accurate, but
  - can be focused around particular characteristics of aircraft of interest





# Aerion Concept

- ◆ Supersonic flight stabilizes laminar flow
- ◆ Low wing sweep
  - delay crossflow transition
- ◆ Sharp leading edge
  - decrease wave drag
  - eliminate attachment line transition
  - favorable pressure gradient delays TS transition
- ◆ Thin wing
  - minimize wave drag
  - fuselage area ruling
  - structural and fuel volume trade
- ◆ Optimization necessary

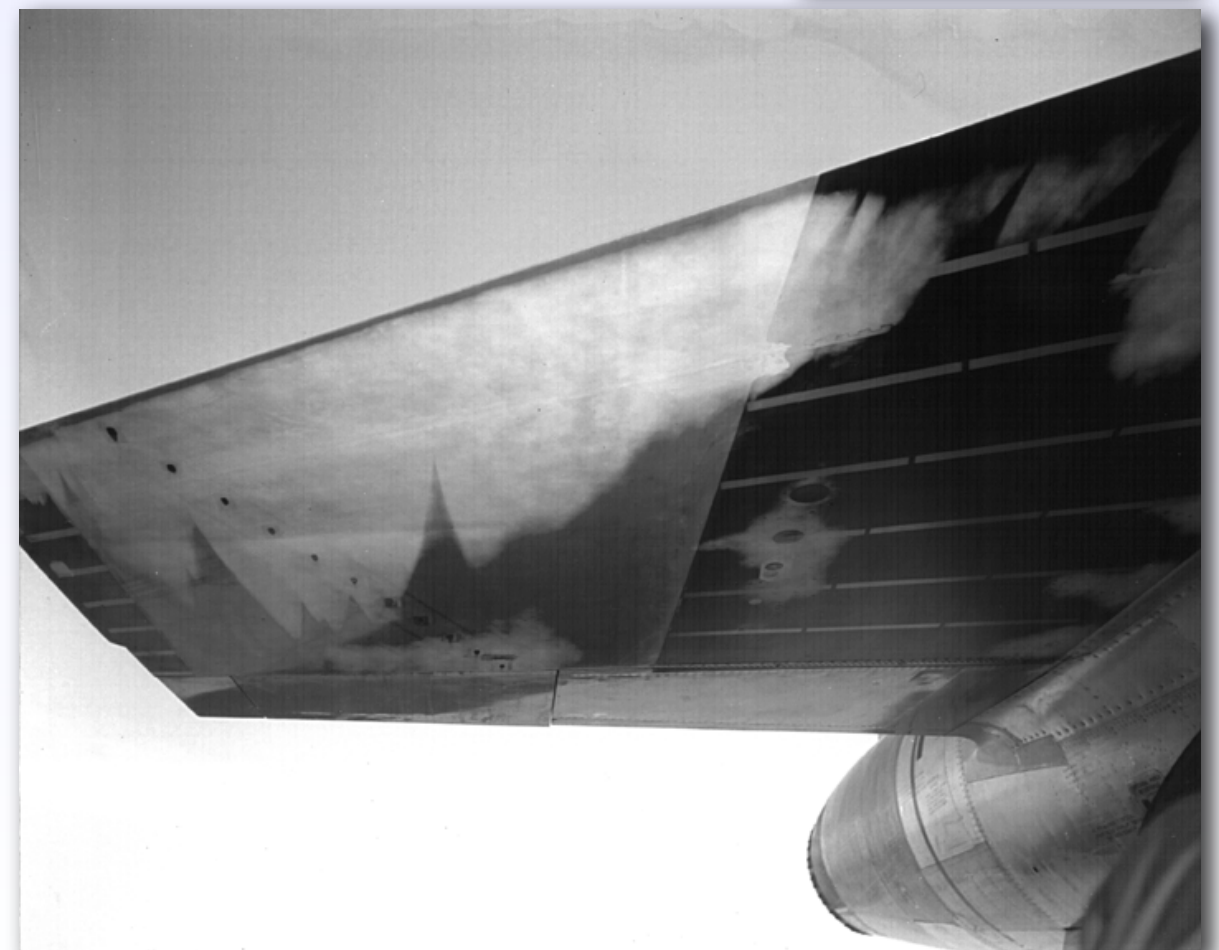






# Does it Really Work?

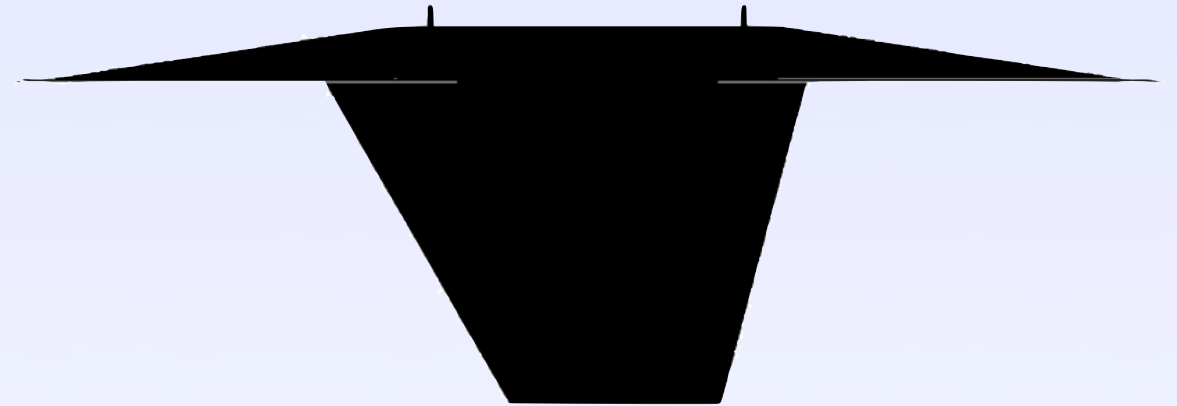
- ◆ V-2 nose cone in 1950
  - Demonstrated 90 million  $Re_{tr}$  at Mach 2.7
- ◆ F104 test in 1959
  - Demonstrated 8 million  $Re_{tr}$  at Mach 2
  - Difficult to analyze due to lack of geometry model
- ◆ Most other tests on high Mach reentry bodies



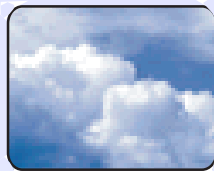


# Does it really work?

- ◆ Flight test under F-15B
- ◆ Aerion-like wing
  - Span: 80 cm
  - Sweep:  $30^\circ$  or  $15^\circ$
  - Thickness: 3.5% root, 2.5% tip

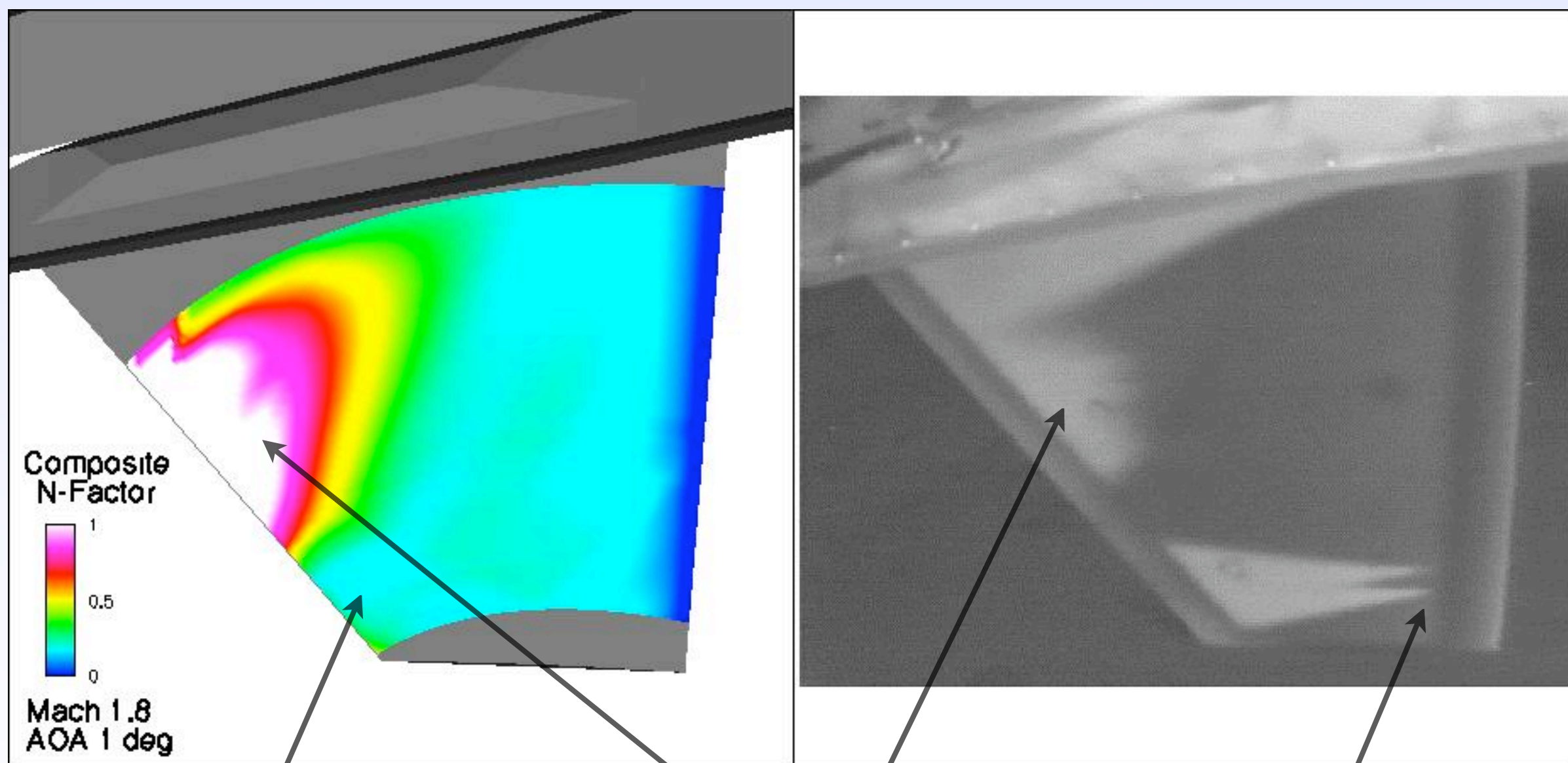






# Does it Really Work?

## Mach 1.8



colors:  
laminar flow

white:  
turbulent flow

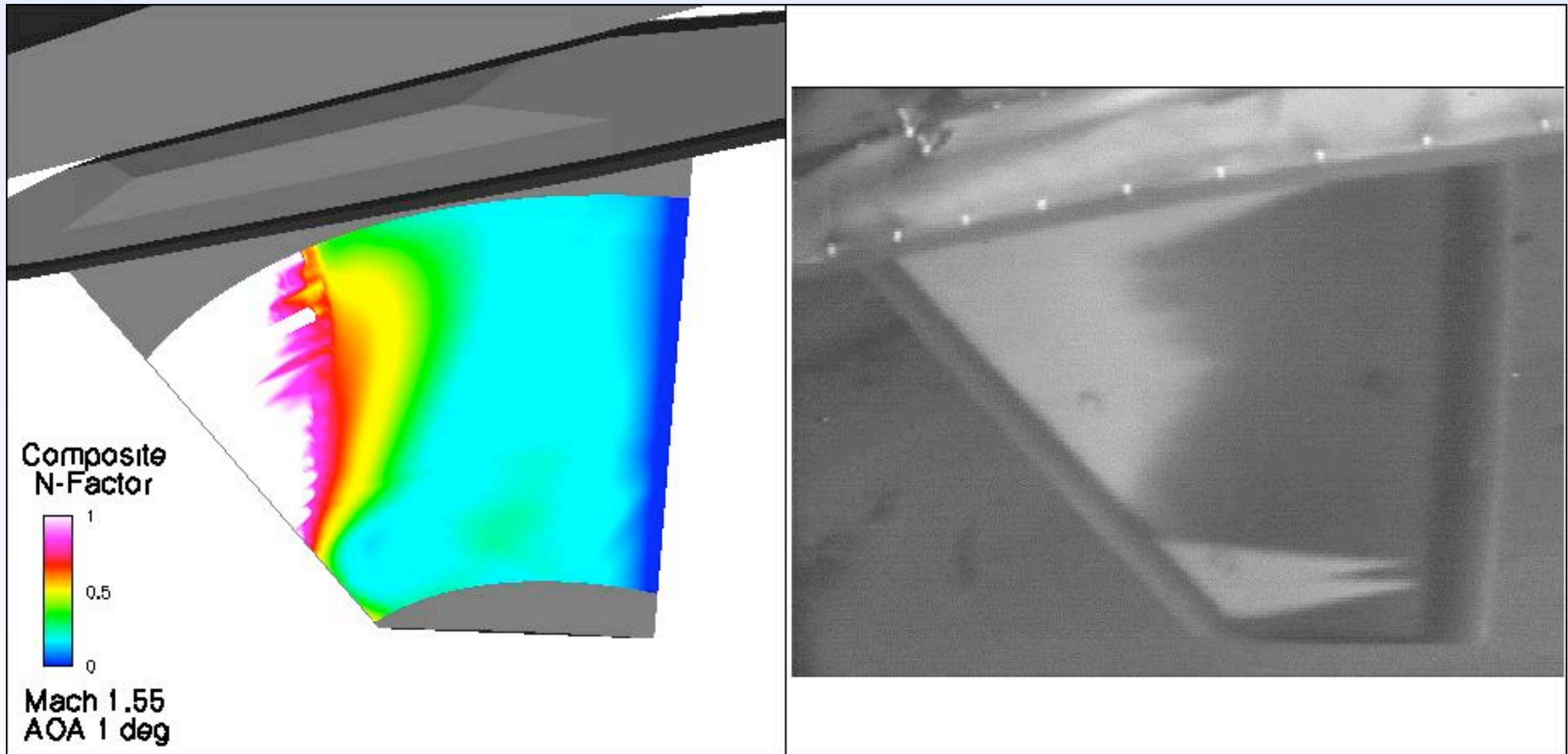
deliberate trips





# Does it Really Work?

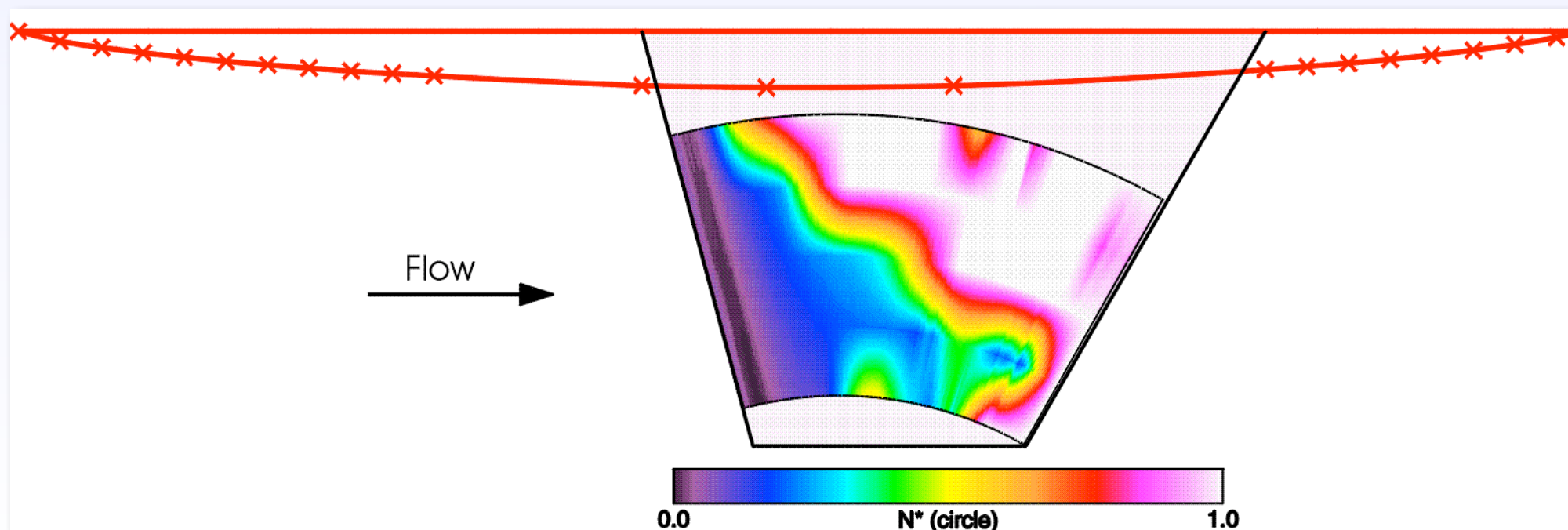
## Mach 1.55

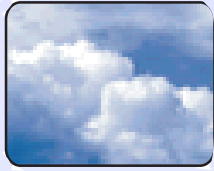




# Early Design with Transition

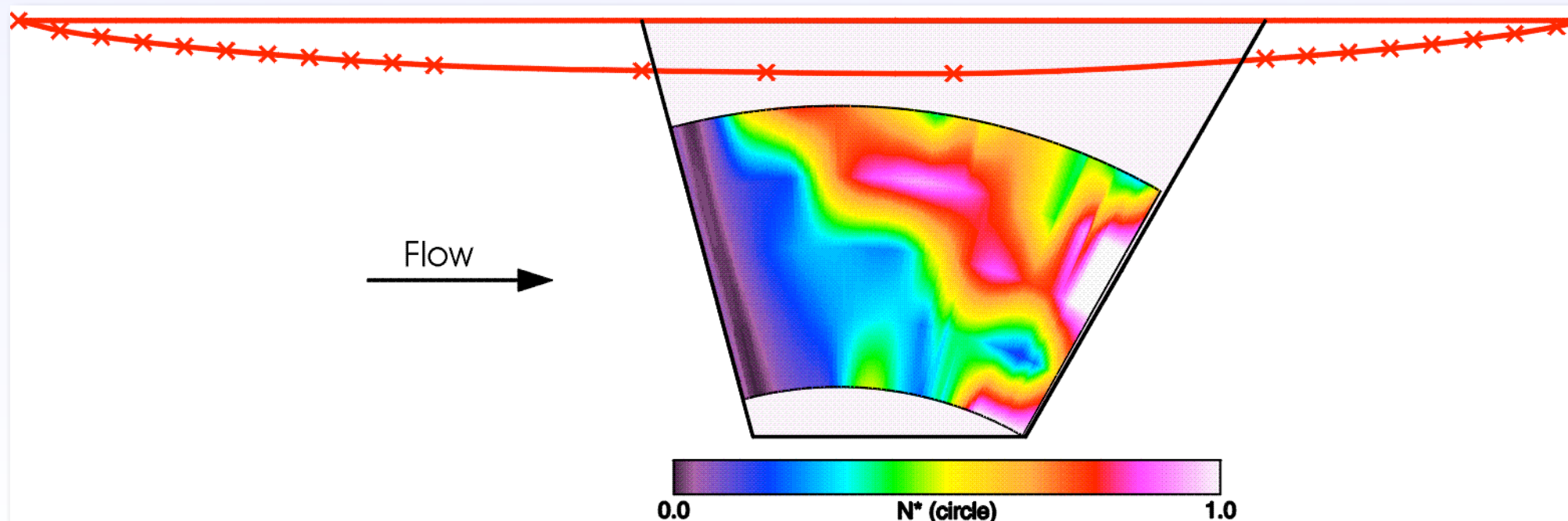
- ◆ Proposed flight test article
  - fuselage half-body added to previous test article
  - Designed for Mach 1.8 at 40,000 feet
- ◆ Addition of half-body spoils laminar flow
  - Mach wave from wing leading-edge intersection
  - perhaps shaping can recover laminar flow?





# Early Design with Transition

- ◆ Shape optimization for laminar flow
  - quadratic response surface + trust region
  - 3 design variables initially
- ◆ Laminar flow increased
  - nearly to trailing edge
  - “hot spots” very close to transition



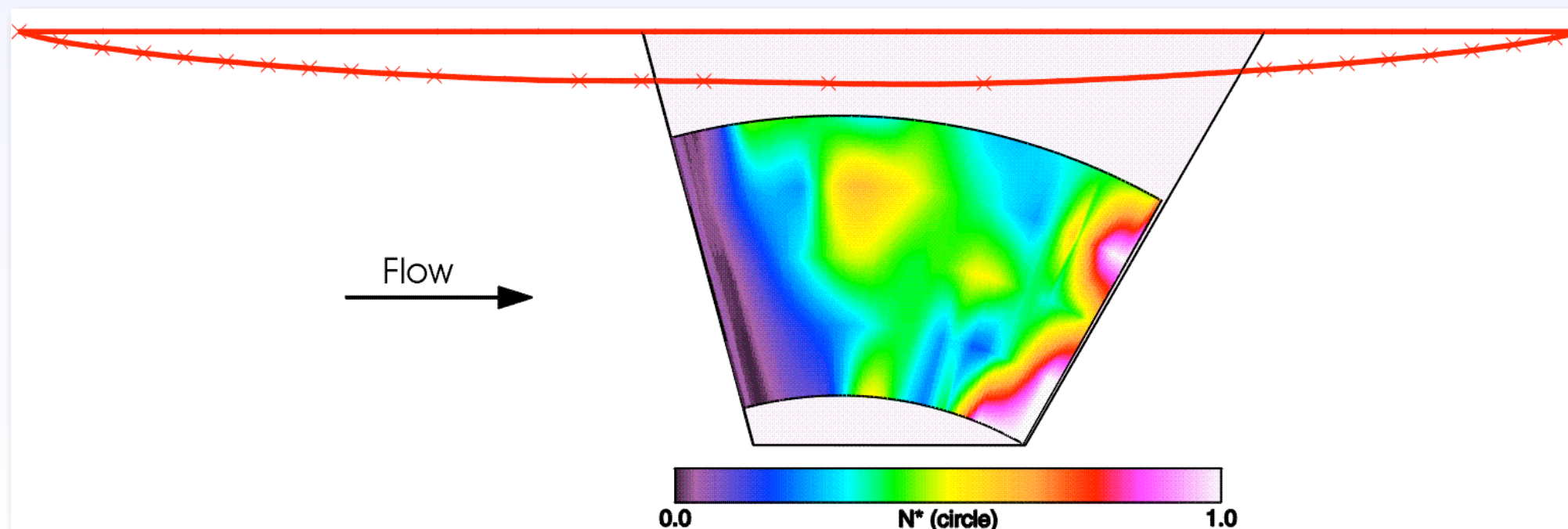




# Early Design with Transition

## ◆ Final design iteration

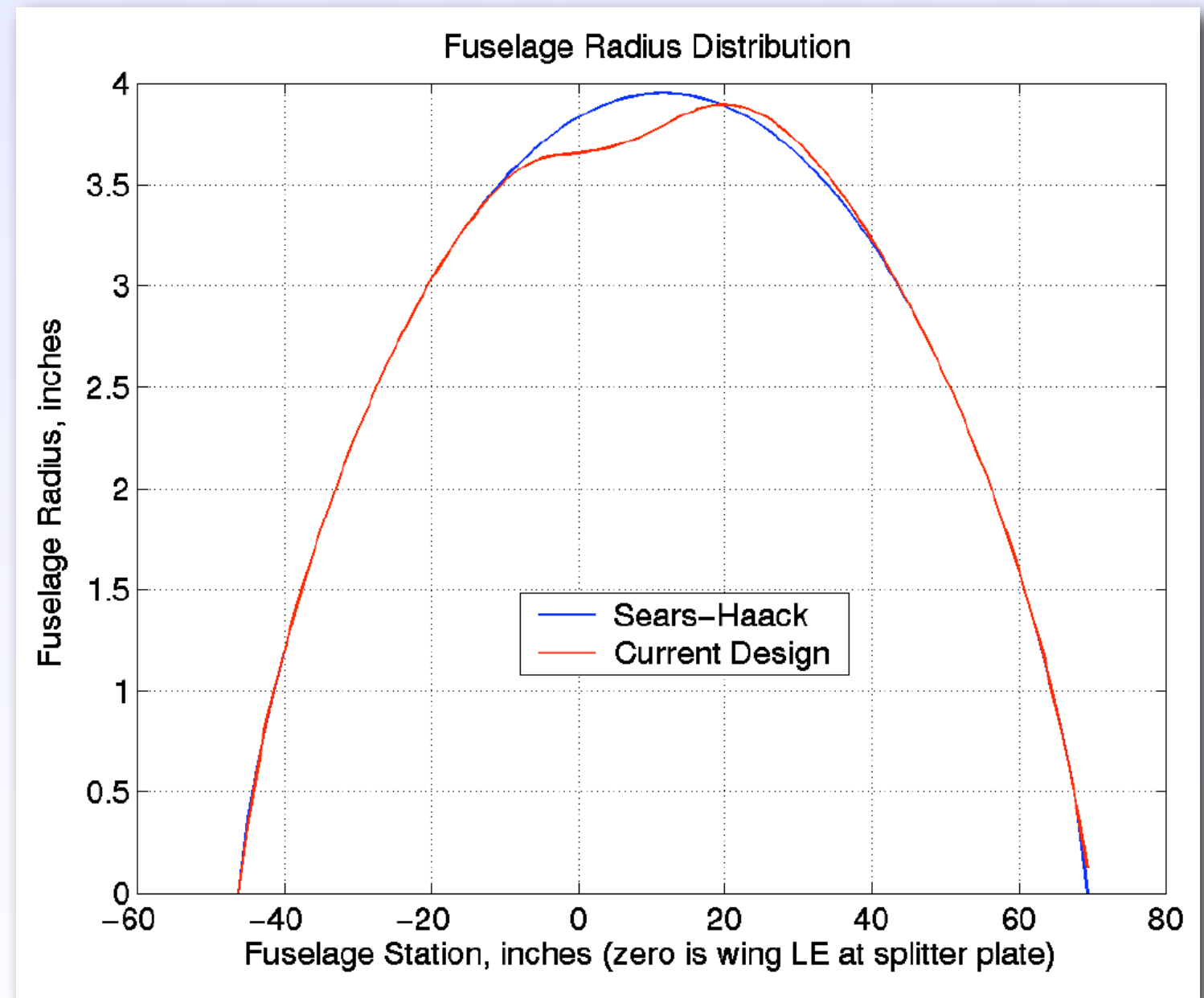
- increased to five design points on fuselage
- transition margins increased

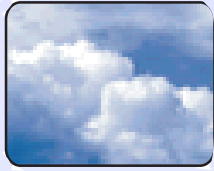




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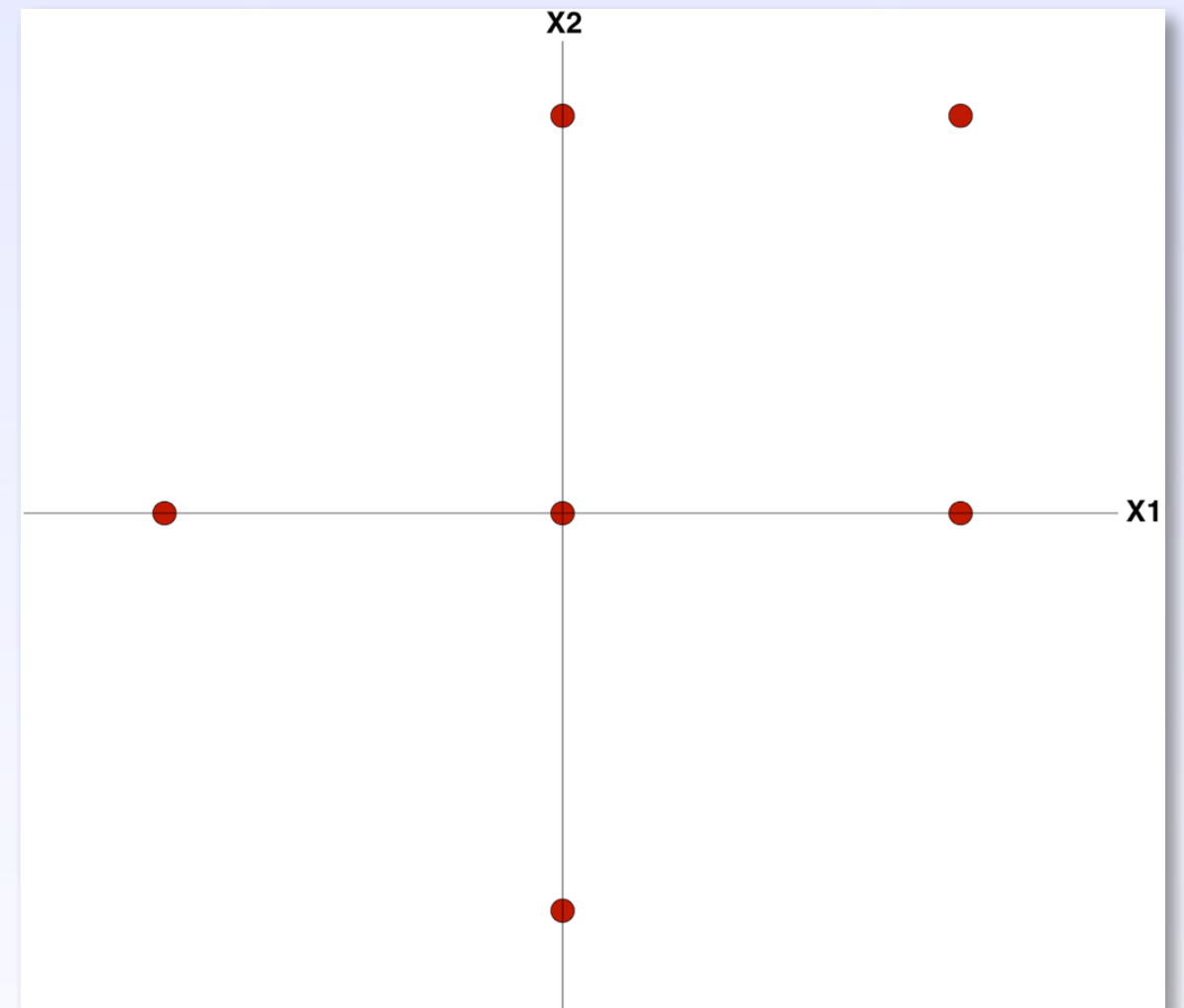
- ◆ Fuselage reshaping is subtle
- ◆ Implies that design for laminar flow can be somewhat independent of area ruling





# Details of Optimization

- ◆ Quadratic response surface with trust region algorithm
- ◆ Simplex-based point stencil
  - symmetric in design space
  - can sometimes reflect simplex to move trust region, re-using some old points
- ◆ 7 iterations
  - took advantage of reflection to save function evaluations
  - trust region updates by hand

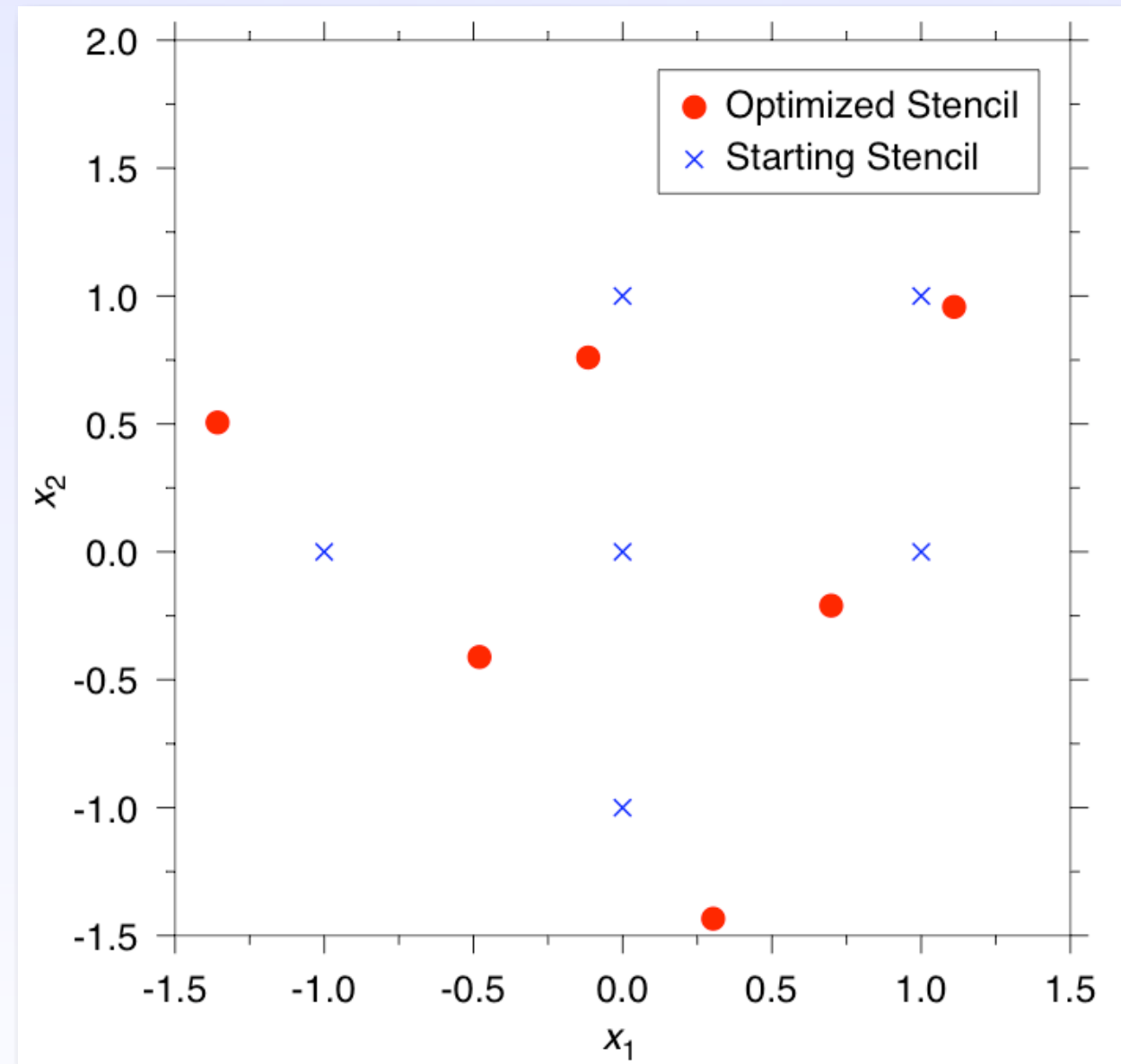






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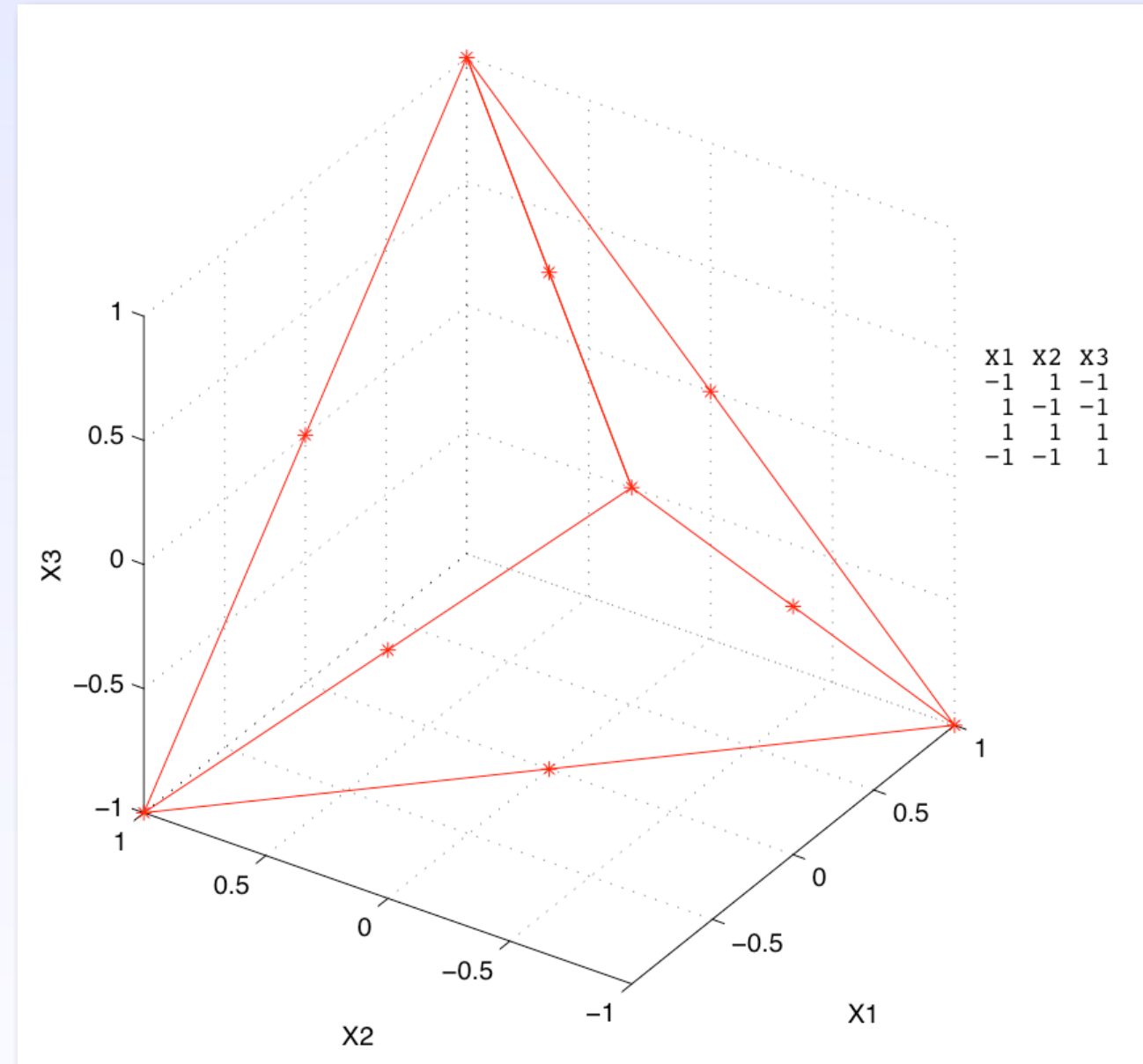
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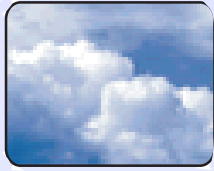




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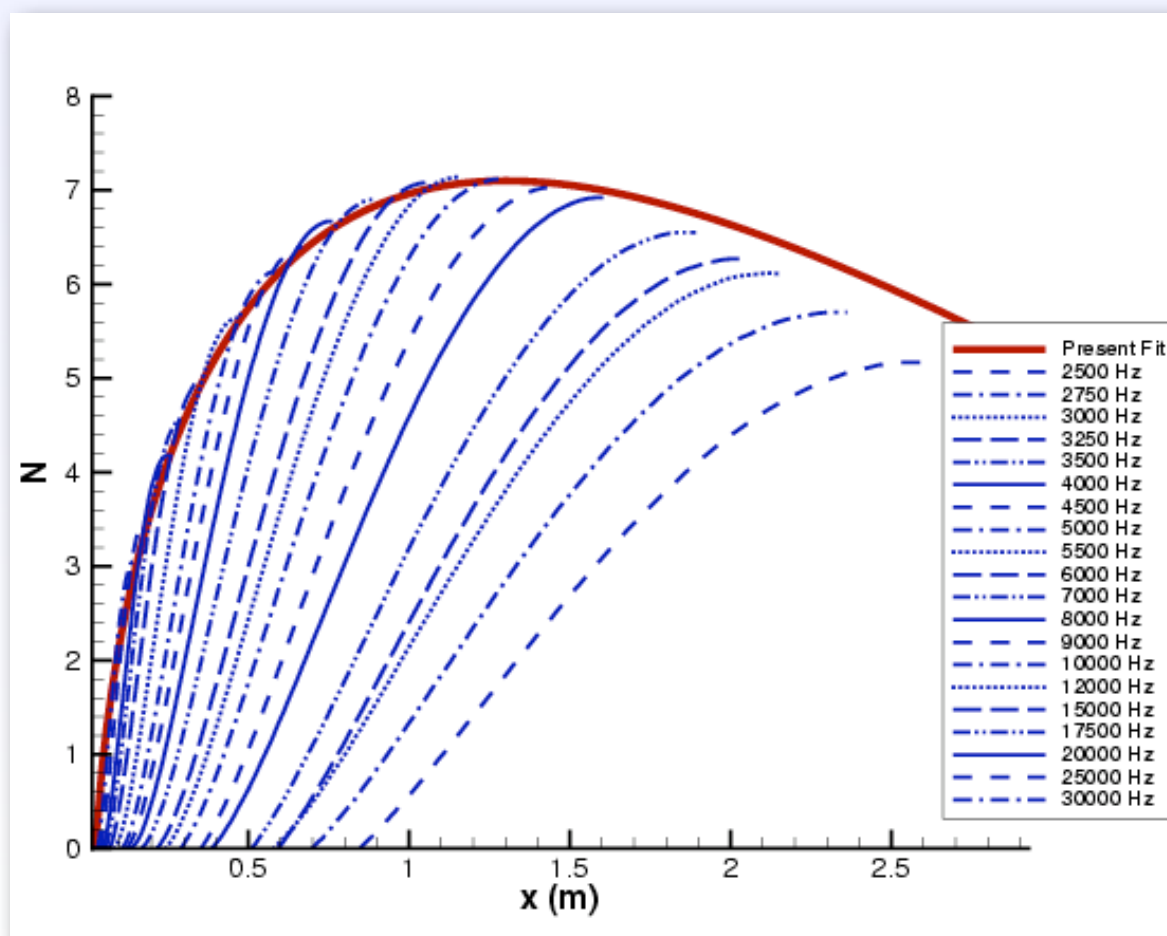
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# Airfoil Design for Laminar Flow

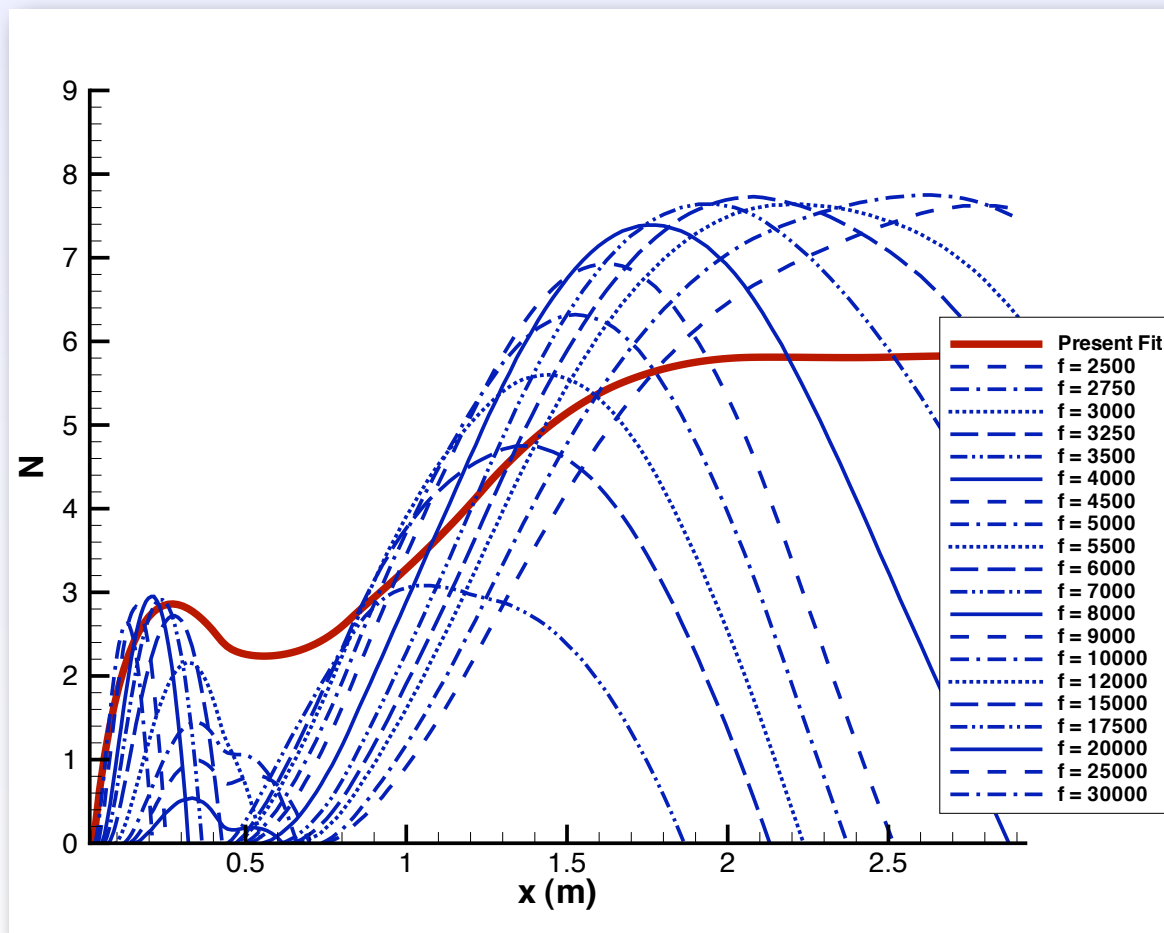
- ♦ Minimize N-factor on 2D airfoil at Mach 1.8
- ♦ 6 shape variables
- ♦ Thickness constrained to not more than 3% t/c
- ♦ Starting shape: parabolic biconvex



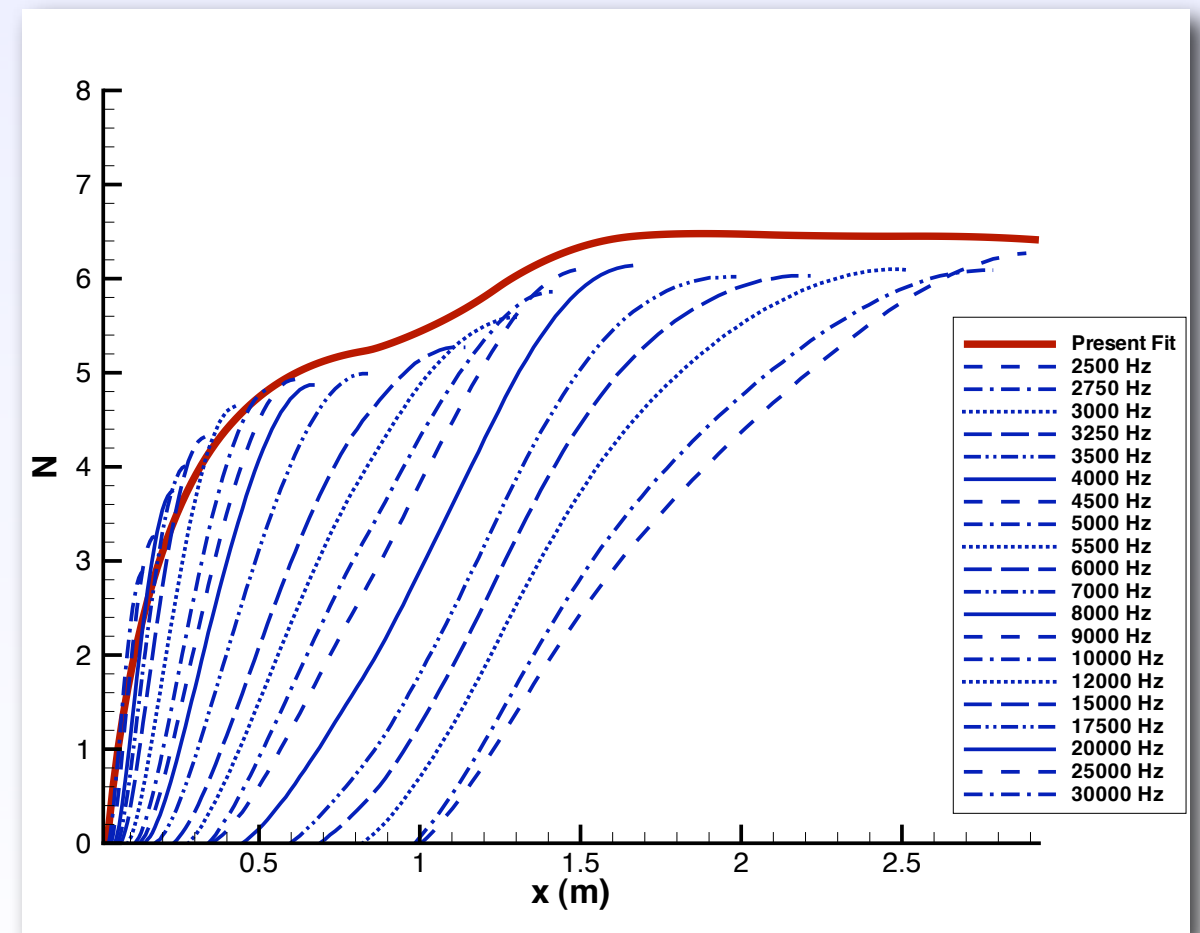


# Airfoil Design for Laminar Flow

Initial optimization broke  
parametric fit



Quick fix: constraint on  
pressure gradient

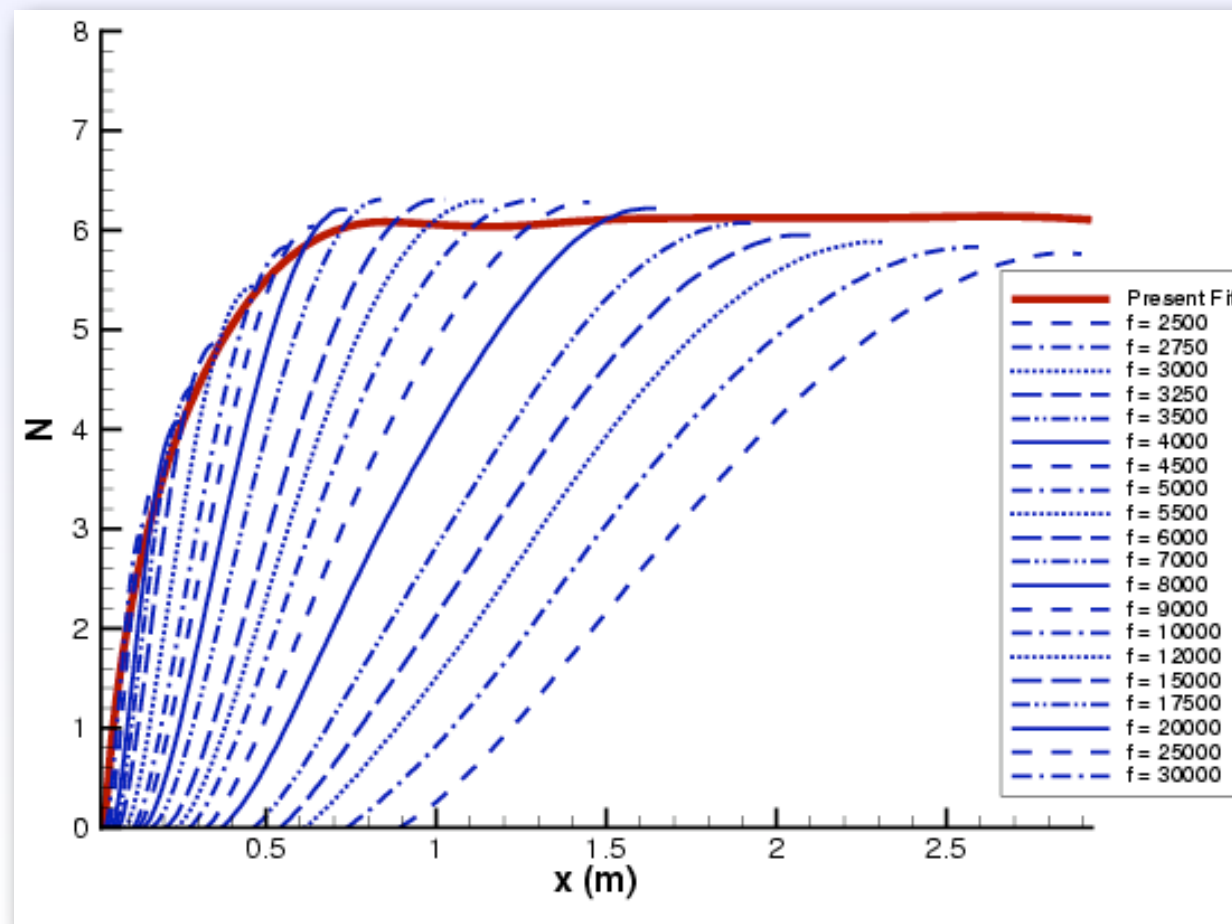






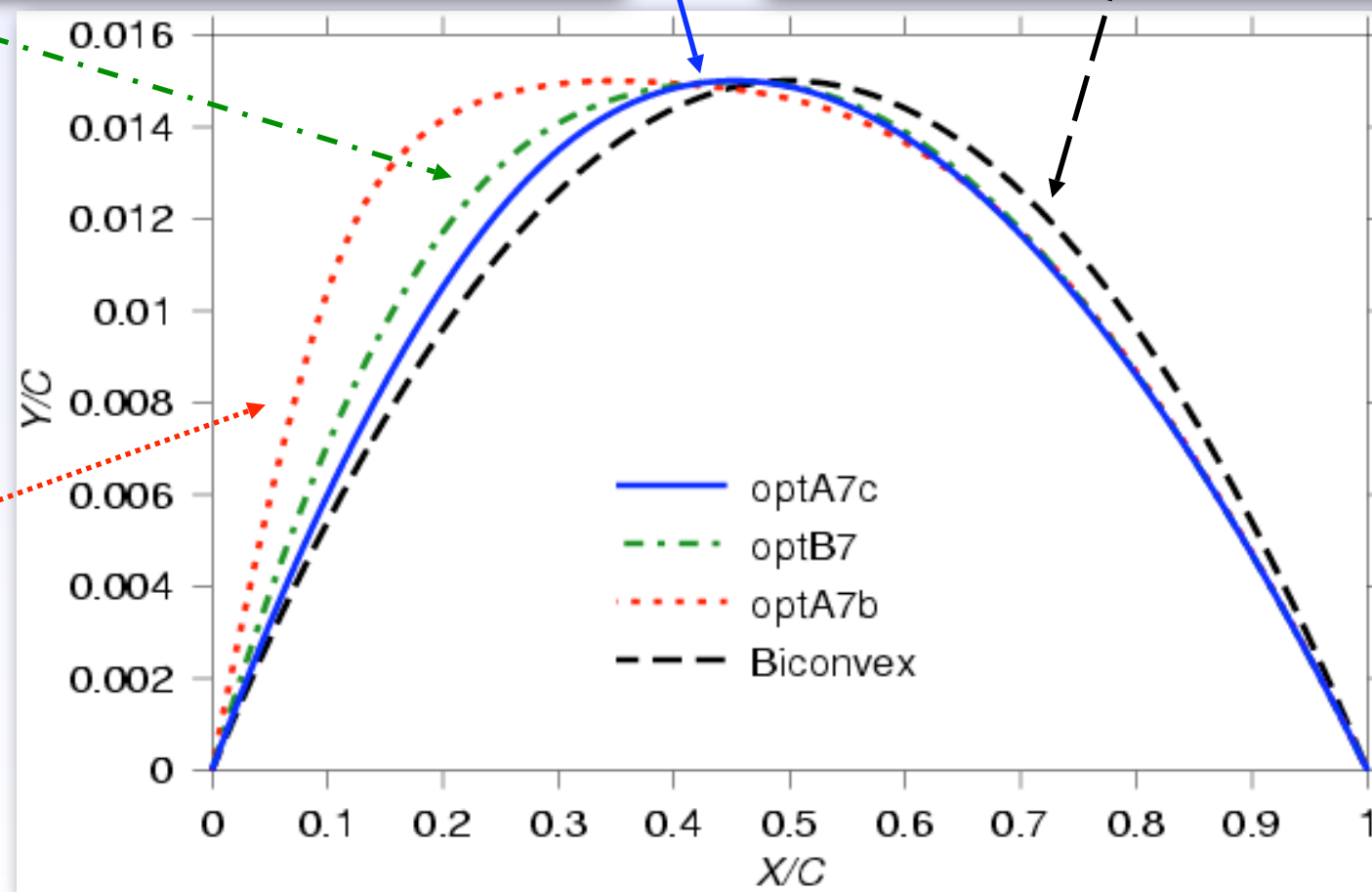
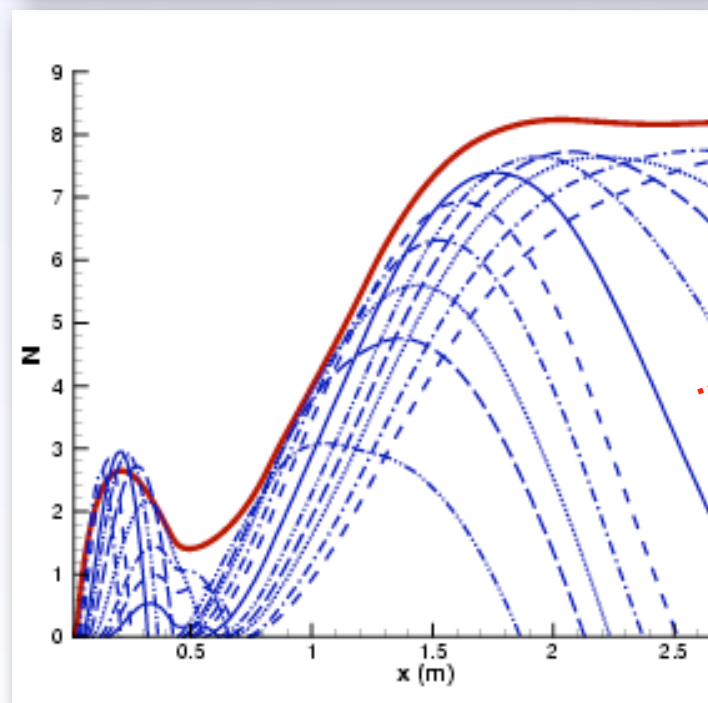
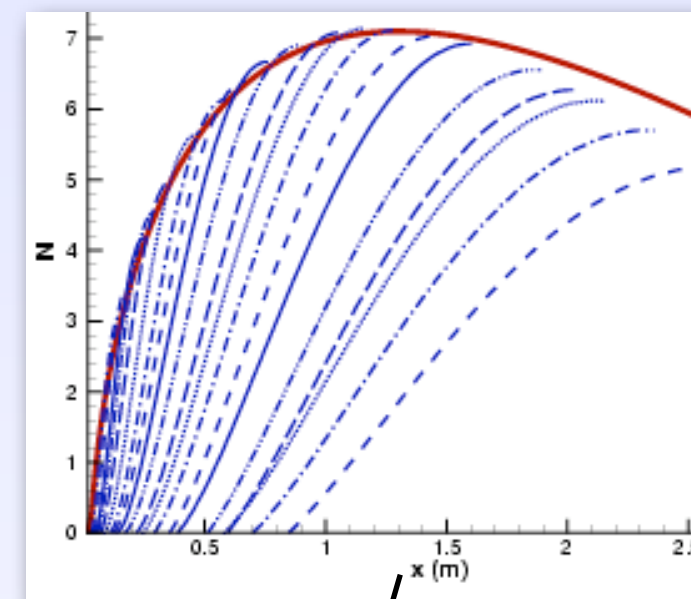
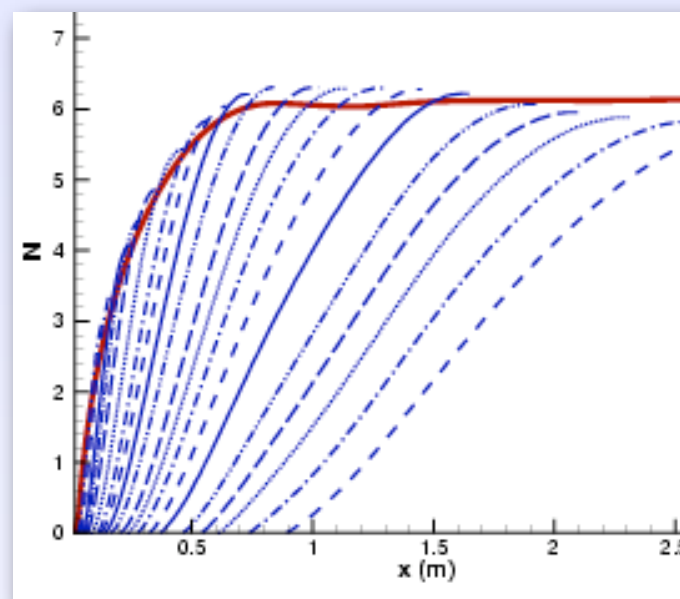
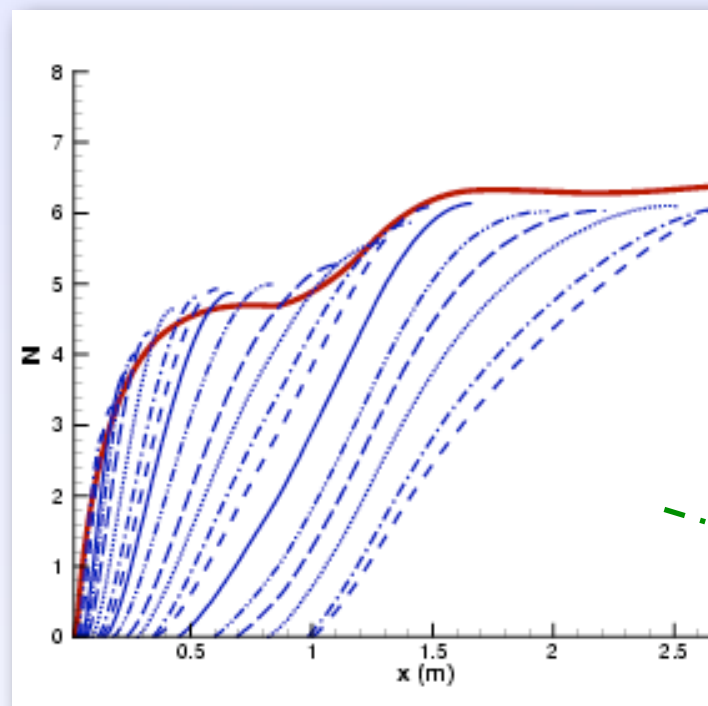
# Airfoil Design for Laminar Flow

- ✦ Original N-factor fits too approximate
- ✦ Final design
  - flat N-factor aft of 20% chord
  - high-fidelity instability analysis in reasonable agreement
  - section maximum thickness slightly forward





# Airfoil Design for Laminar Flow





# Details of Optimization

- ✦ Gradient-based sequential-quadratic optimization
- ✦ Complex-step derived gradients
- ✦ Maximum N-factor splined with Akima algorithm
- ✦ Issues when multiple maxima in N-factor arise
  - maximum location jumps between different peaks
  - optimizer sees inaccurate gradients near optimum
  - tried reformulated objective using norms of discrete N-factors
    - smooth objective near optimum
    - does not improve convergence rate
    - regions of airfoil with control over maxima still moves around



# Rocket-Sled Test

- ♦ Rocket-propelled sled accelerated to Mach 1.5 - 1.6
  - Test blade representative of Aerion wing planform and airfoils
  - 30 million + Reynolds number
- ♦ Main issues
  - Structural vibration from sled runners and pusher rockets
  - Very high Reynolds/foot ~ 5x flight scale
    - Laminar stability requires higher surface quality (more polished)
    - IR requires high emissivity coating (less polished)
  - Heating from rocket plume destabilizes laminar flow
- ♦ Testing to determine feasibility is on-going



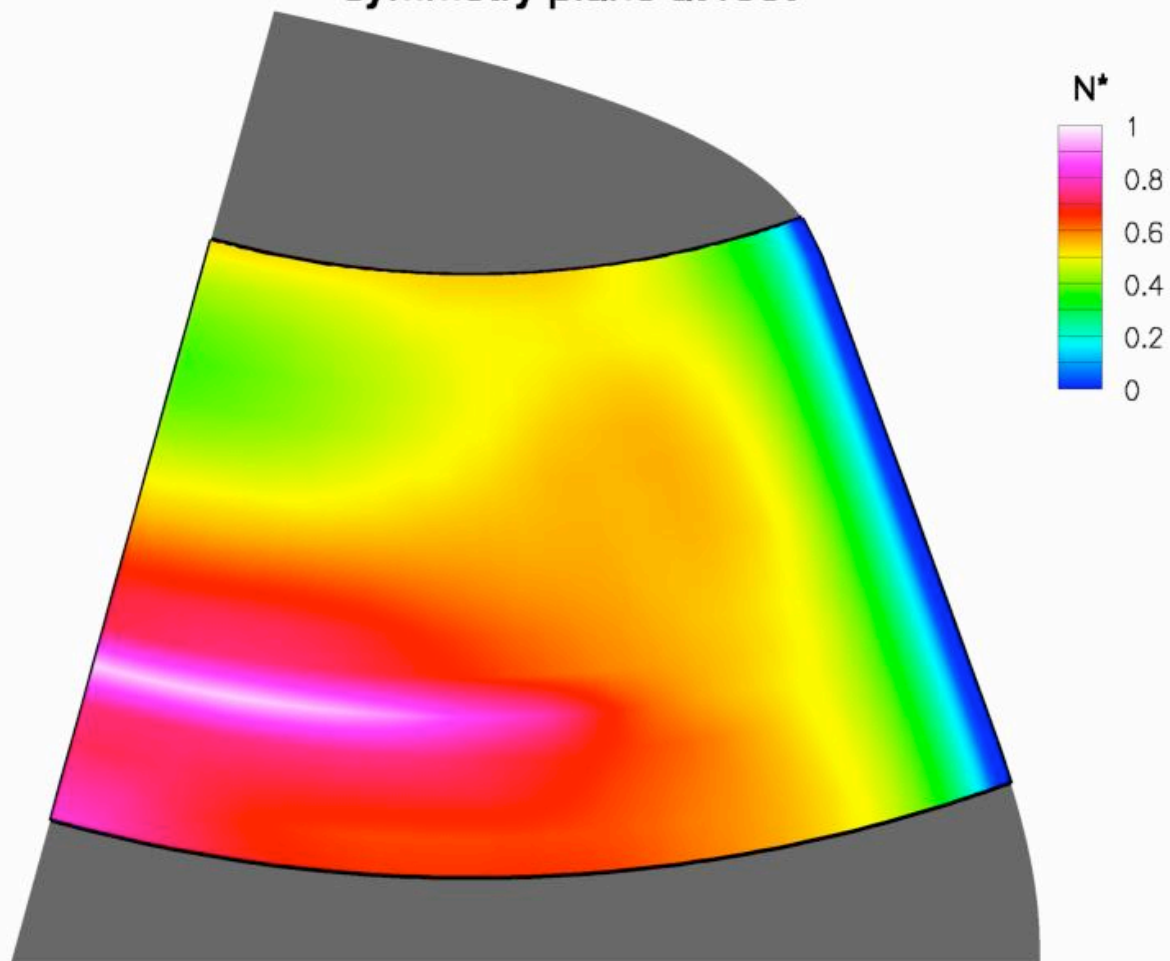




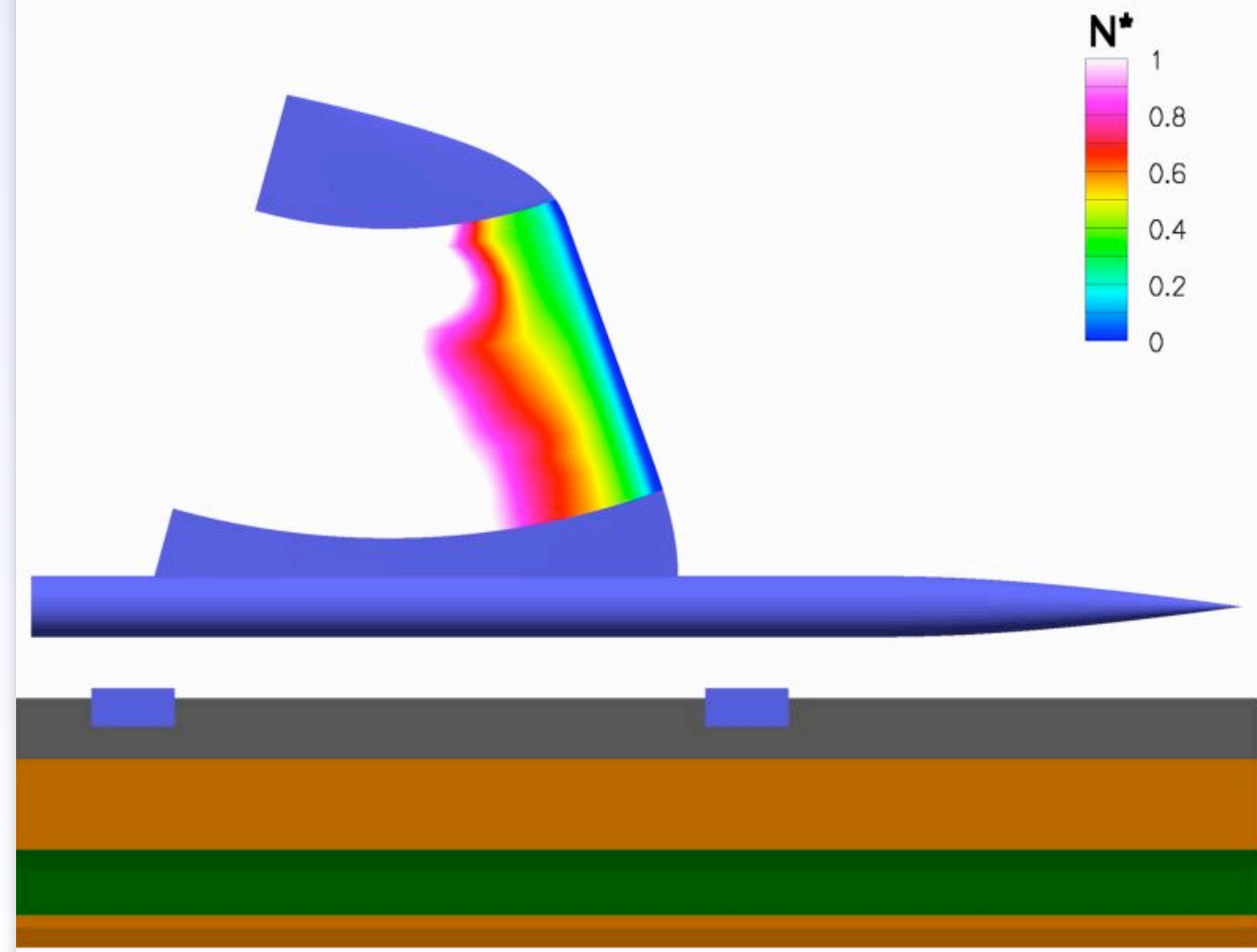
# Rocket-Sled Test

Complex geometry necessary for aerodynamic analysis and design of test article

Rocket-Sled Test Article at Mach 1.6, 5000 ft  
Biconvex Airfoils  
symmetry plane at root



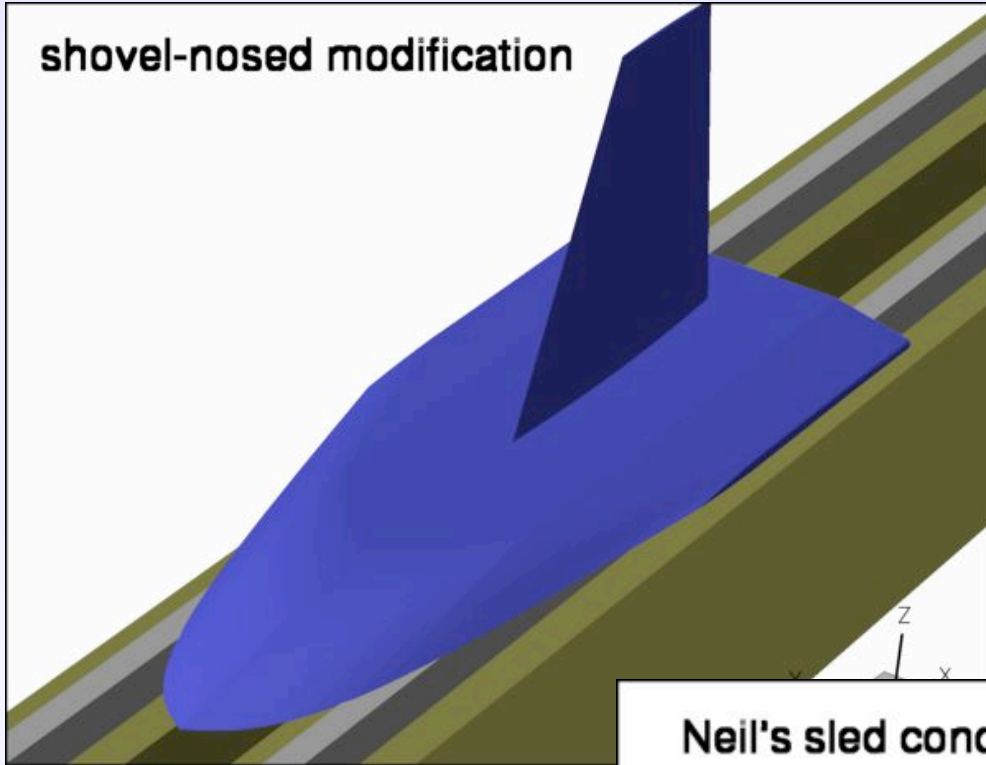
Baseline sled at Mach 1.6



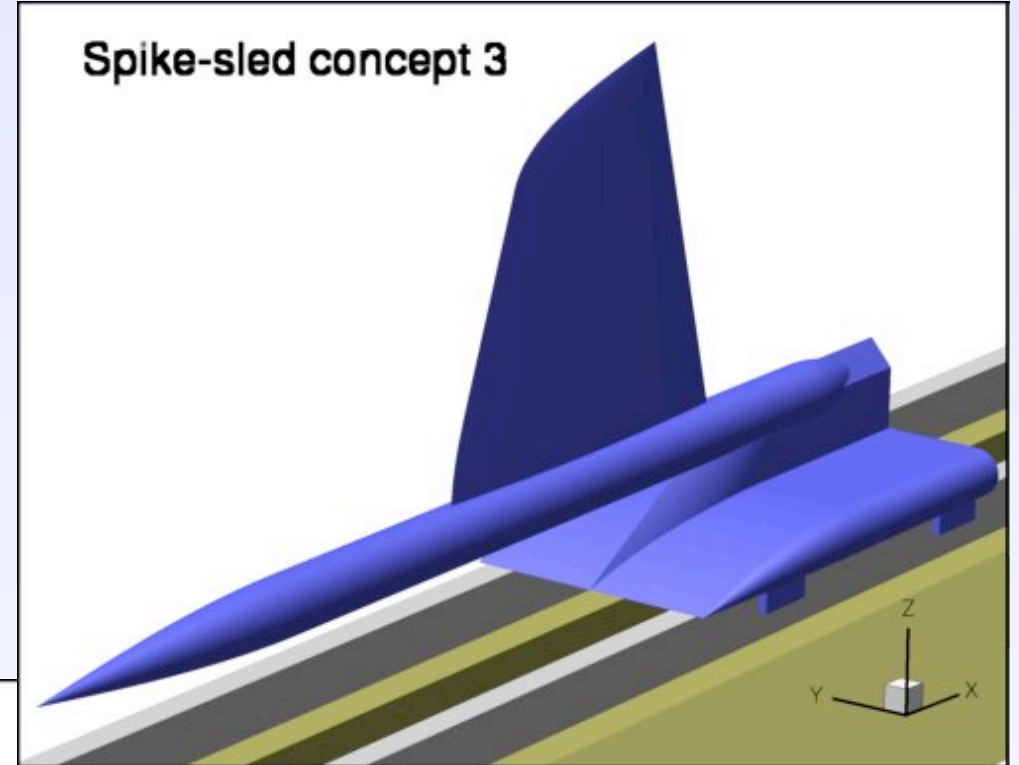


# Rocket-Sled Test

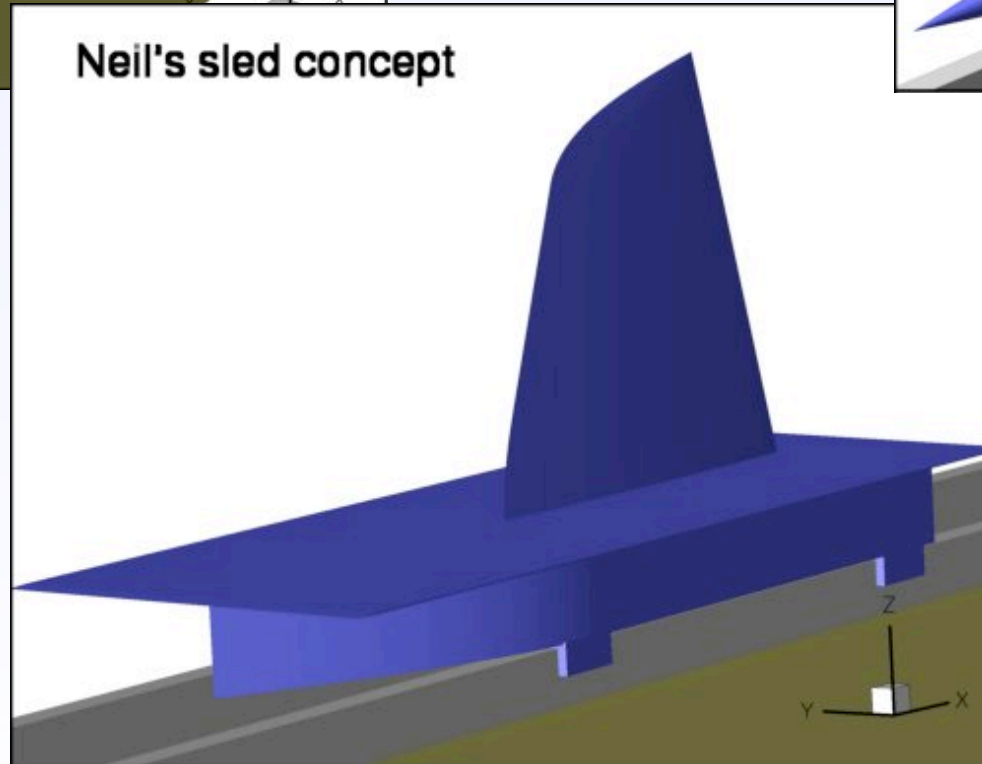
shovel-nosed modification



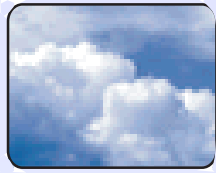
Spike-sled concept 3



Neil's sled concept

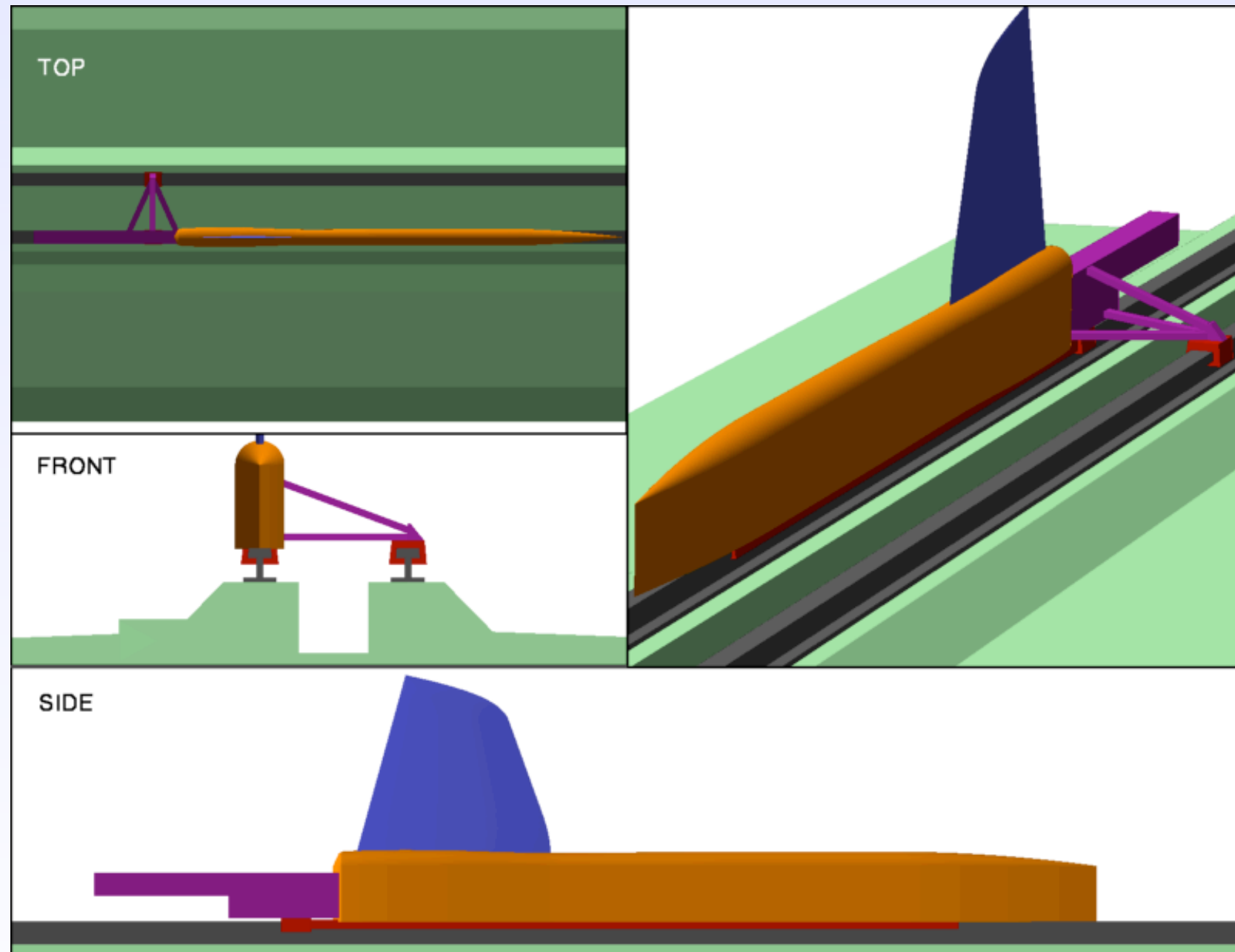


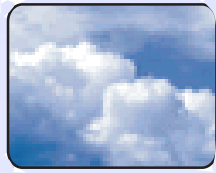
CFD-ready  
geometries analyzed  
with Cart3D



# Rocket-Sled Test

- ◆ Settled on monorail sled design
- ◆ Minimizes flow disturbances on test surface
- ◆ Allows more flexibility for avoiding choking and excessive forces due to flow in channel between rails
- ◆ Good spread of shoes to react forces and moments

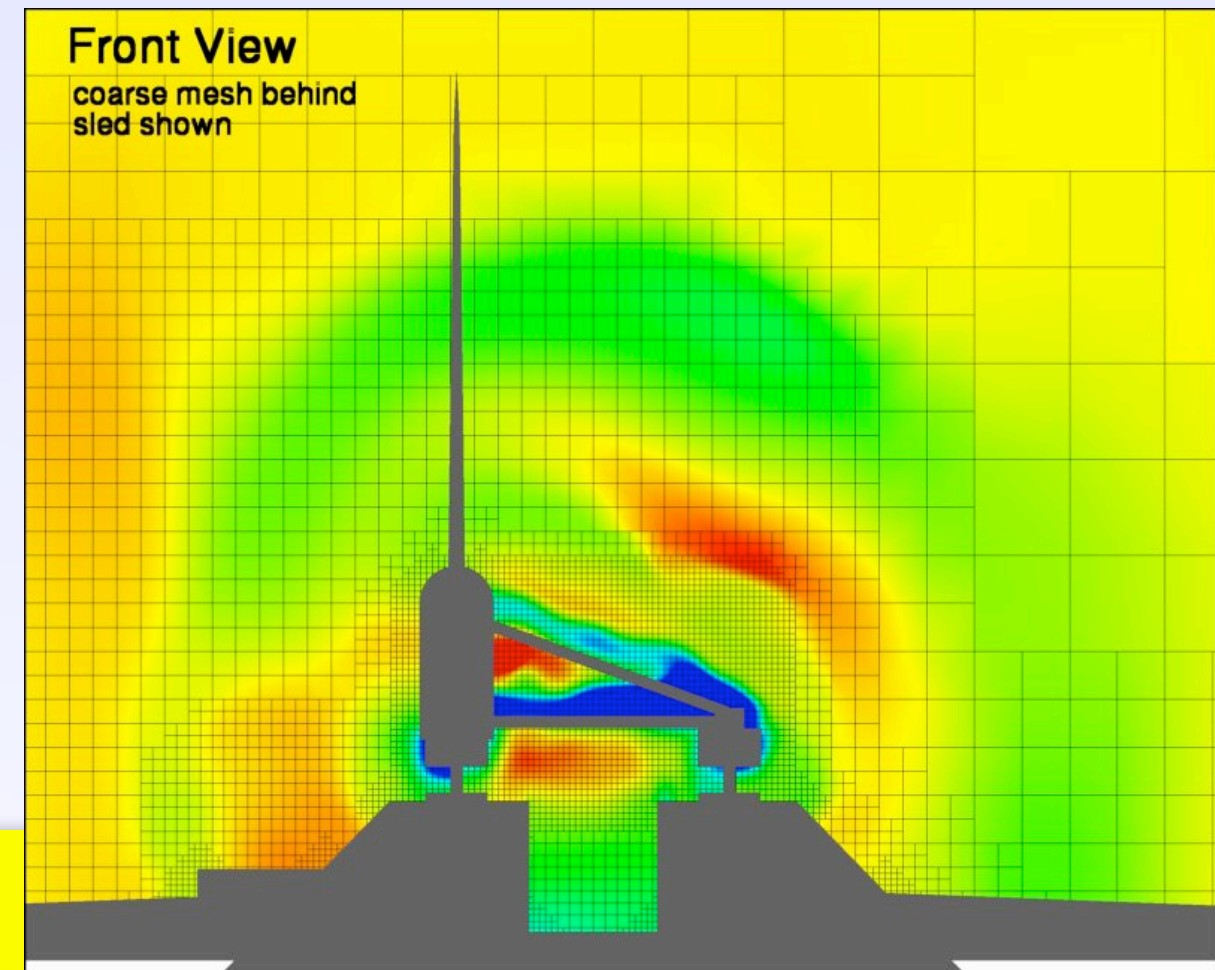
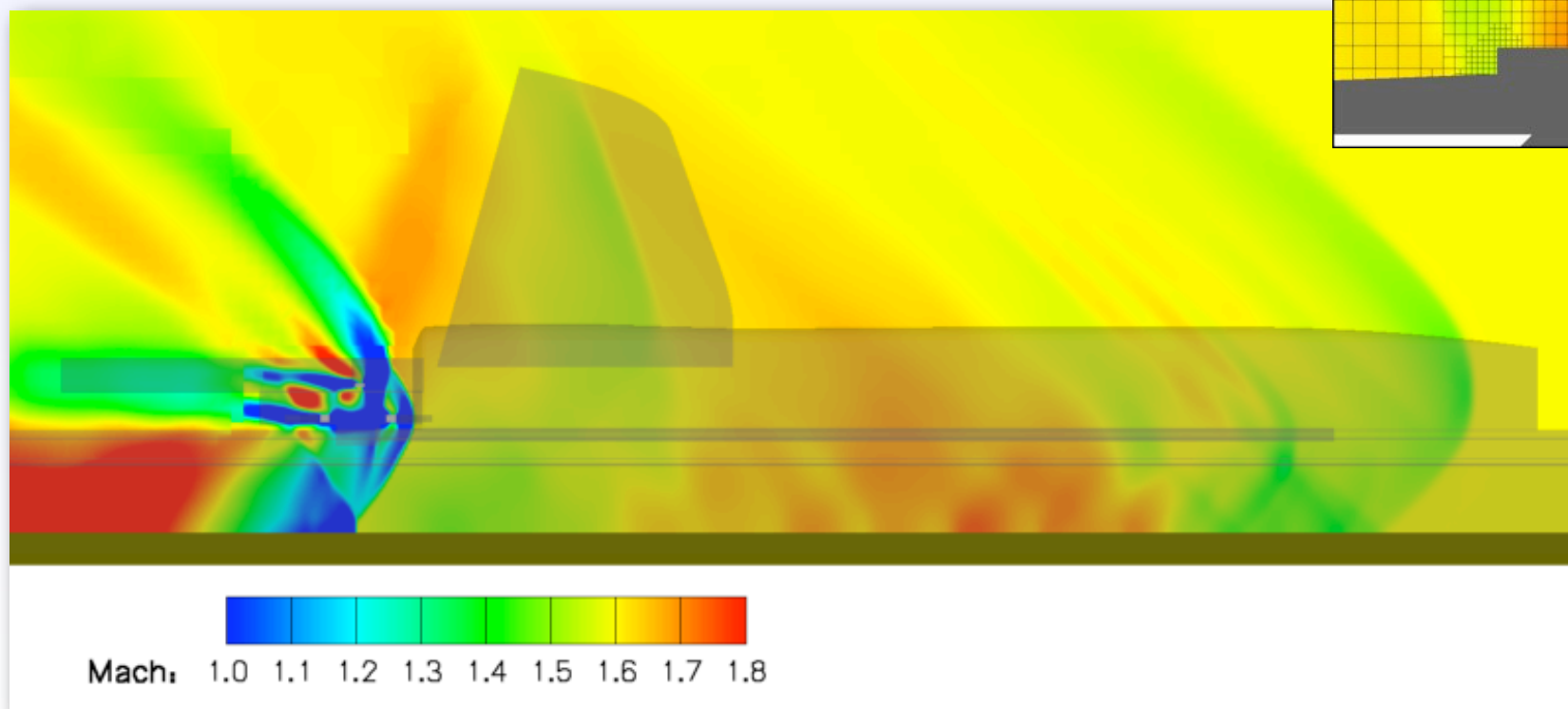




# Rocket-Sled Test

## ◆ Typical Euler solutions on full geometry

- test wing
- sled fairing and outrigger
- rails
- track bed

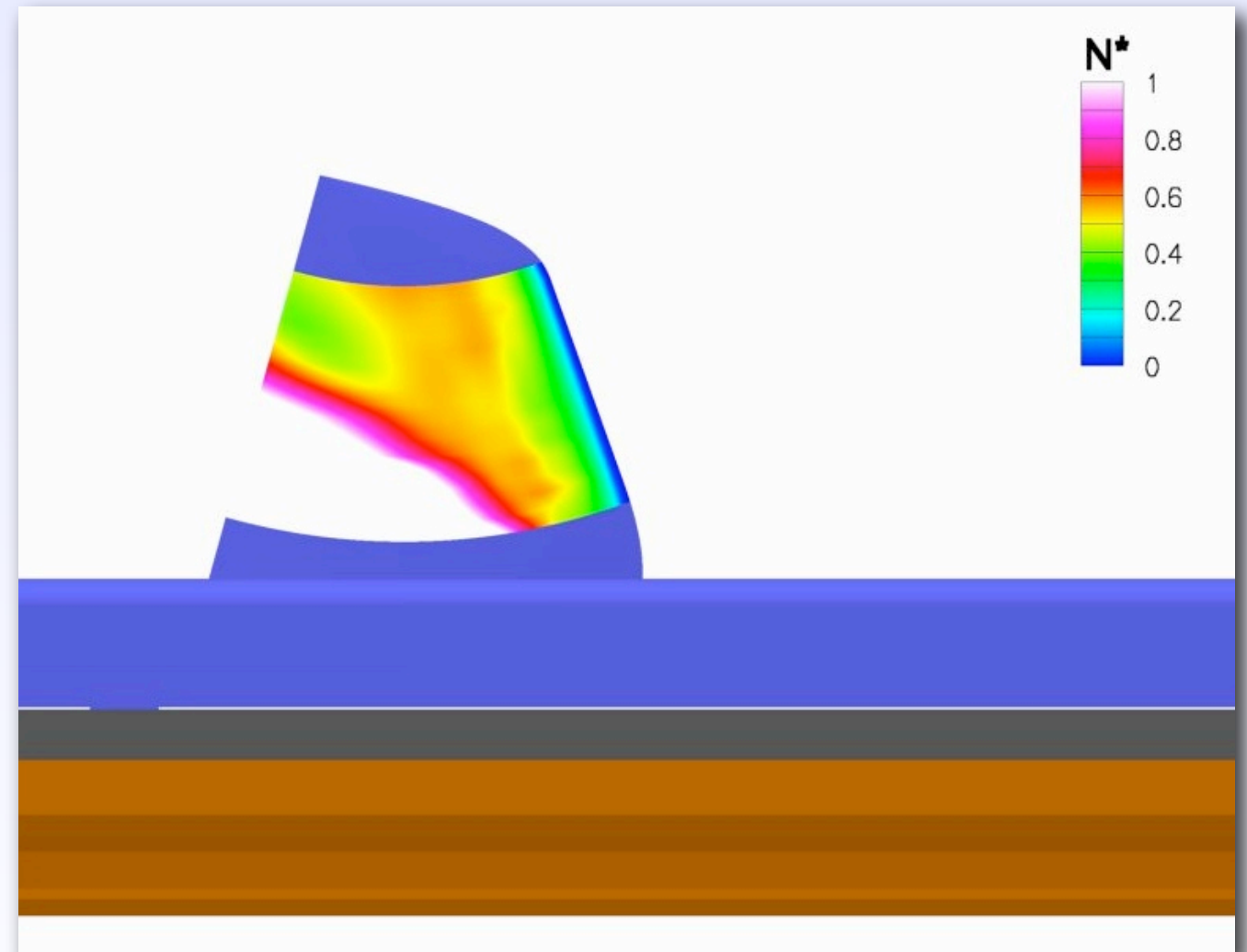


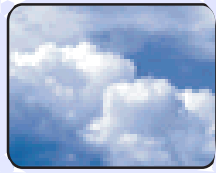




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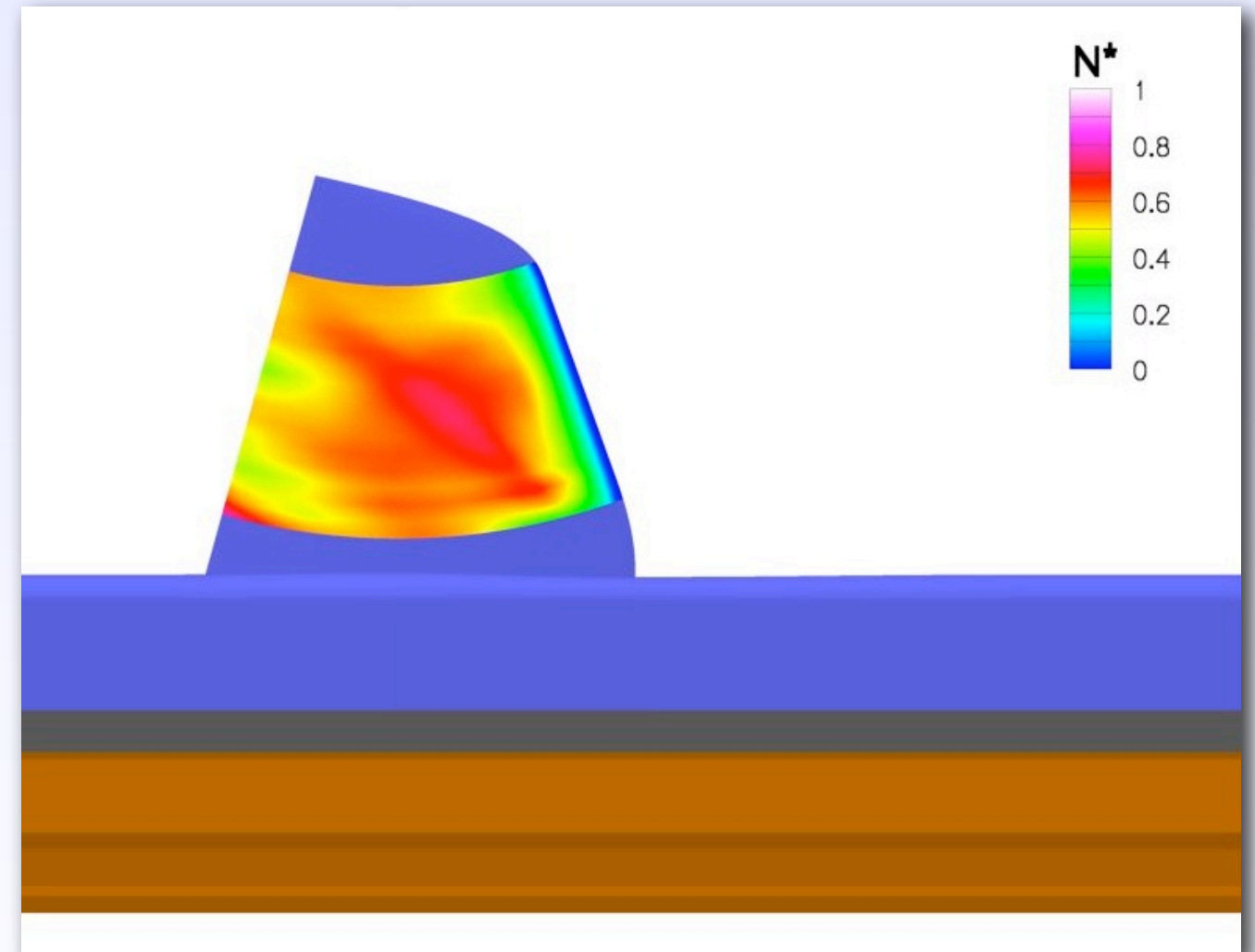
- ◆ Baseline sled design still not ideal for laminar flow
- ◆ Increase in boundary-layer crossflow compared symmetry plane
  - similar to half-wing
  - nose shock and other pressure disturbances bounce around

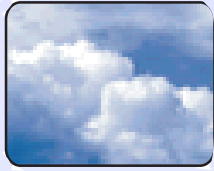




# Rocket-Sled Test

- ◆ Sled fairing modified to lower maximum N-factor
  - Cart3D coupled with transition design code
  - nonlinear simplex optimization
- ◆ Airfoil modifications also effective

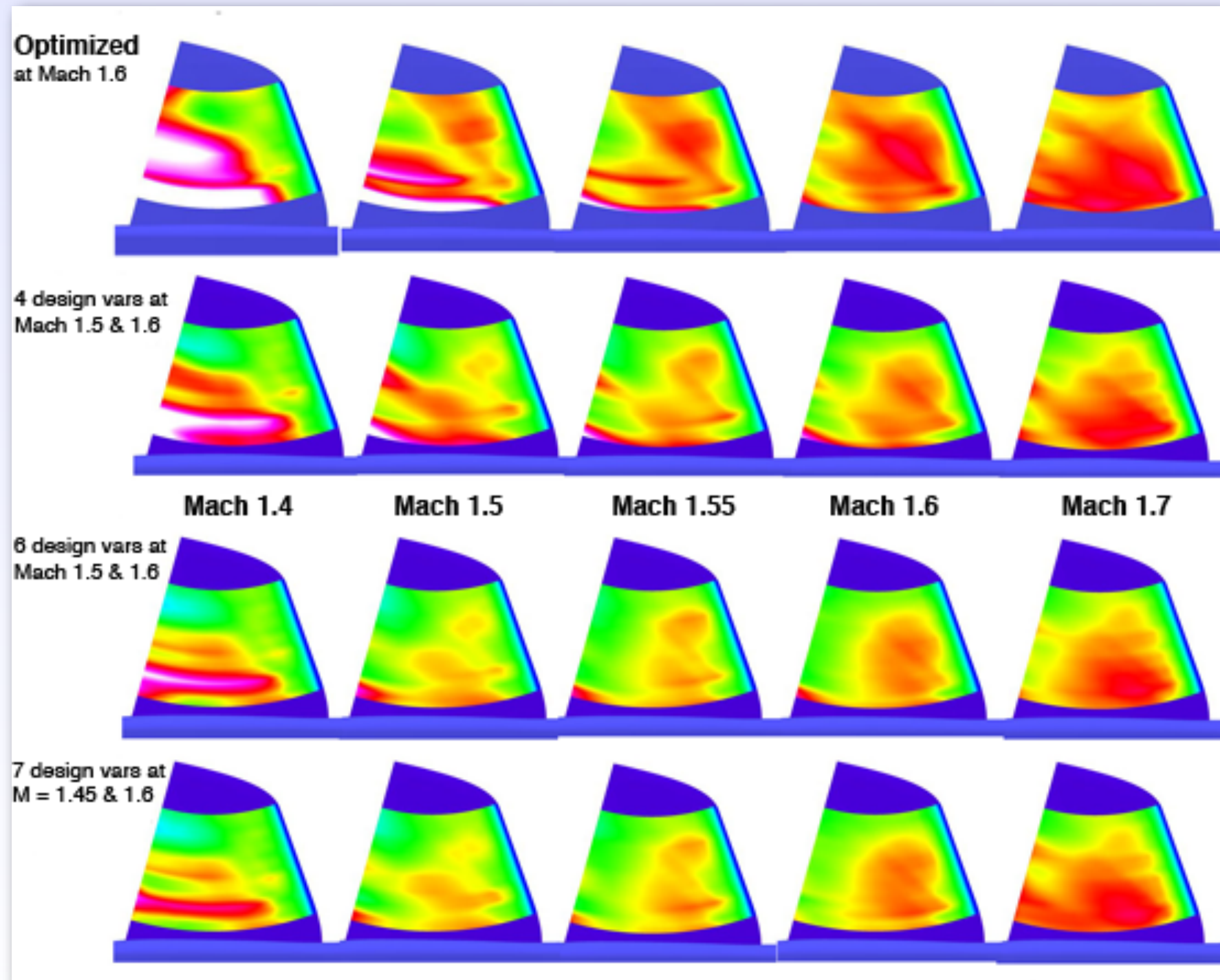




# Rocket-Sled Test

## Dual-point optimizations

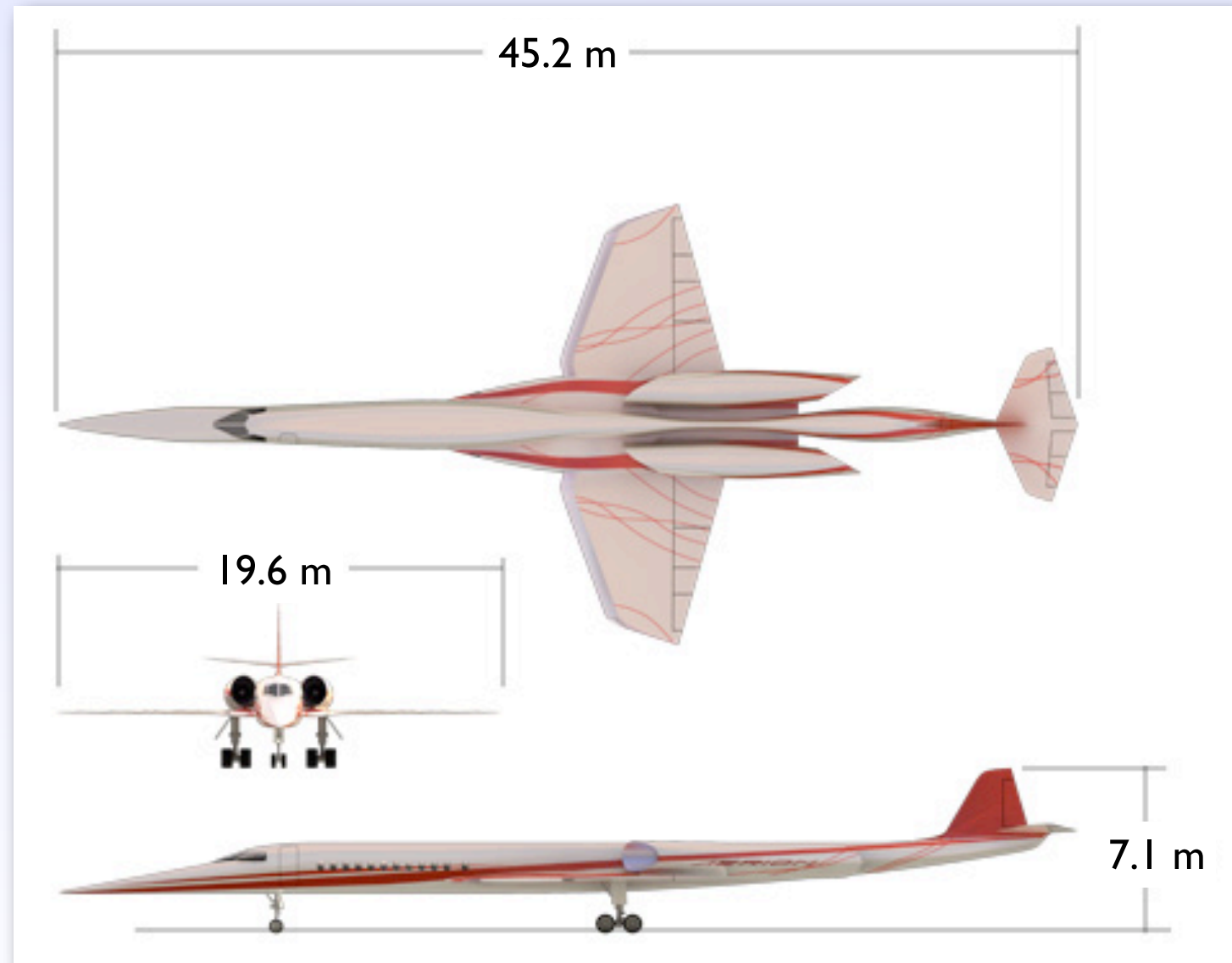
- ✦ Objective is linear combination of laminar extent at two Mach numbers
- ✦ Widens useful Mach number range
- ✦ Allows more design variables



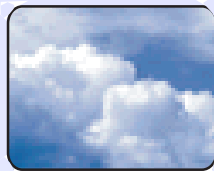


# Full Aircraft Aerodynamic Optimization

- ♦ Two-part optimization
  - inviscid full-configuration drag minimization
  - viscous wing/body drag minimization
- ♦ Due to supersonic cones of influence







# Geometry Generation

## ♦ CAD-based

- labor-intensive, time-consuming
- geometric instead of aircraft design parameters
  - control points
  - trimming surfaces
- not practical for trade studies, optimization

## ♦ Perturbation method

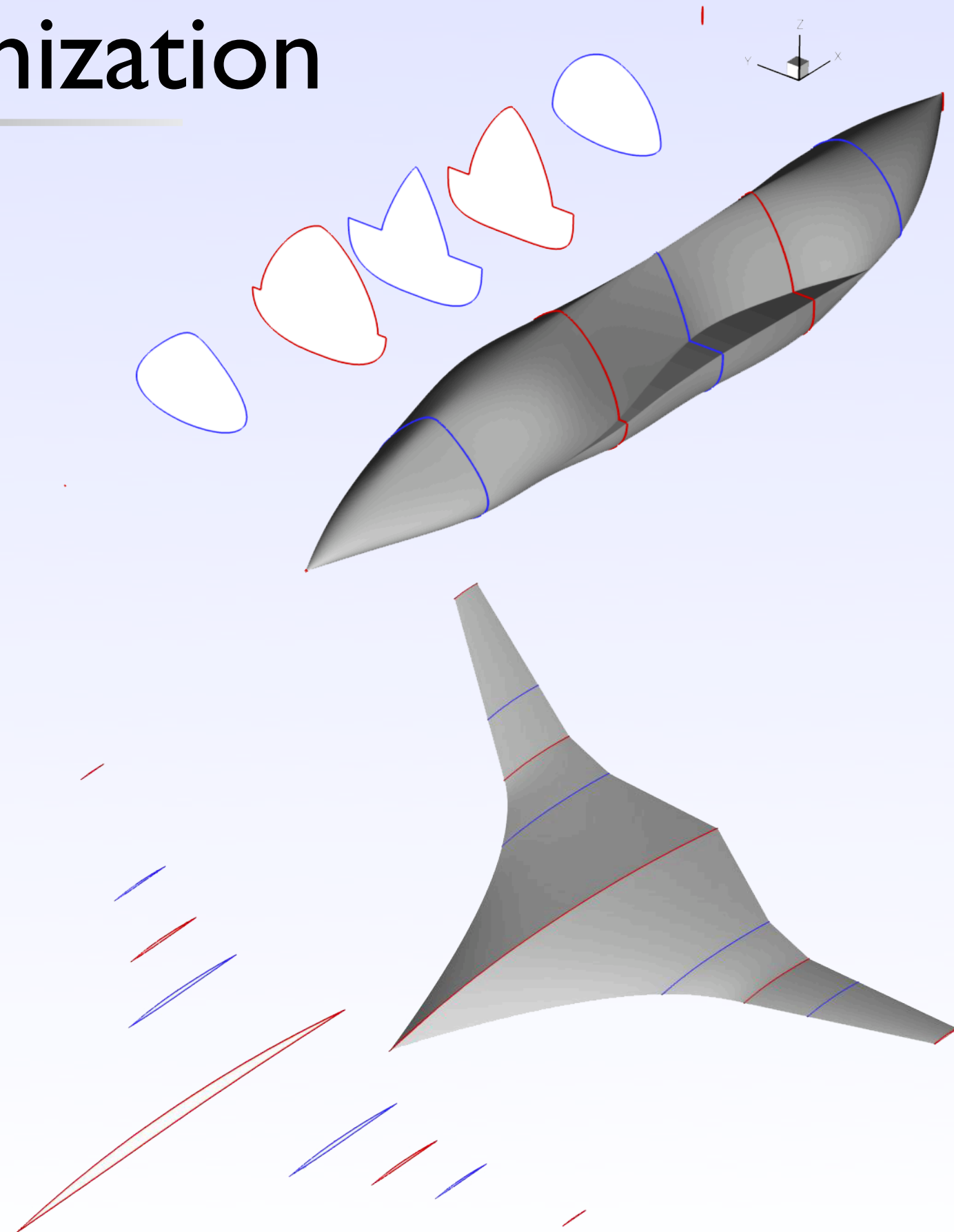
- modifications to a baseline geometry model
- powerful when making small local changes
- impractical when making gross changes

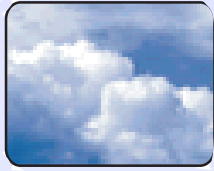
## ♦ Parametric geometry



# Geometry Generation for Optimization

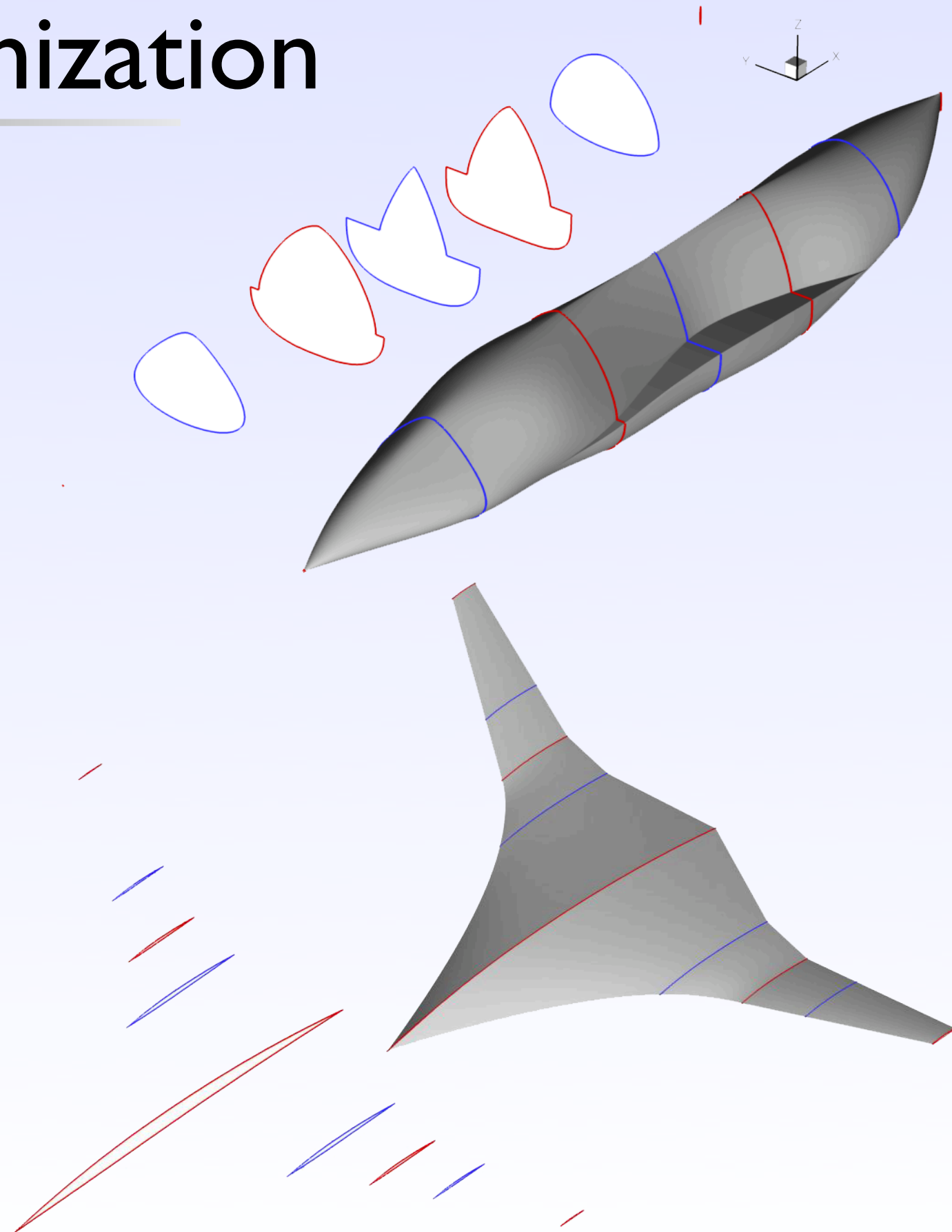
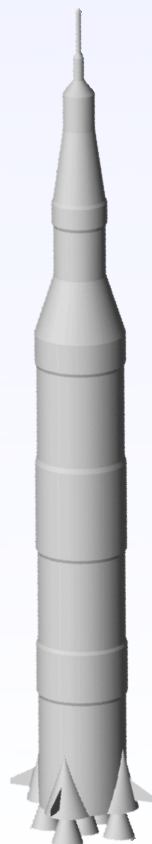
- ◆ Rapid Aerospace Geometry Engine (RAGE)
- ◆ Axially splined bodies
  - fuselages
  - nacelles
- ◆ Lofted stack of airfoils
  - wings
  - tails
  - pylons





# Geometry Generation for Optimization

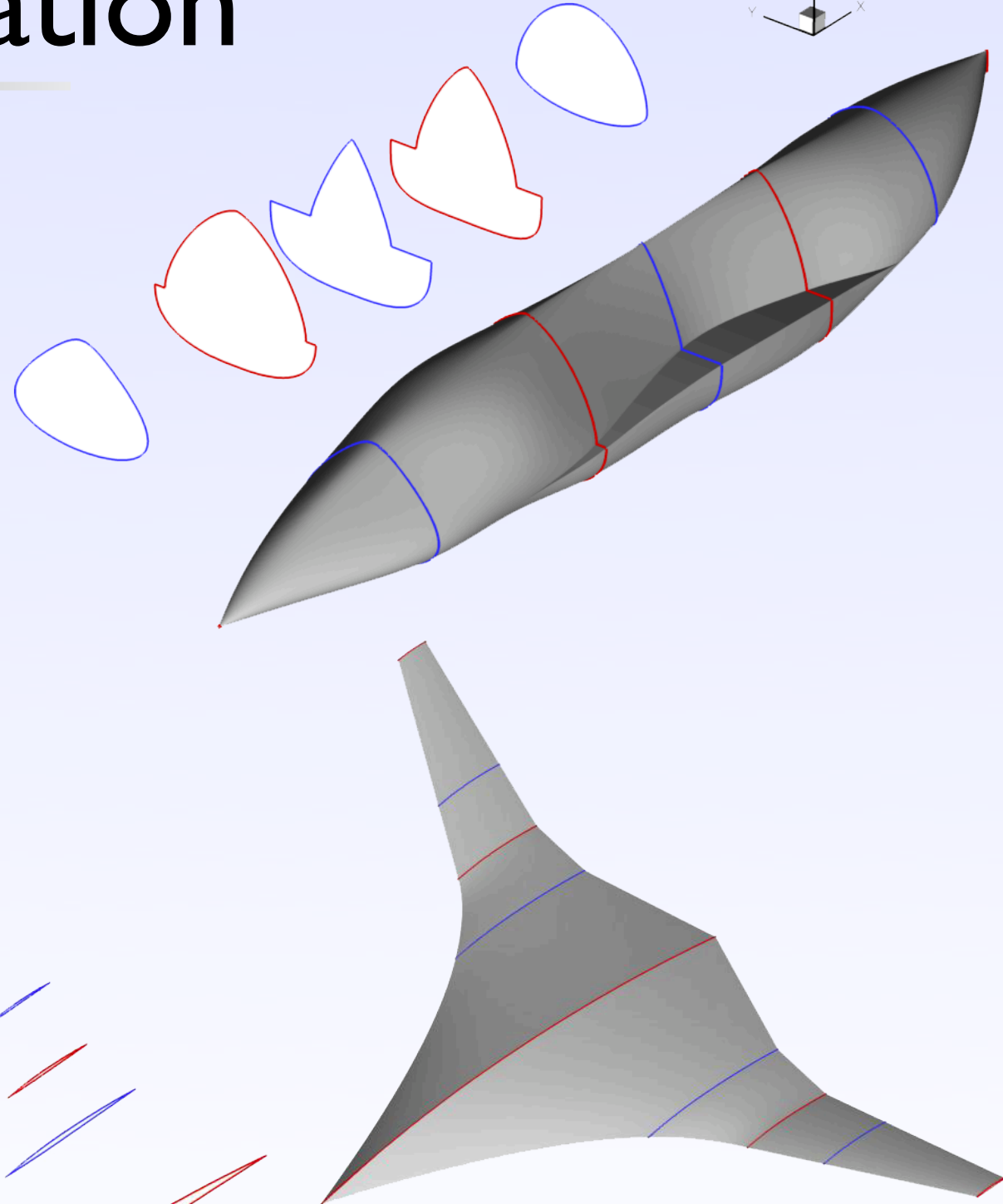
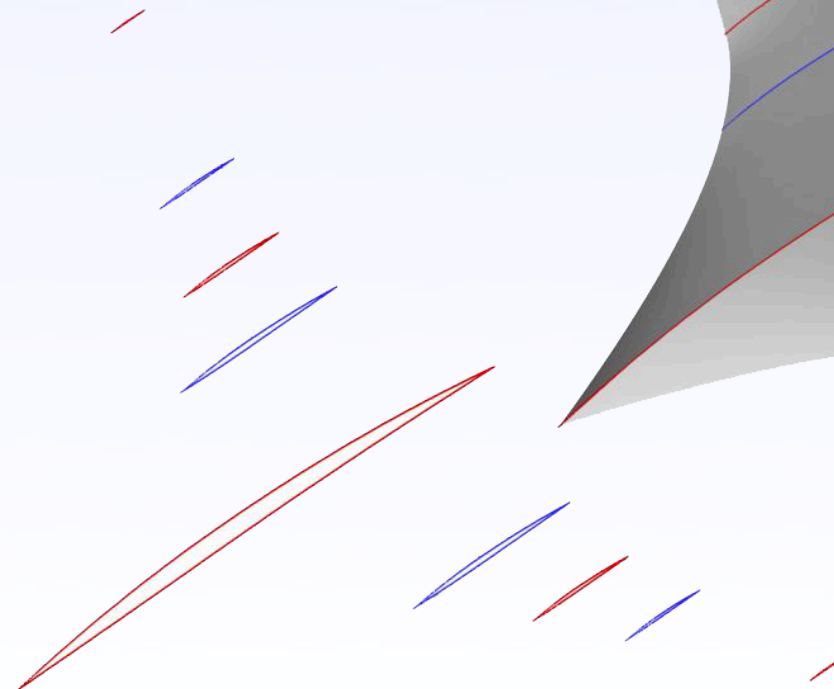
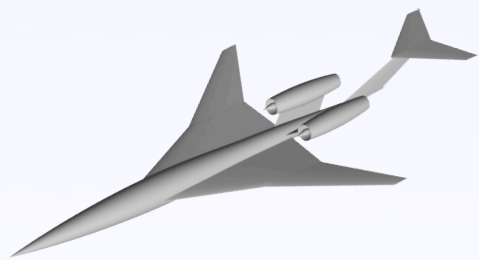
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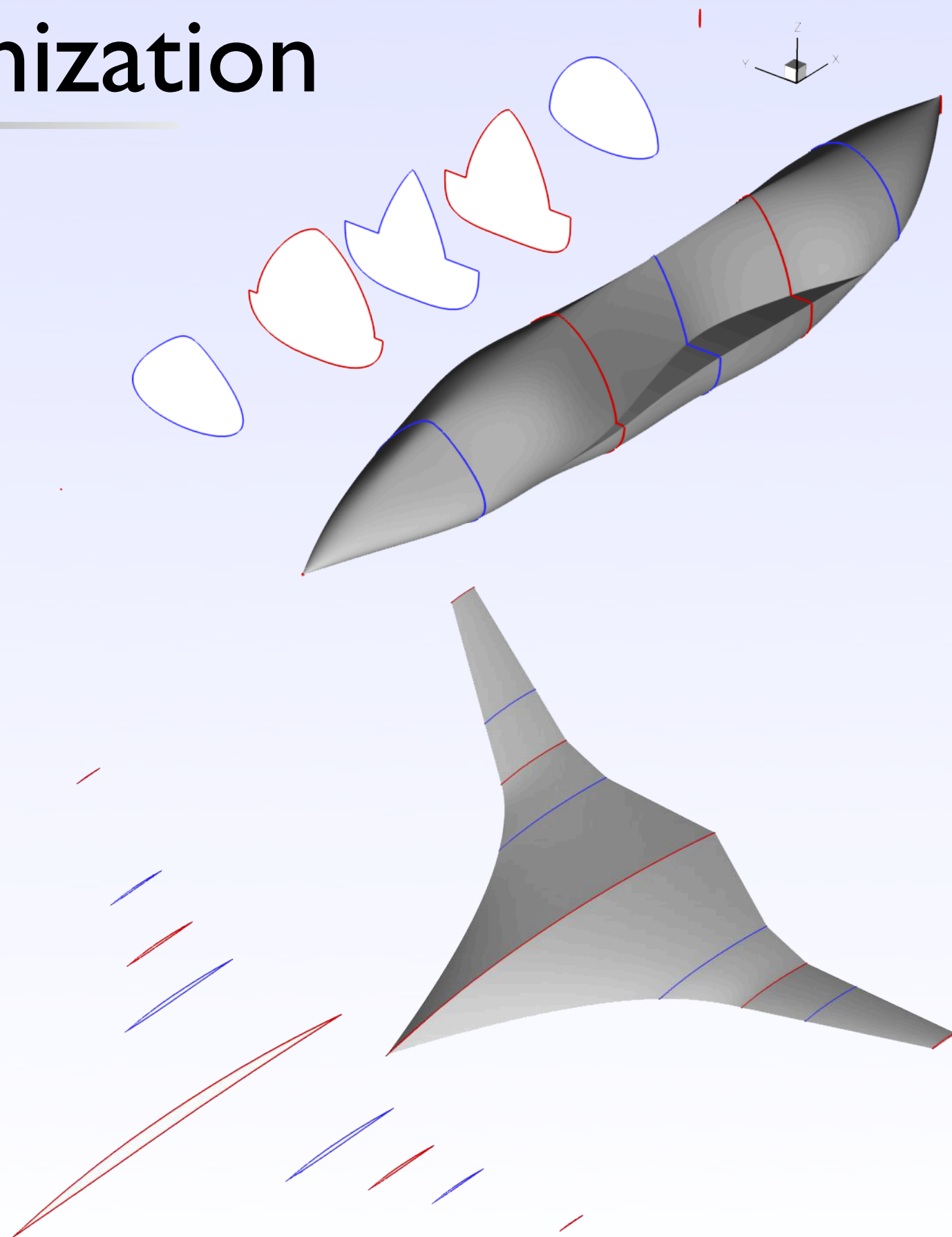
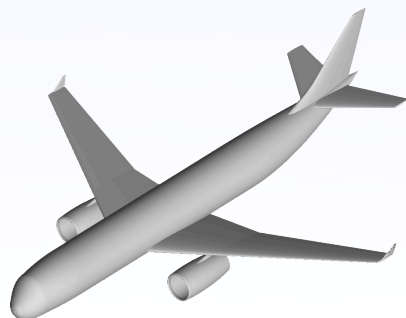
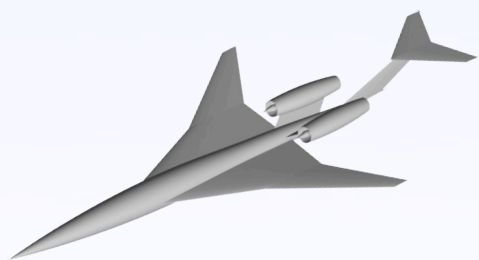


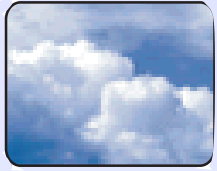




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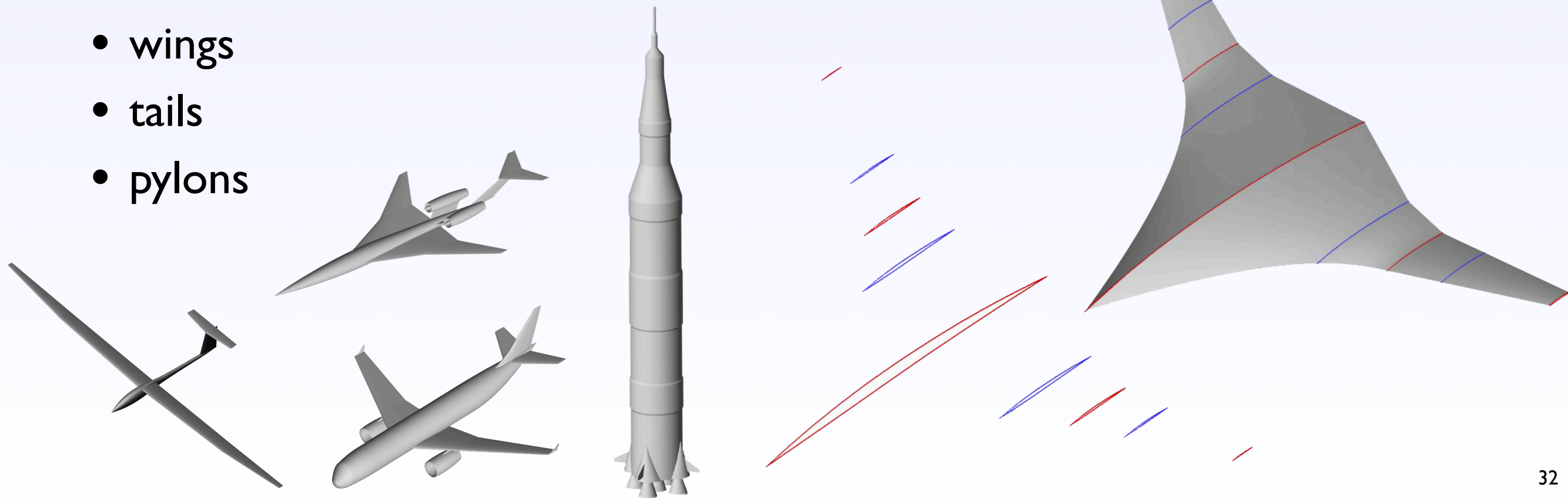
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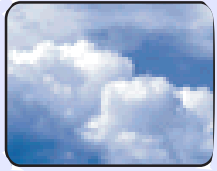




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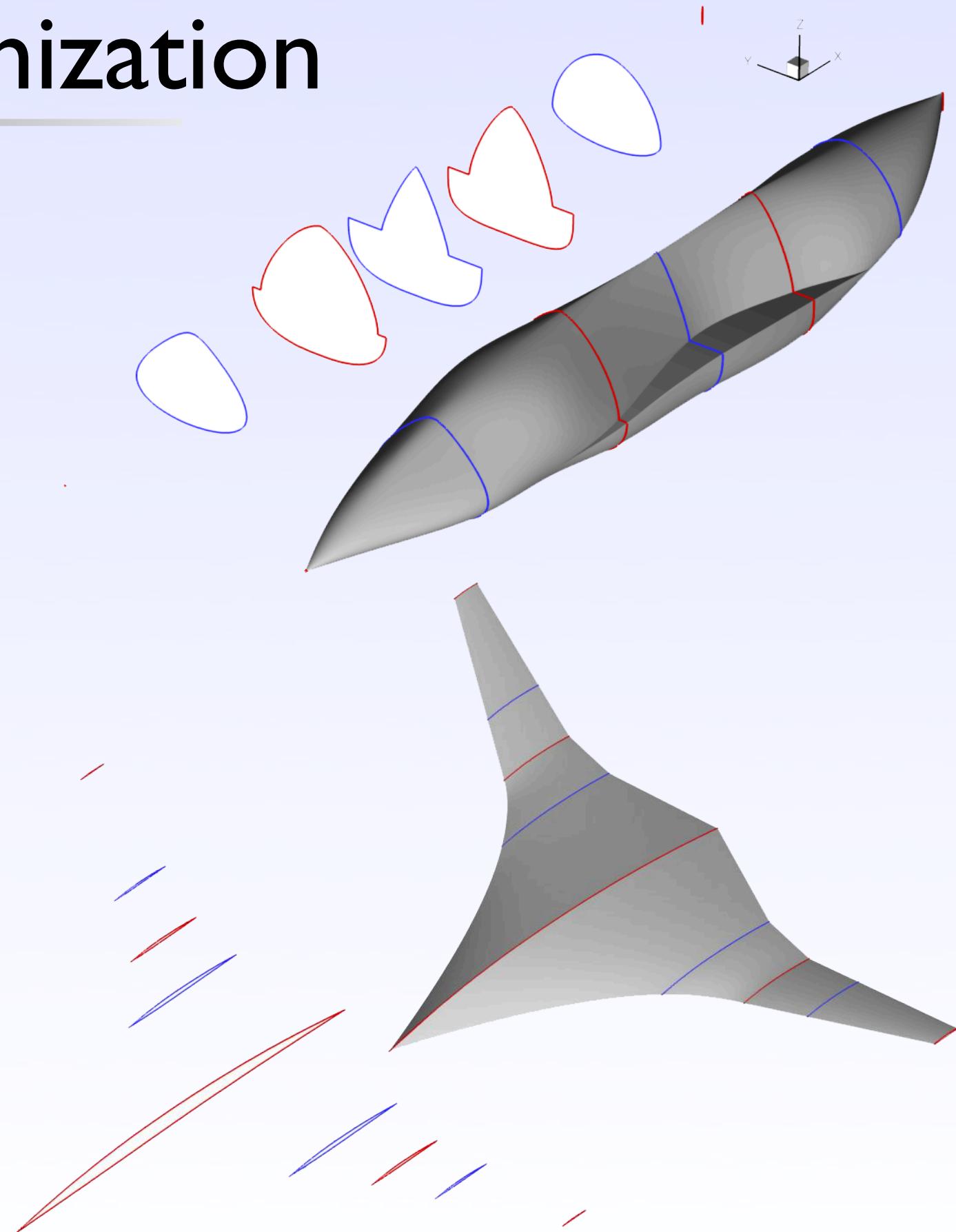
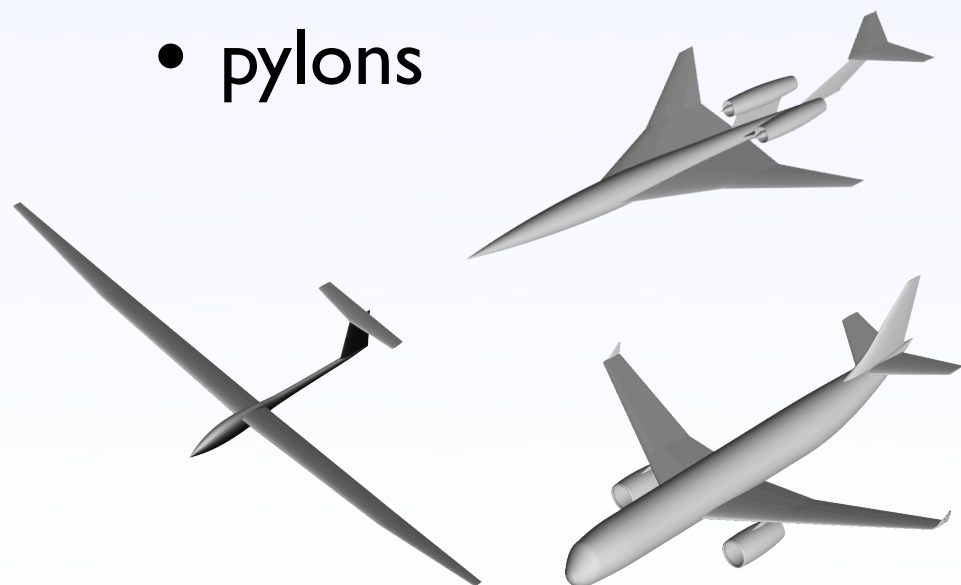
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# Full Aircraft Aerodynamic Optimization

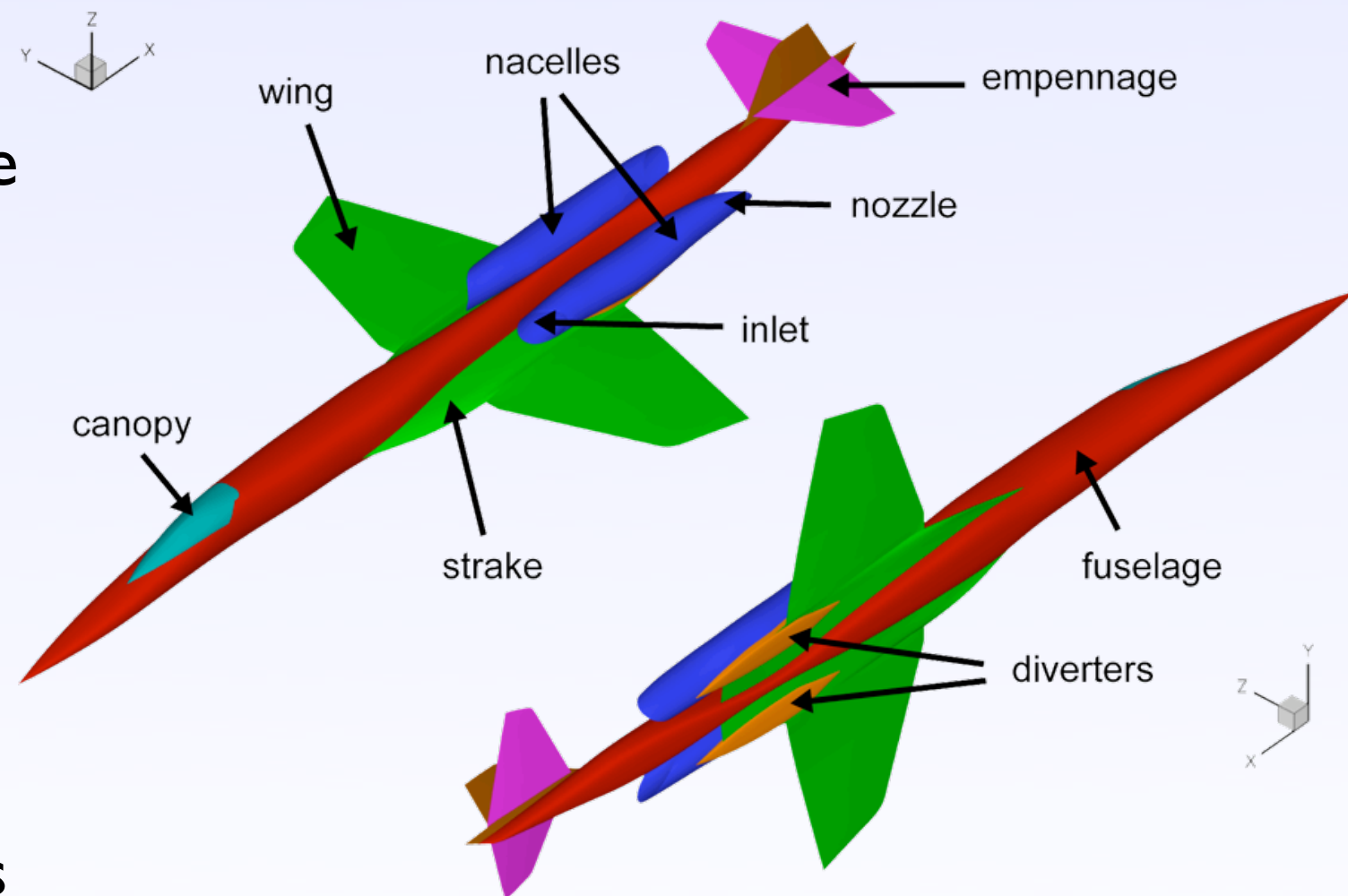
## Inviscid Drag Minimization of Full Configuration

### ♦ Geometry

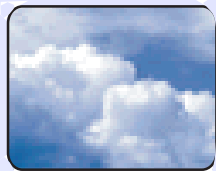
- wing, strake, fuselage, canopy, inlet, nozzle, diverter, empennage
- fix portions of fuselage, strake and wing to maintain laminar flow

### ♦ Optimization

- nonlinear simplex
- geometric constraints
- inlet and nozzle flow constraints
- lift constrained

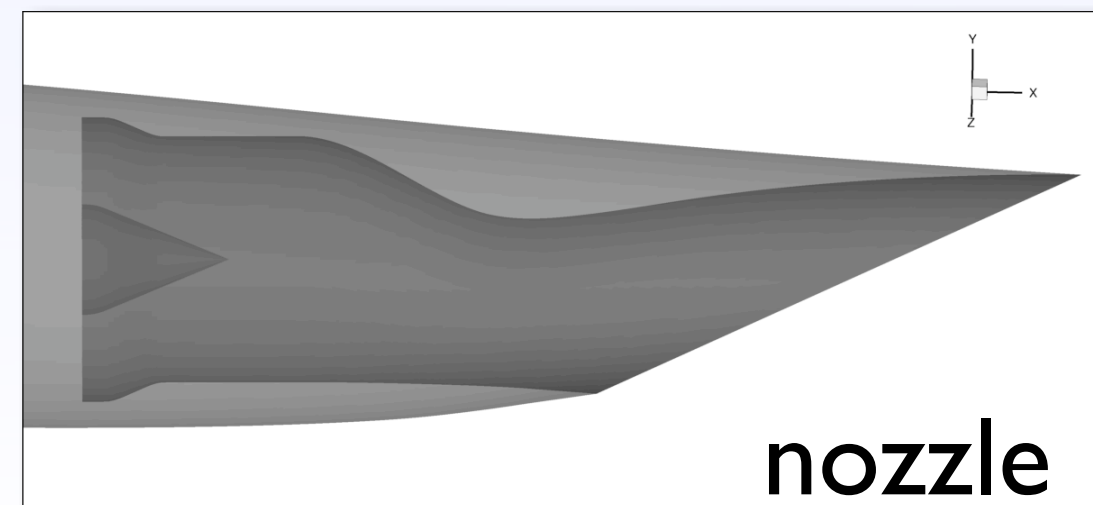
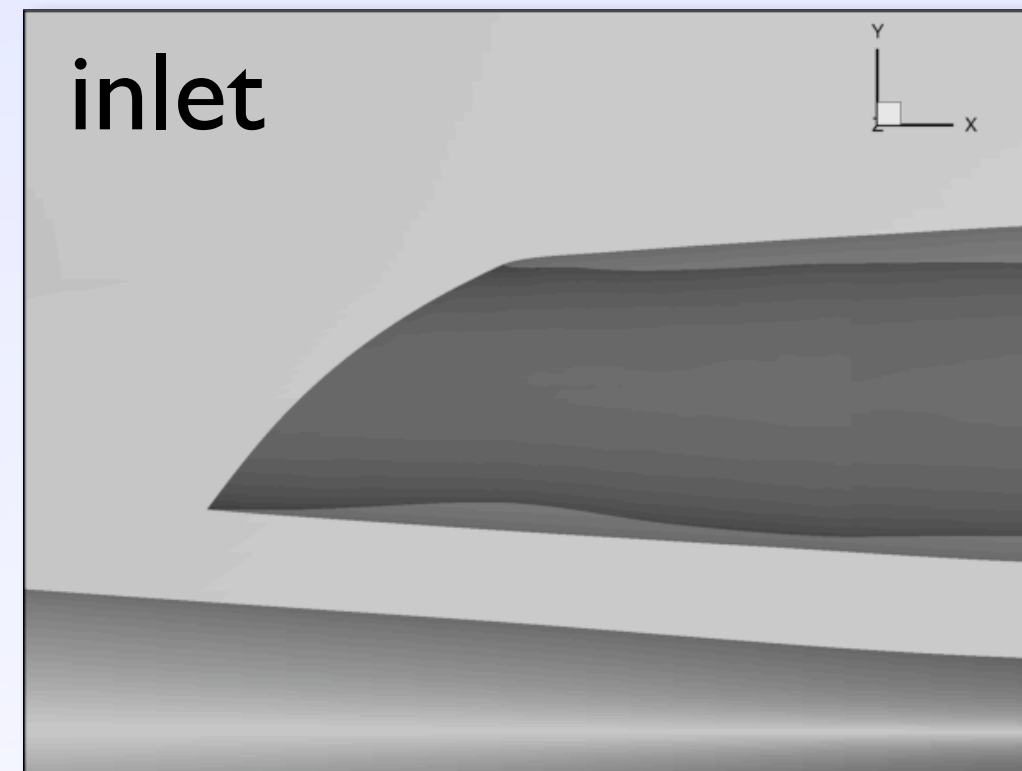
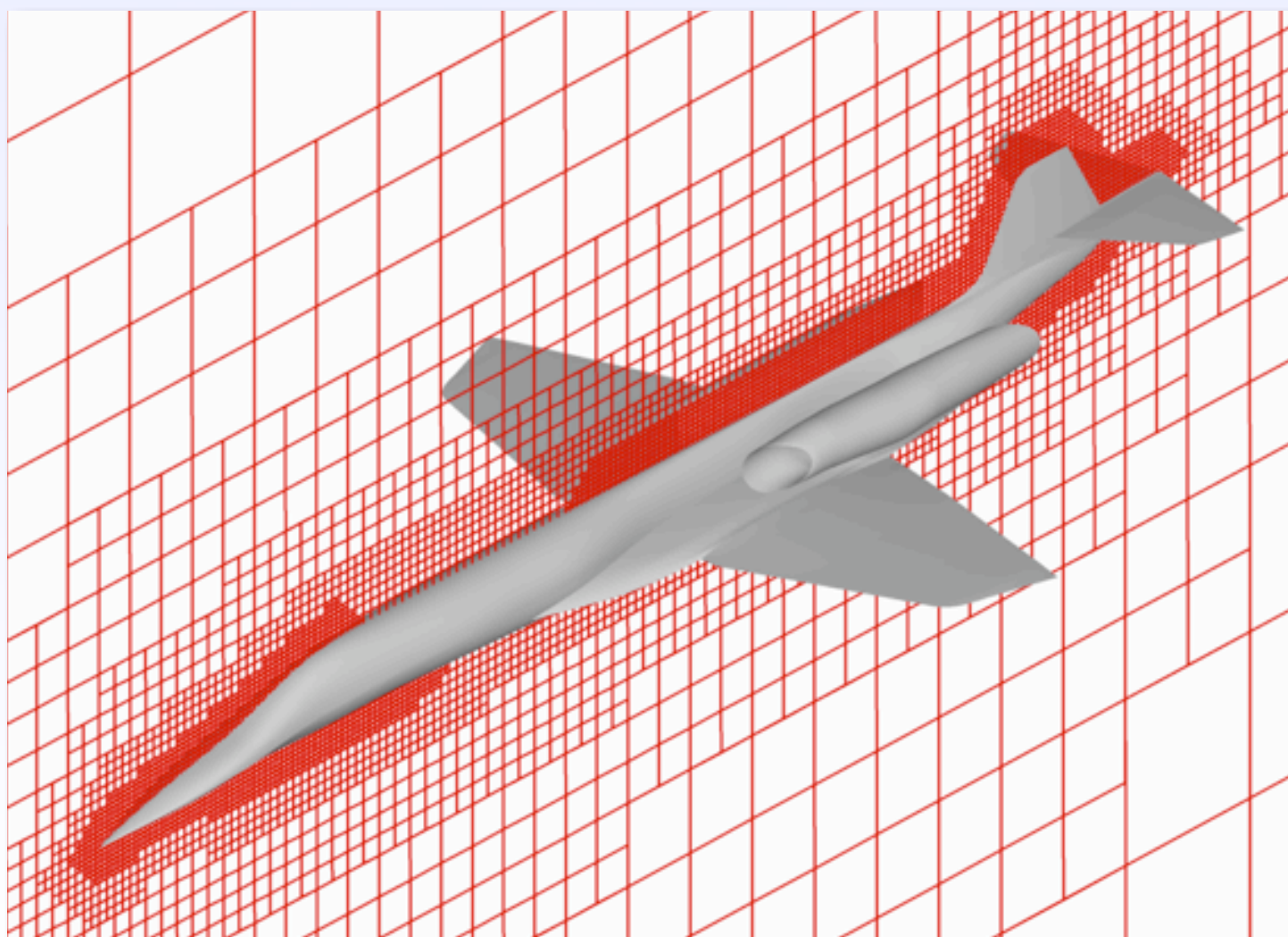






# Inviscid Optimization

- ♦ Cart3D inviscid Euler solver
- ♦ Minimize drag and maximize thrust
- ♦ Off-design constraints

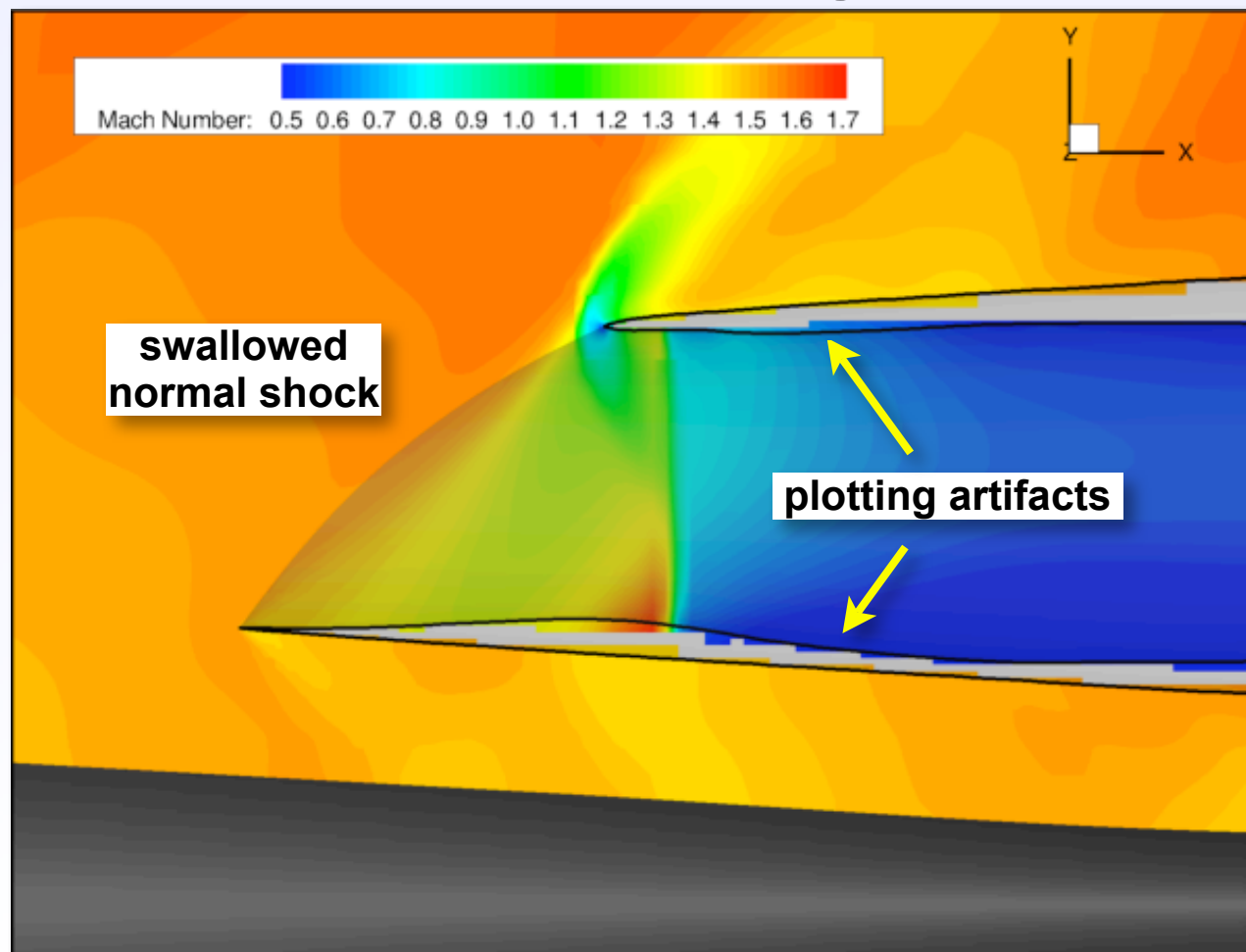




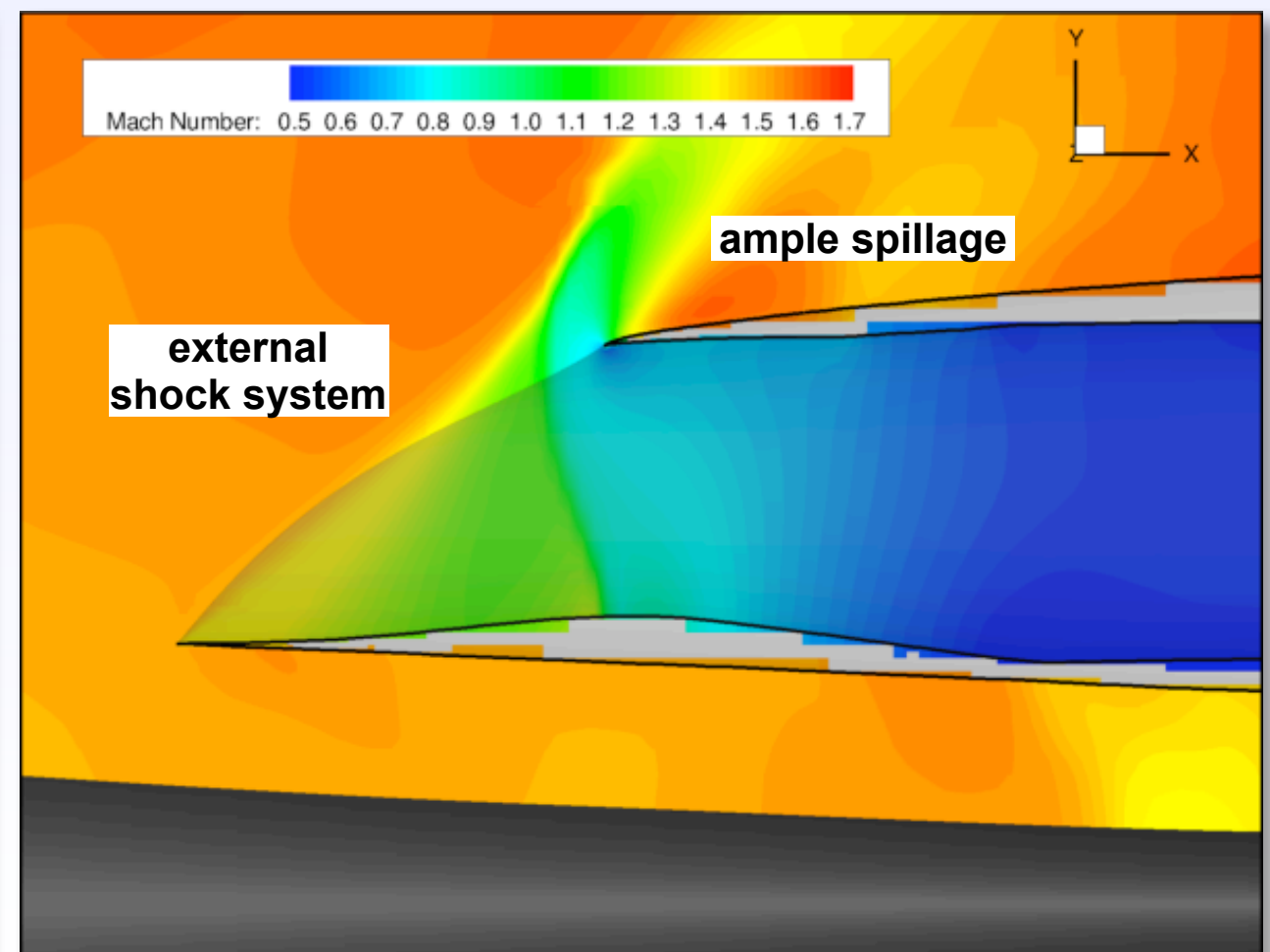
# Inlet Optimization at Mach 1.5

- ◆ 4.6% increase in pressure recovery
- ◆ 4.8% increase in aircraft drag
- ◆ Stable inlet throughout mission profile
- ◆ 5.8% decrease in objective function

**Initial geometry by  
“stream tracing”**



**Optimized Geometry**

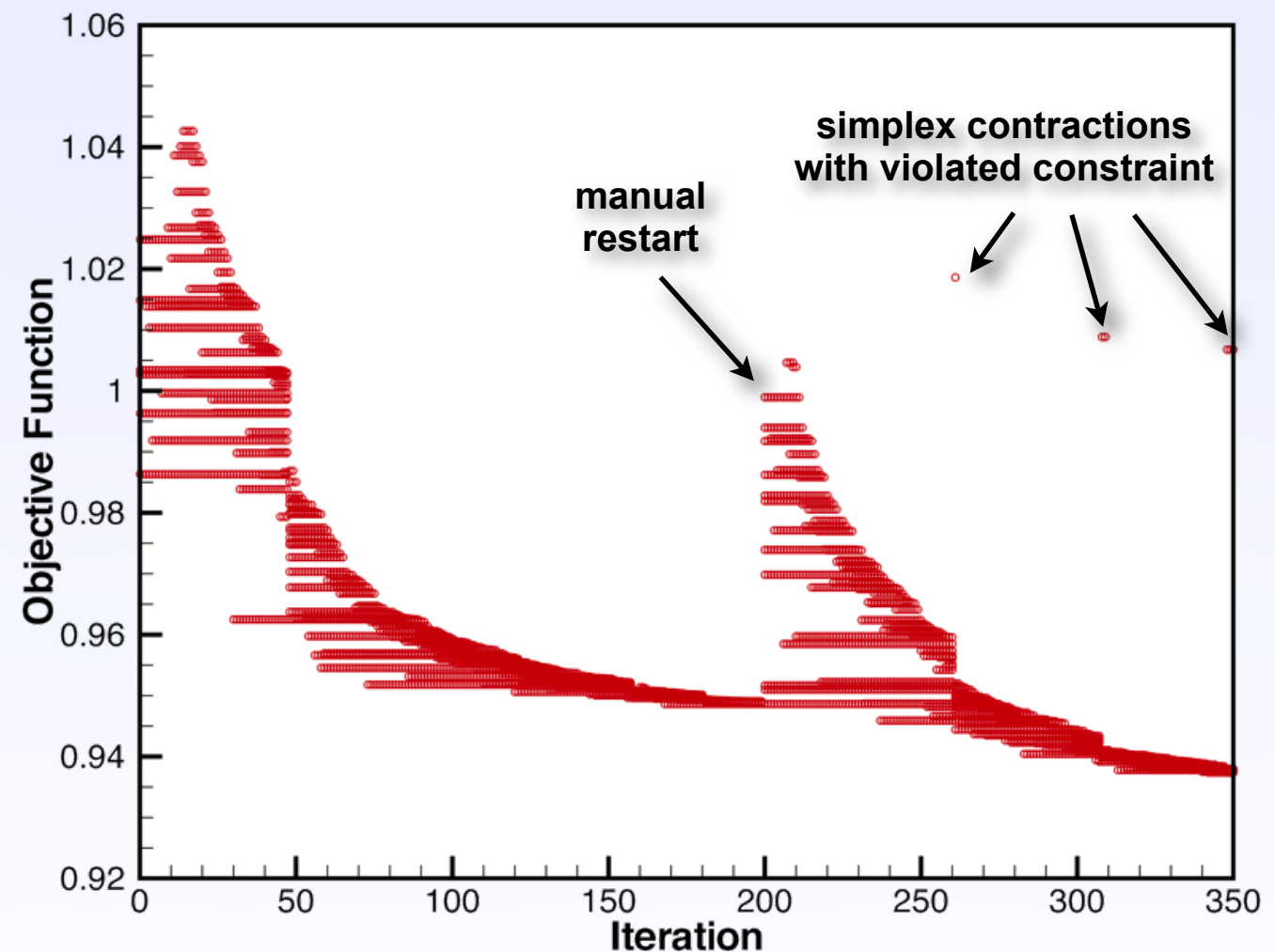




# Inlet Optimization Details

- ♦ Minimize weighted sum of aircraft drag and pressure recovery at Mach 1.5
- ♦ Constrain inlet lip Mach number to force ample spillage region at Mach 1.5 and Mach 1.6
- ♦ Constrain lift coefficient
- ♦ Vary all geometric parameters plus angle of attack
  - 100 distinct design variables
  - 15-20 at a time

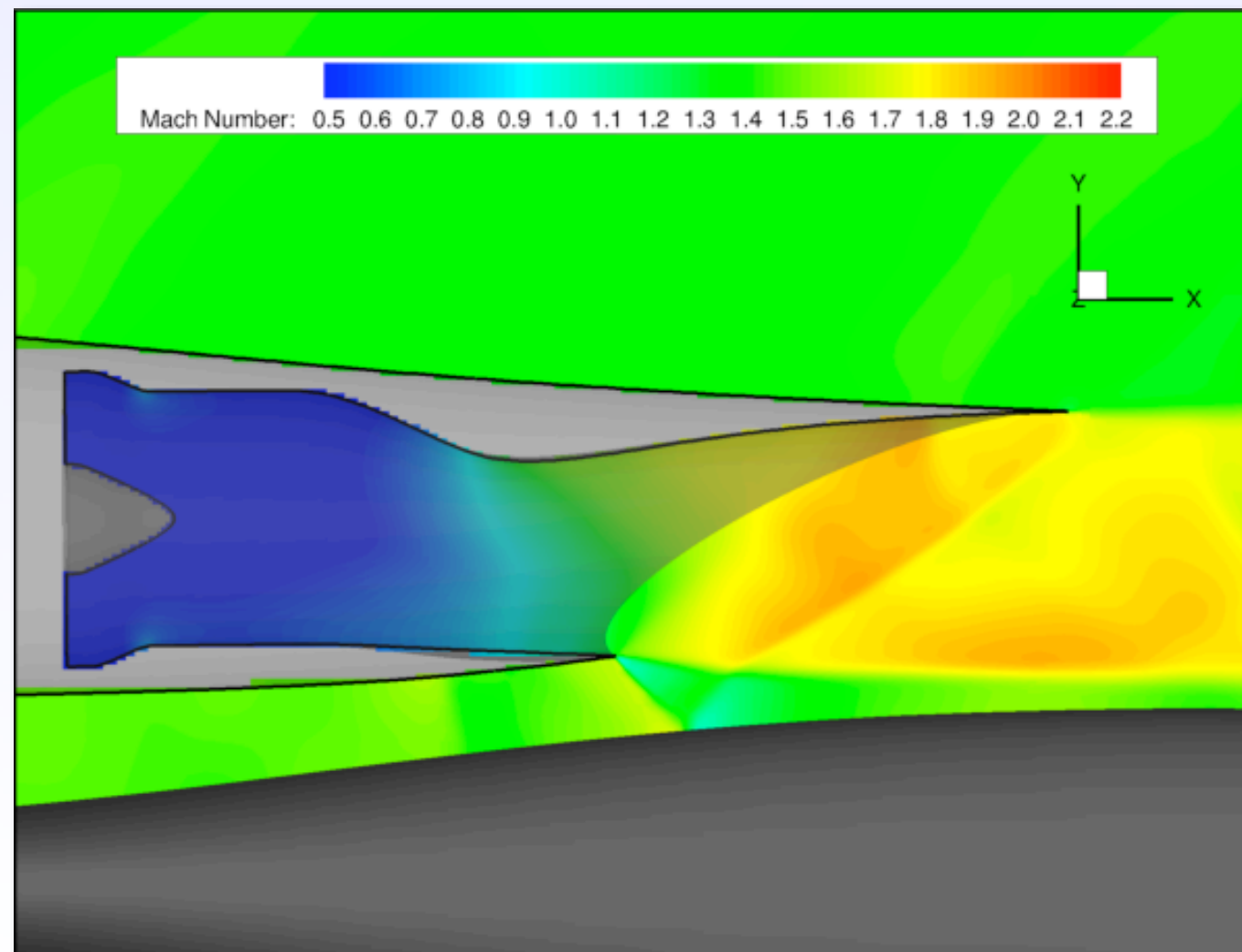
**constrained Nelder-Mead  
nonlinear simplex method**



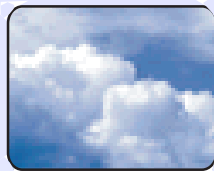


# Nozzle Optimization

- ◆ Similar optimization techniques as inlet design
- ◆ 10% thrust improvement
- ◆ Less than 1% increase in airframe wave drag
- ◆ Currently also using takeoff condition constraint







# Full Aircraft Aerodynamic Optimization

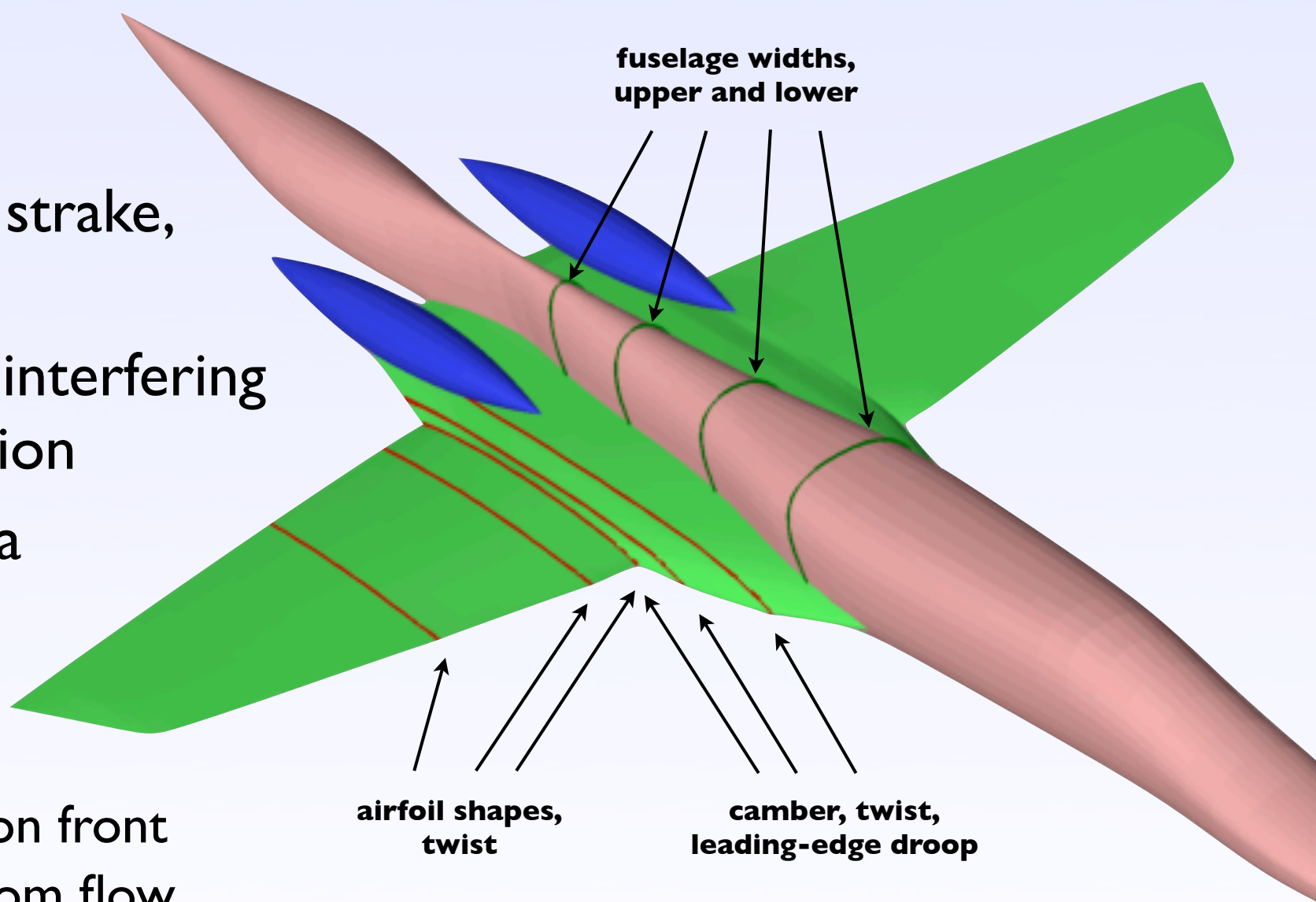
## Optimization for Laminar Extent

### ◆ Geometry

- simplified nacelles, wing, strake, fuselage
- fix aft portions to avoid interfering with propulsion integration
- approximate canopy area

### ◆ Optimization

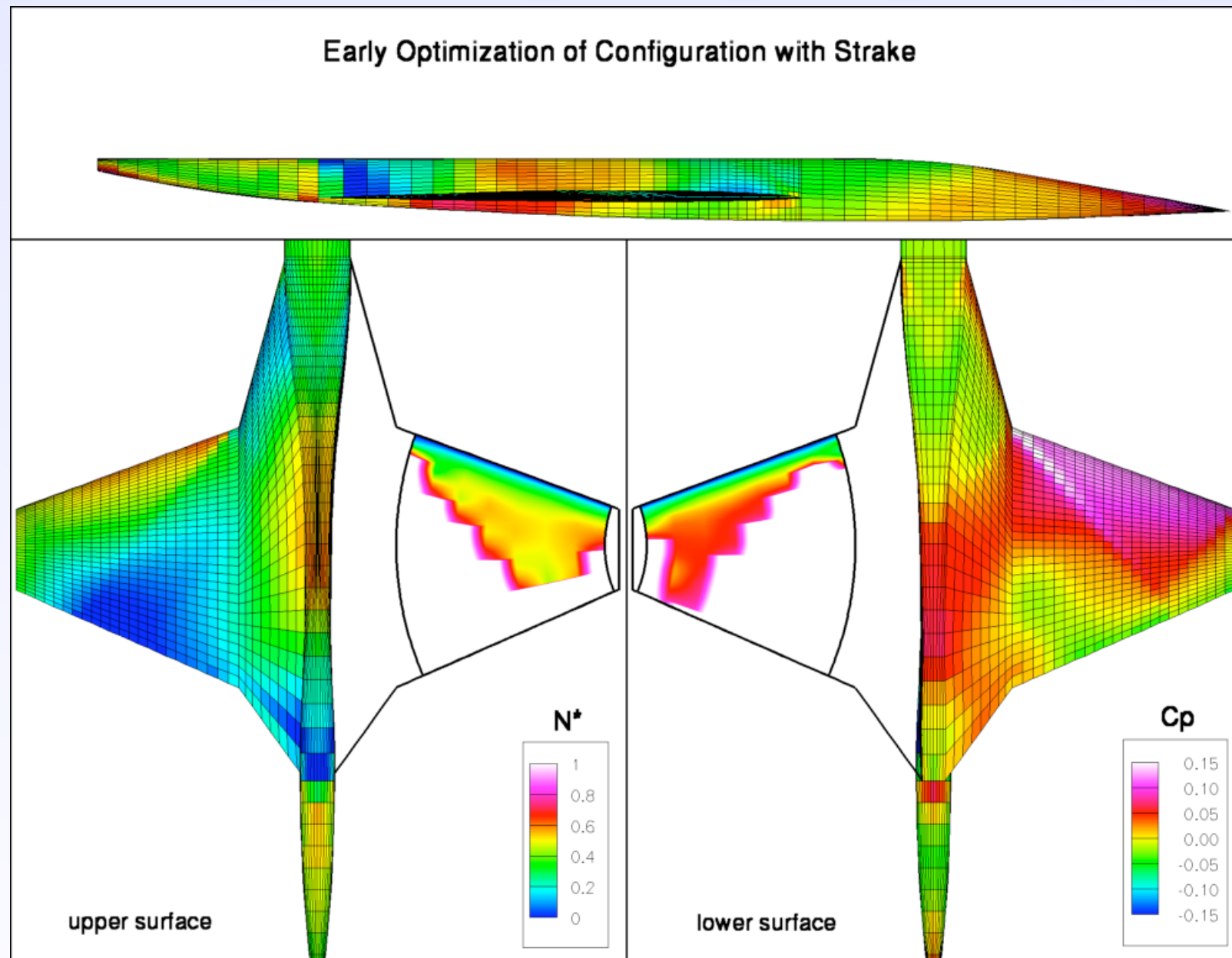
- genetic algorithm
  - erratic jumps in transition front
  - occasional bad points from flow solver
- geometric and lift constraints





# Viscous Optimization: Early Difficulties

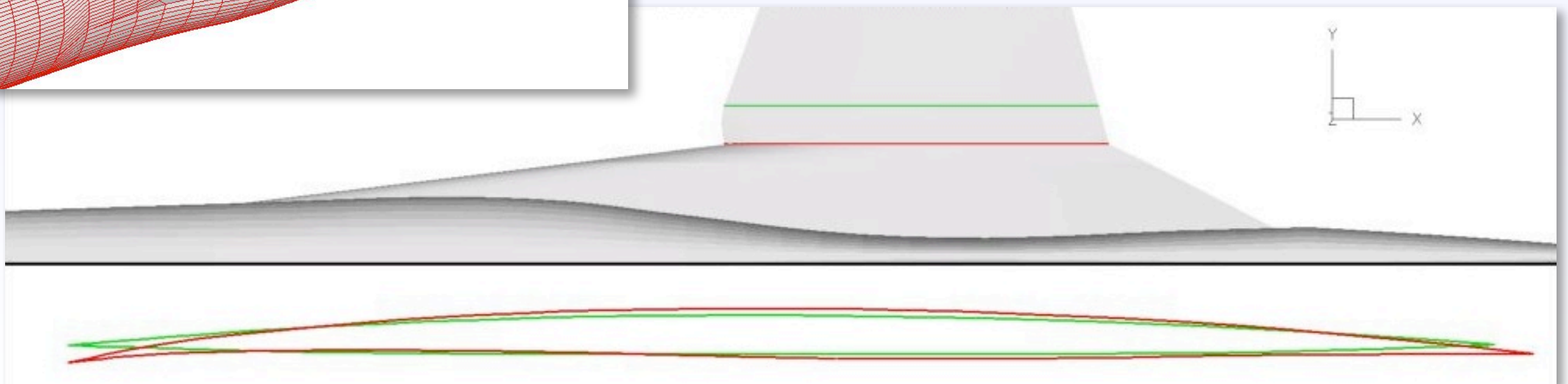
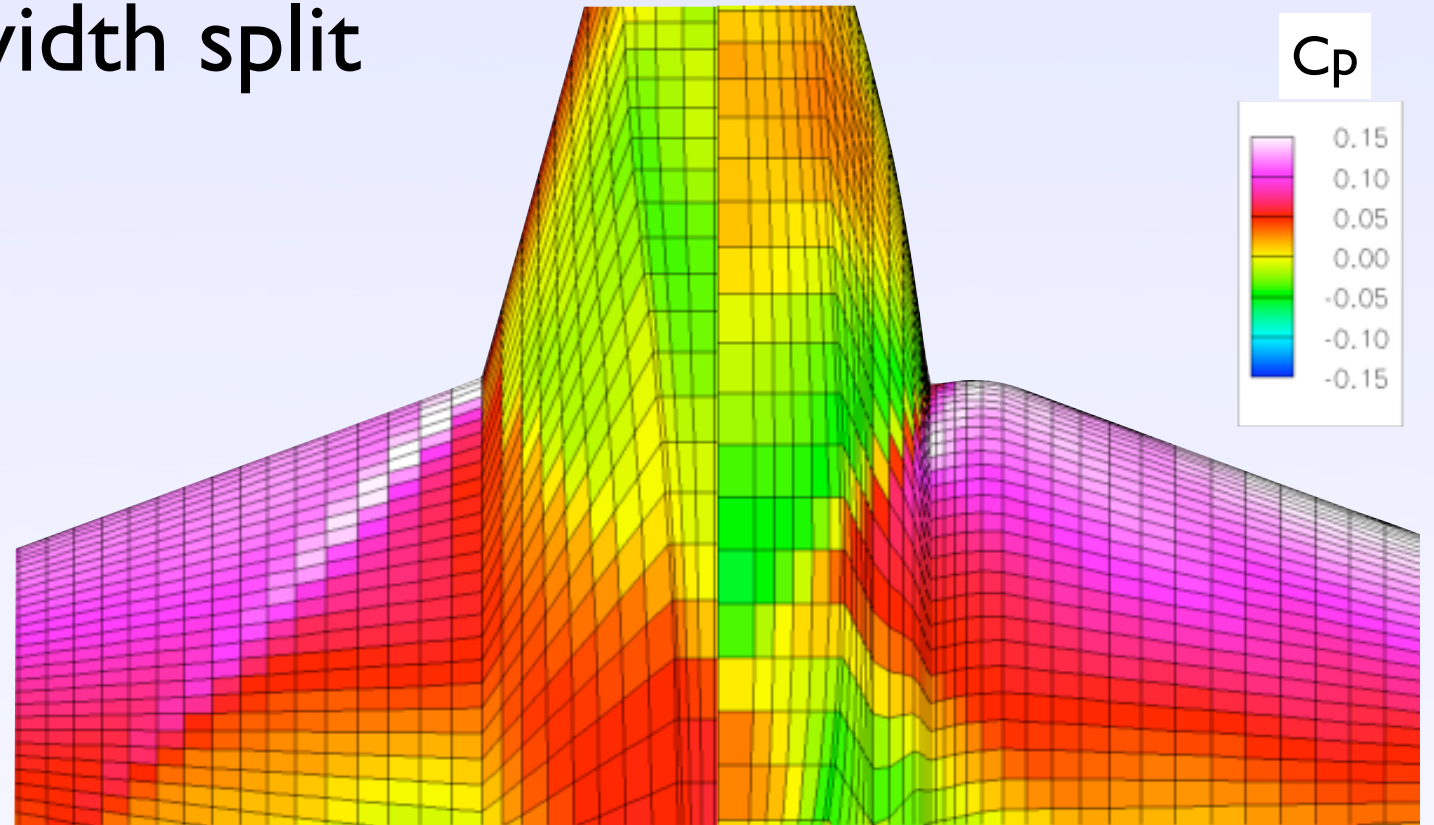
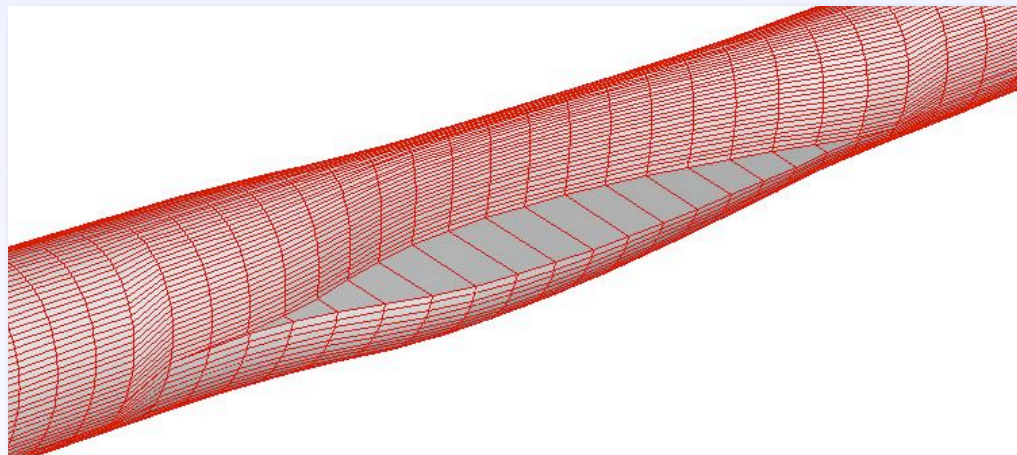
- ✦ White areas indicate turbulent flow
- ✦ Difficulties in obtaining adequate laminar flow due to addition of strake





# Viscous Optimization: Key Elements

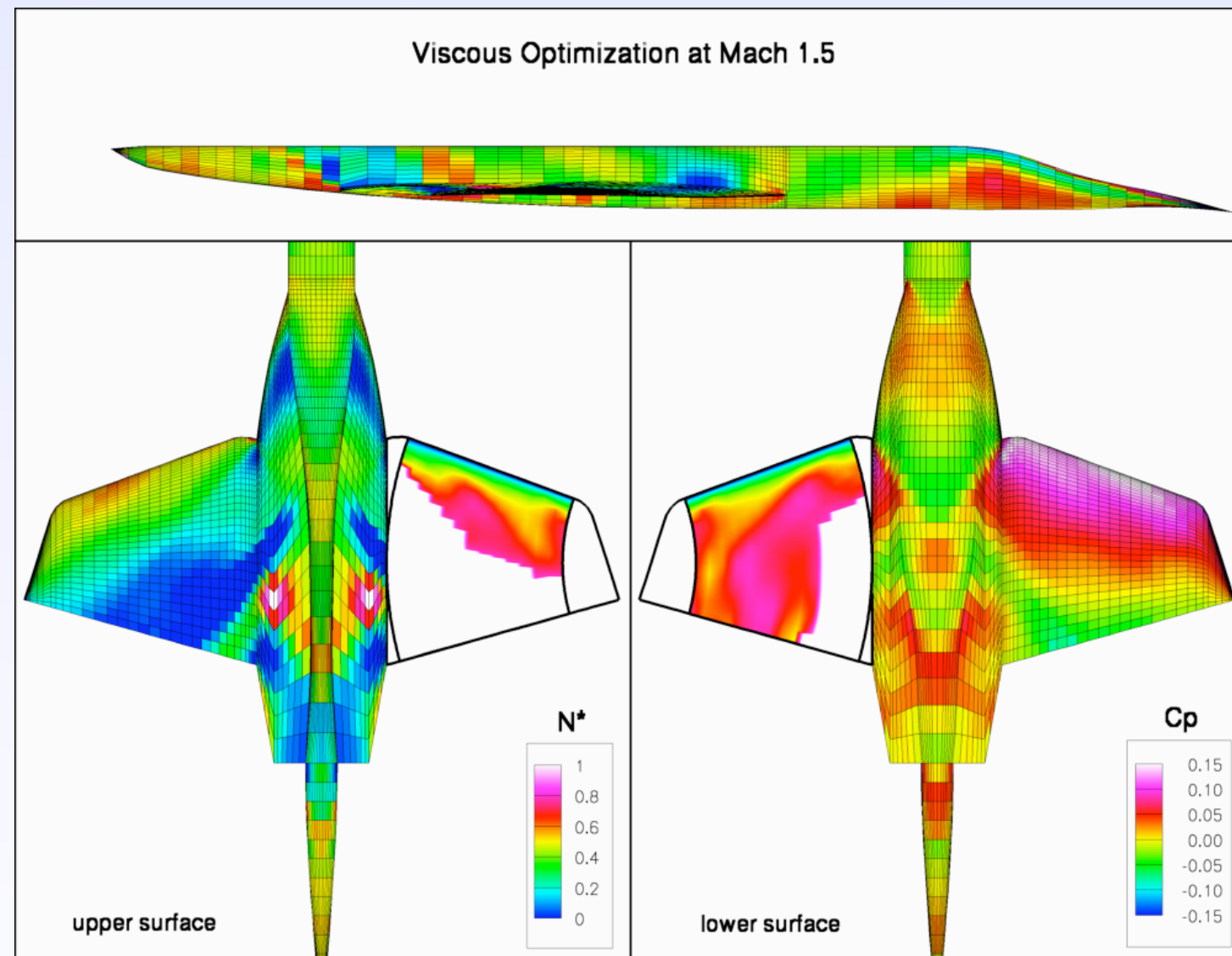
- ✦ Upper/lower fuselage width split
- ✦ Airfoil nose droop
- ✦ The notch





# Viscous Optimization: Typical Result

- ✦ Less than 100% laminar fraction due to wave drag trade
- ✦ Optimization “encouraged” to favor lower surface due to nacelle and spoiler placement







# Details of Optimization

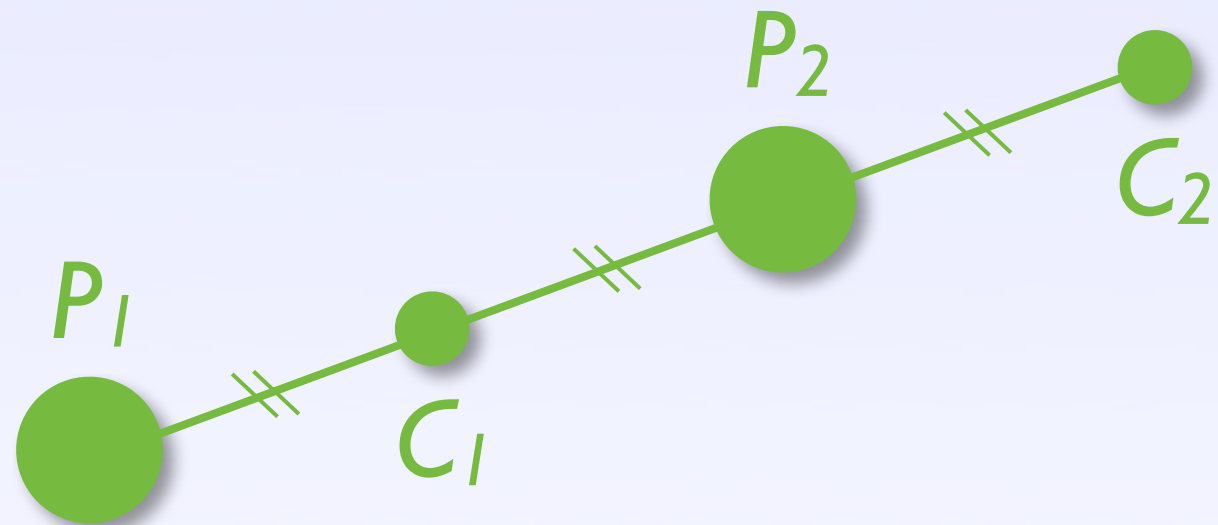
## ♦ Genetic Algorithm

- real-valued crossover, mutation
- least-squares Lagrange multiplier estimate for constraint penalty
- Highly parallelizable

♦ 10 to 25 variables

♦ 400 to 2000 population members

♦ A502 panel method used instead of Euler solver

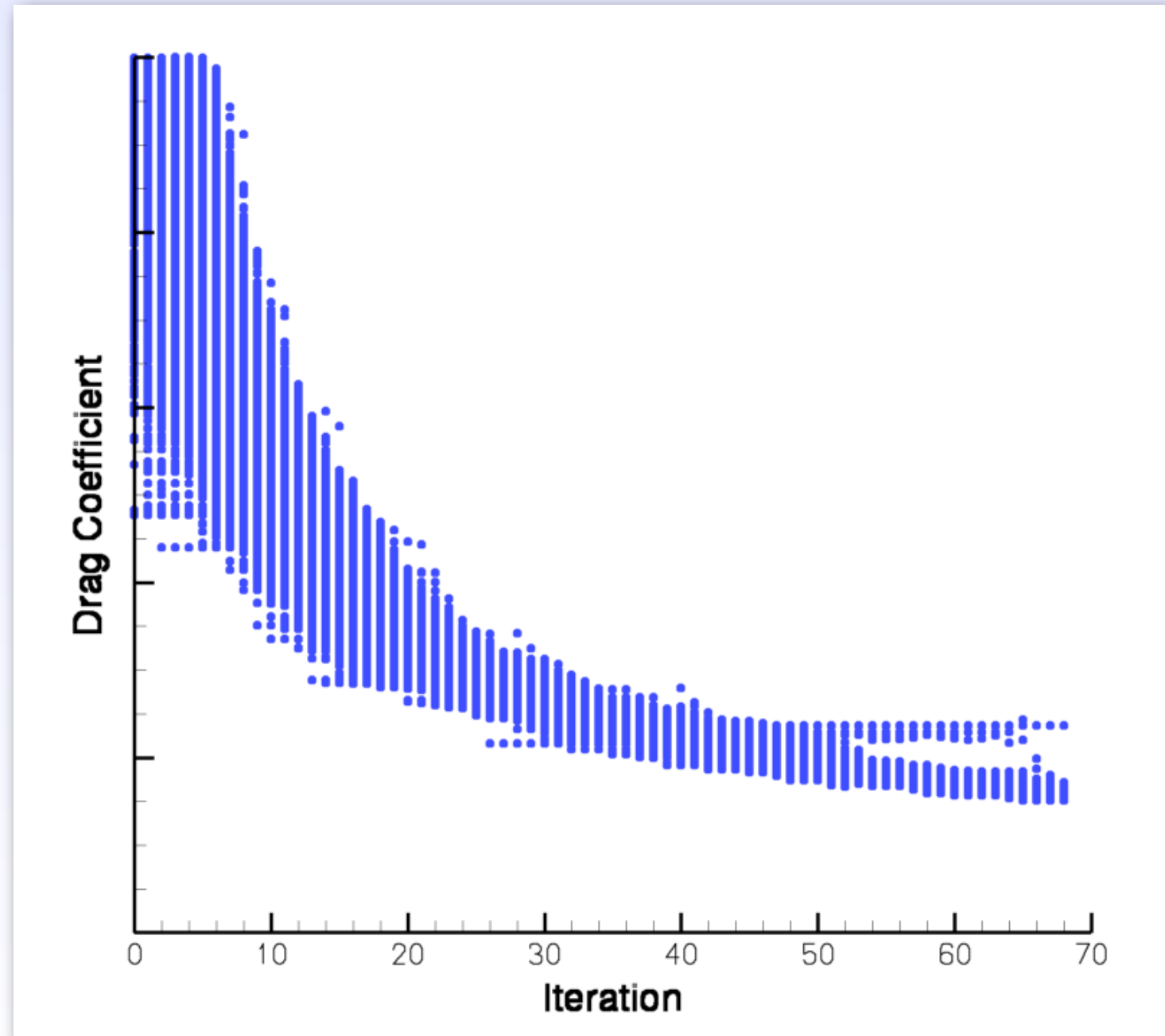


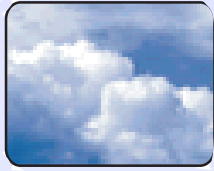


# Details of Optimization

## ◆ Example convergence history

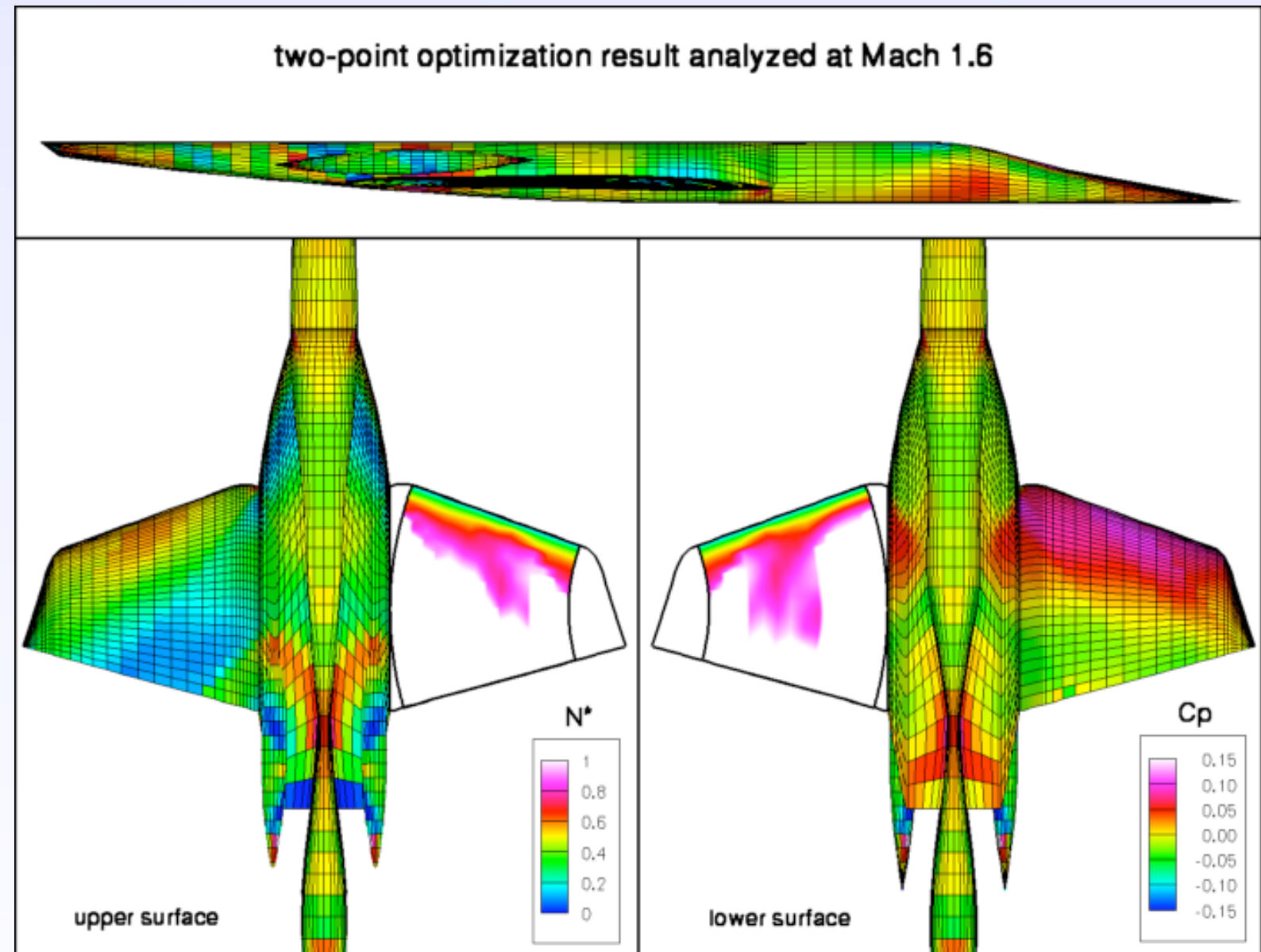
- 24 design variables
- population: 2304
- 16 cpu-weeks





# Sensitivity to Mach

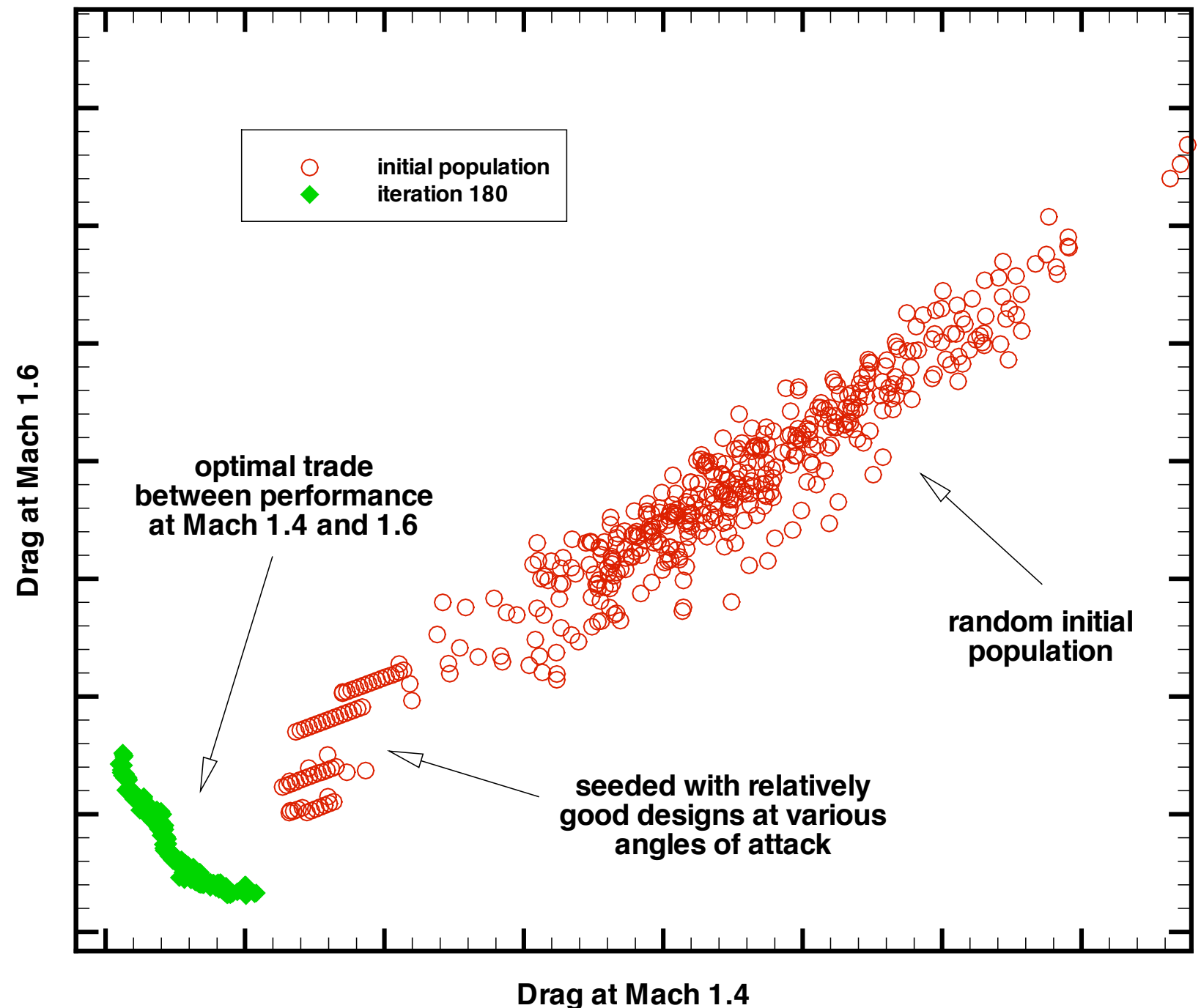
- ♦ Long-range cruise at Mach 1.4
- ♦ High-speed cruise at Mach 1.6
- ♦ Laminar extent poor at Mach 1.6





# Multi-Objective Optimization

- ◆ Optimized at both Mach 1.4 and 1.6 simultaneously
- ◆ Pareto-optimal set
- ◆ Population-based optimization (GA)
  - ranking and niching per book by Deb

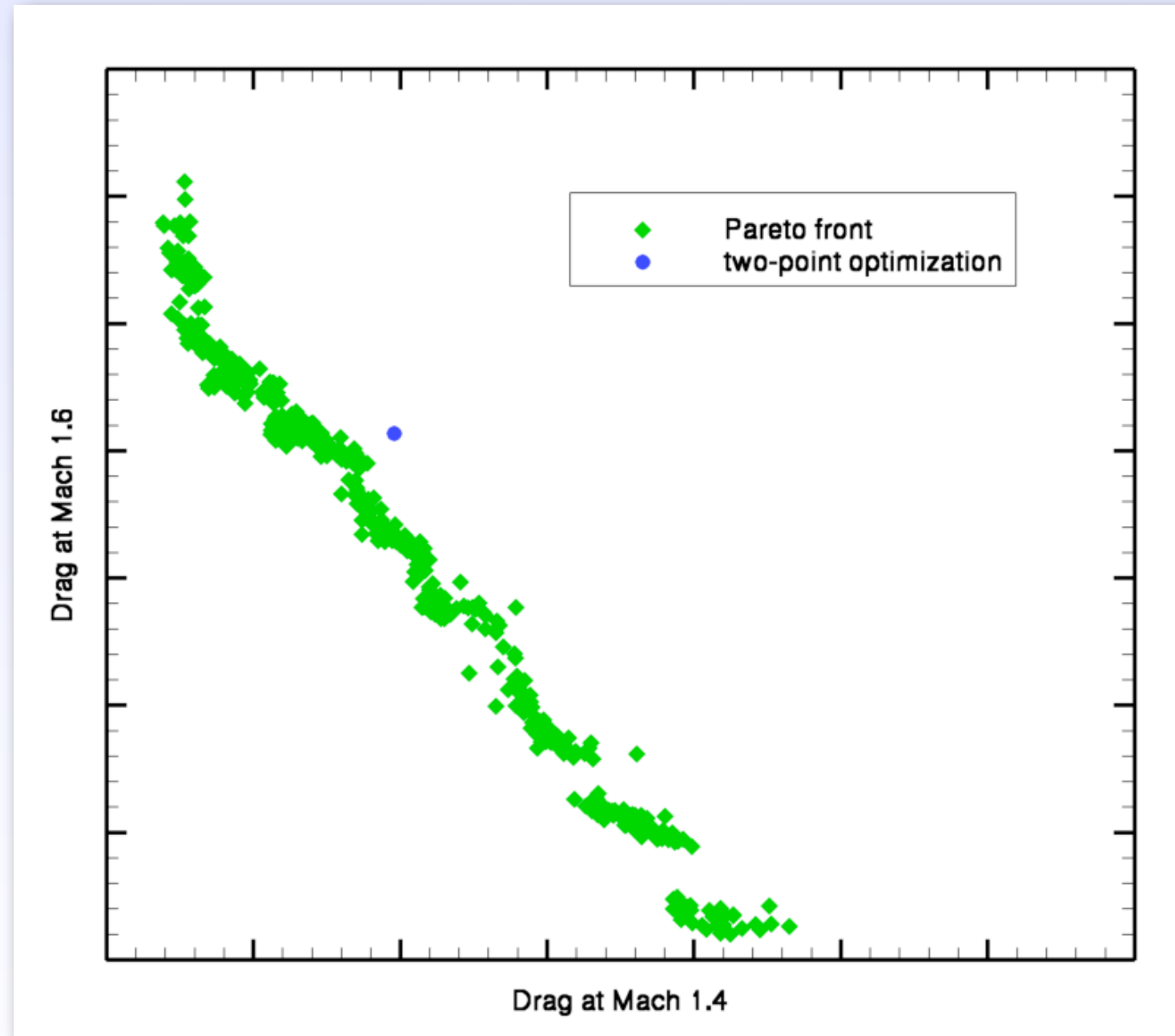
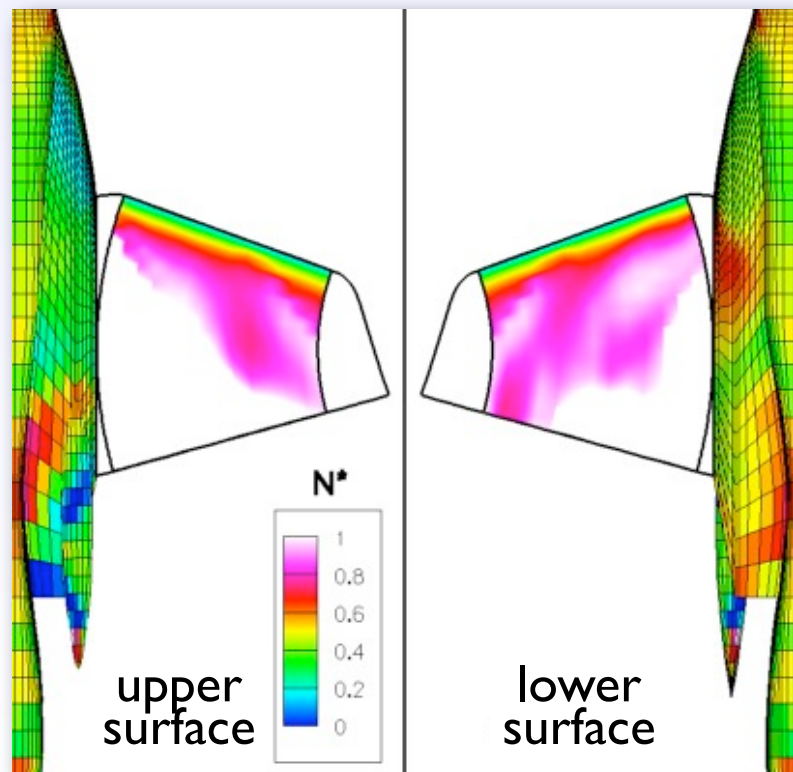






# Multi-Objective Optimization

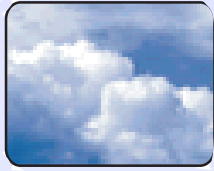
- ◆ Shows tradeoff between drag at two cruise speeds
- ◆ Found better Mach 1.6 result than single-point optimization



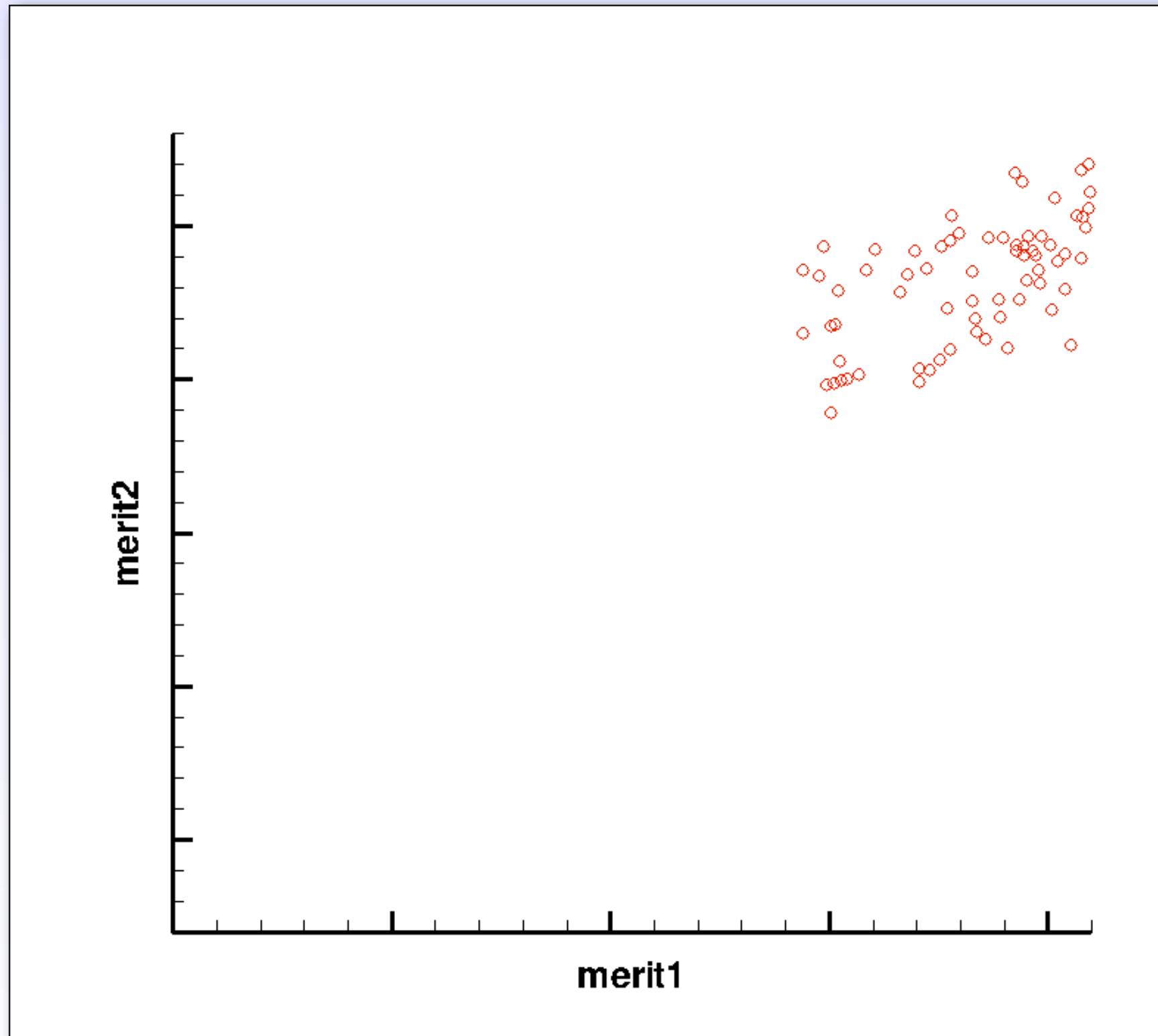


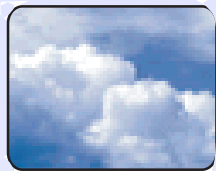
# Multi-Objective Optimization

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# Multi-Objective Optimization





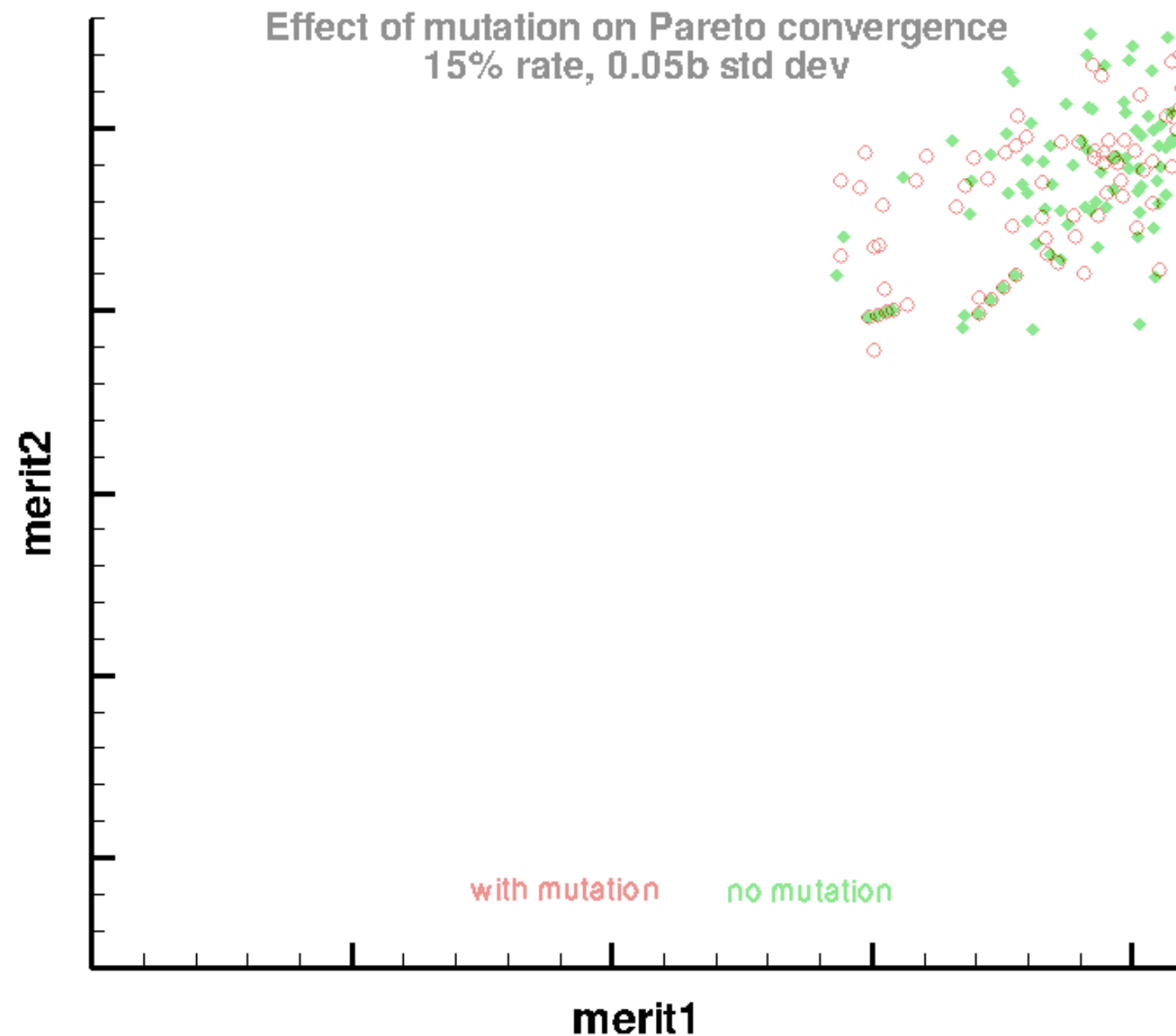
# Multi-Objective Optimization

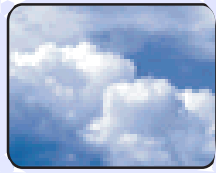
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# Multi-Objective Optimization





# Conclusions

- ✦ Optimization is key to Aerion natural laminar flow design
  - achieving laminar extent with minimal wave drag penalty
  - propulsion integration with 3D intakes and nozzles
- ✦ Simple optimization algorithms can be quite useful
- ✦ Robustness more important than fast convergence
- ✦ Some improvement more important than a provable optimum
  - “An optimal airplane is one that is out on the ramp ready to fly a mission.” *C. L. Johnson*



# Conclusion



Before

After

