

Managing Models in Simulation-Based Design

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Outline:

- Problem setting
- Model management as means to decrease uncertainty and cost
- Other uncertainty issues
- If time, software development environment

Setting

- Design of engineering systems, characterized by design variable vector x
- Forward or analysis problem
 - Specify x ; solve the governing partial differential equation (or equations) for intermediate field or state variable u
 - Evaluate outputs of engineering interest, f , based on u
- Design problem
 - Formulate design objectives and constraints based on f
 - Find the best value of f

Requirement for models

- Conflict of model uncertainty (a large impediment to practical acceptance of PDE-based design) and cost
 - Must be sufficiently fine (high-fidelity) so that the outputs and their derivatives represent system performance
 - Must be sufficiently coarse to be affordable for repeated use within design context
- Some approaches to resolving the conflict
 - Reduce/manage uncertainty associated with analysis and design
 - Use higher-fidelity models at earlier stages of design
 - Improve tractability of high-fidelity models in all stages of design

Focus: CFD-based aerodynamic optimization

- Progression of state of the art in CFD
 - Structured grids
 - Heuristic solution adaptation
 - Overset and unstructured grids
 - In progress
 - Adaptive analysis with error bounds/estimates
 - Adaptive design optimization with well-defined error bounds
 - Future
 - Multiscale problems

Environment – the FUN3D Suite

- Direct development team of about 10 people works on analysis and design using the RANS equations on 3D unstructured grids
- Discrete adjoint formulation used as a basis for error estimation, grid adaptation, and design
- Elasticity PDE formulation used for moving mesh applications
- Automated complex-variable conversion is used for direct differentiation
- A unique capability: exact dual integration algorithm used for computing hand-coded discrete adjoint for full RANS discretization

Compute derivatives via adjoints

Combine cost function f with Lagrange multipliers λ_f and λ_g to form Lagrangian, L :

$$L(\mathbf{D}, \mathbf{Q}, \mathbf{X}, \lambda_f, \lambda_g) = \underbrace{f(\mathbf{D}, \mathbf{Q}, \mathbf{X})}_{\text{Objective: Lift, drag, boom, etc.}} + \lambda_f^T \underbrace{\mathbf{R}(\mathbf{D}, \mathbf{Q}, \mathbf{X})}_{\text{Flow Equations}} + \lambda_g^T \underbrace{(\mathbf{K}\mathbf{X} - \mathbf{X}_{\text{surface}})}_{\text{Mesh Equations}}$$

Differentiate with respect to \mathbf{D} :

$$\begin{aligned} \frac{dL}{d\mathbf{D}} = & \frac{\partial f}{\partial \mathbf{D}} + \left[\frac{\partial \mathbf{R}}{\partial \mathbf{D}} \right]^T \lambda_f + \left[\frac{\partial \mathbf{Q}}{\partial \mathbf{D}} \right]^T \left\{ \frac{\partial f}{\partial \mathbf{Q}} + \left[\frac{\partial \mathbf{R}}{\partial \mathbf{Q}} \right]^T \lambda_f \right\} \\ & + \left[\frac{\partial \mathbf{X}}{\partial \mathbf{D}} \right]^T \left\{ \frac{\partial f}{\partial \mathbf{X}} + \left[\frac{\partial \mathbf{R}}{\partial \mathbf{X}} \right]^T \lambda_f + \lambda_g^T \mathbf{K} \right\} - \lambda_g^T \left[\frac{\partial \mathbf{X}}{\partial \mathbf{D}} \right]_{\text{surface}} \end{aligned}$$

$$\left[\frac{\partial \mathbf{R}}{\partial \mathbf{Q}} \right]^T \lambda_f = - \frac{\partial f}{\partial \mathbf{Q}} \quad \begin{array}{l} \text{Flowfield} \\ \text{Adjoint} \\ \text{Equation} \end{array}$$

$$\mathbf{K}^T \lambda_g = - \left\{ \frac{\partial f}{\partial \mathbf{X}} + \left[\frac{\partial \mathbf{R}}{\partial \mathbf{X}} \right]^T \lambda_f \right\} \quad \begin{array}{l} \text{Mesh} \\ \text{Adjoint} \\ \text{Equation} \end{array}$$

$$\frac{dL}{d\mathbf{D}} = \frac{\partial f}{\partial \mathbf{D}} + \lambda_f^T \frac{\partial \mathbf{R}}{\partial \mathbf{D}} - \lambda_g^T \left[\frac{\partial \mathbf{X}}{\partial \mathbf{D}} \right]_{\text{surface}} \quad \begin{array}{l} \text{Sensitivity} \\ \text{Equation} \end{array}$$

(Courtesy
Eric Nielsen)

Benefits of adjoints

- Adjoint relate the local equation error to outputs of engineering interest providing
 - Rigorous error estimation and grid adaptation metric
 - No need for *a priori* knowledge of the flowfield
 - No reliance on heuristics for adaptation
 - Natural stopping criterion for convergence
 - Increases efficiency, reduces cost and uncertainty in analysis and design
 - The most efficient means of computing derivatives for functions of high dimensionality
 - Unlike other methods (e.g., finite differencing), independent on dimensionality

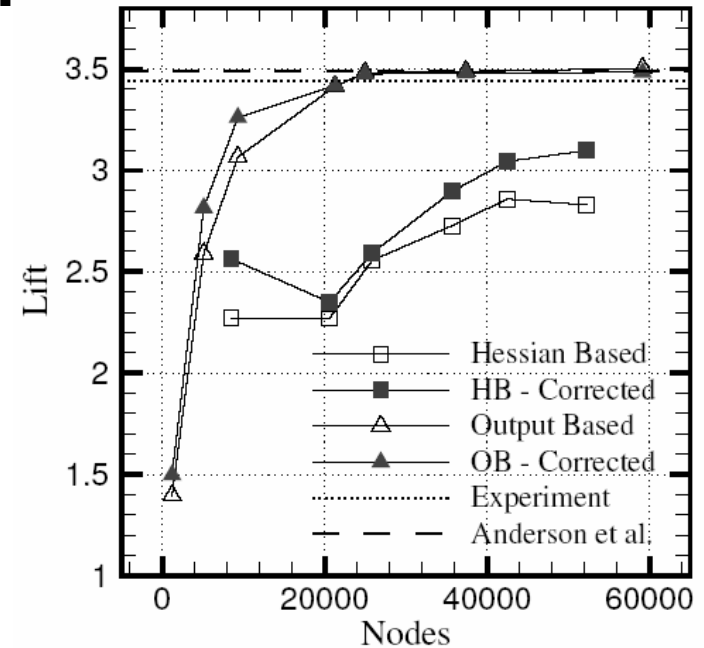
Adjoint-Based Mesh Adaptation

2D High-Lift Example

- Need accurate lift evaluation
- The initial mesh is coarse
- The adjoint-based technique recognizes important regions of the flow

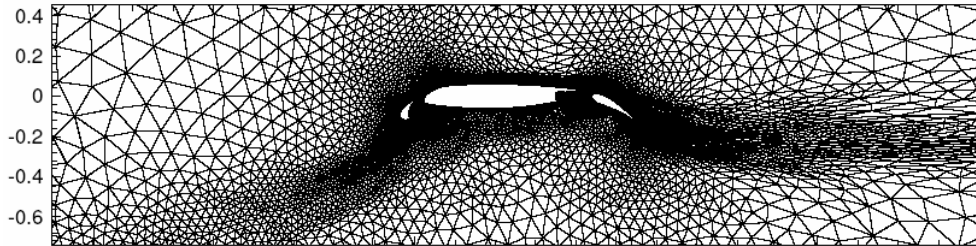
Courtesy Venditti & Darmofal at MIT (using FUN2D)

EET - Lift
 $Re = 9 \times 10^6$ - $M_\infty = 0.26$ - $\alpha = 8^\circ$



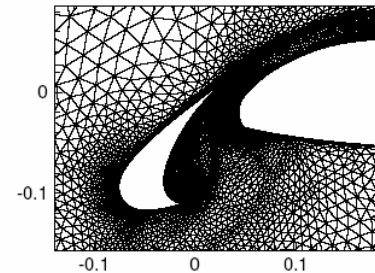
Output-based Adaptation (Lift)

24965 Nodes



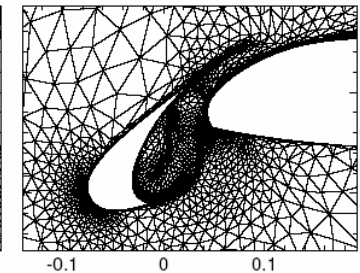
Output-based Adaptation (Lift)

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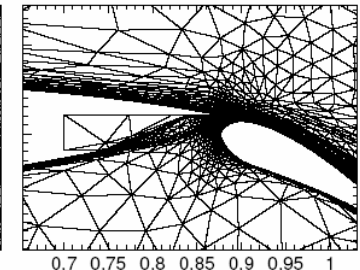
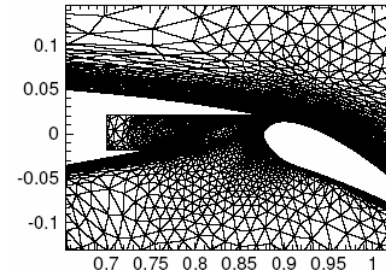
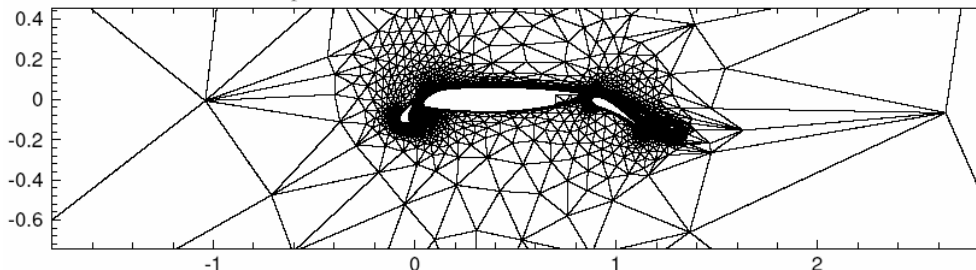
Pure Hessian-Based Adaptation

52235 Nodes

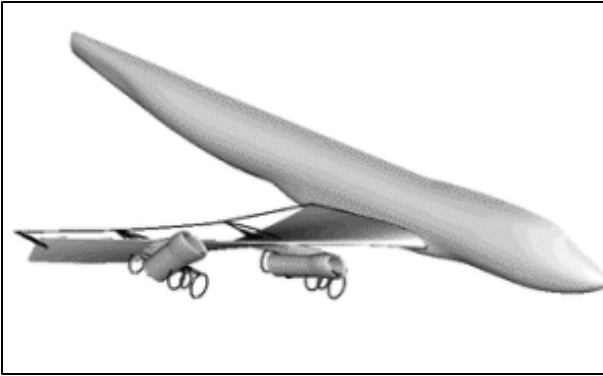


Pure Hessian-Based Adaptation

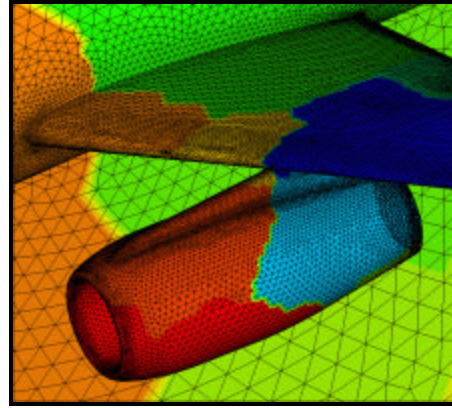
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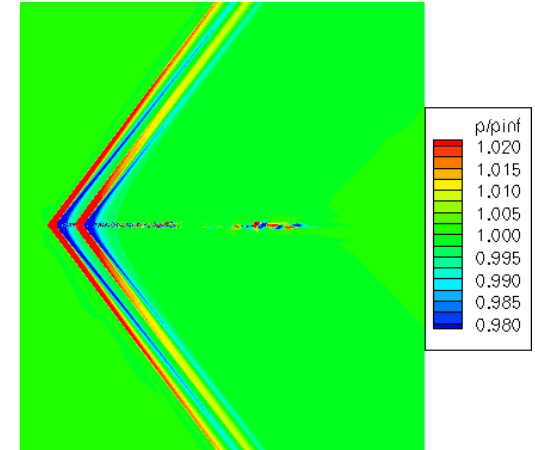
The FUN3D design environment



Parameterization

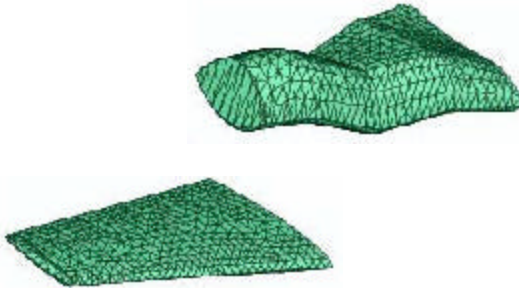


Domain Decomposition



Flow Solver: f (e.g. C_D)

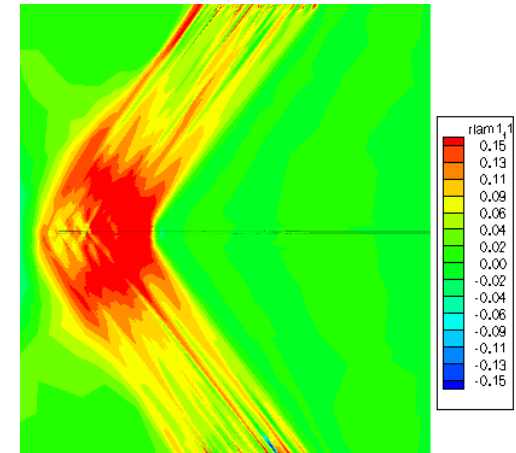
Minimize(f)



Mesh Movement

$$\nabla f$$

Derivative Evaluation



Adjoint Solver: $?_f$

Specifics of simulation-based optimization setting

- Despite quality and efficiency of models, expensive and not very robust function & derivatives
 - Pervasive efforts in improving tractability of hi-fi models in design optimization (Sandia, Boeing, INSEAN, to name a few)
- Assume a set of models (hi/lo-fi) of varying accuracy/cost, with no information about model relationship or structure
 - E.g., variable-resolution, varying convergence, variable-fidelity physics, etc.
 - Special model structure or context provides additional algorithmic possibilities (e.g., variable-resolution models in multigrid context, Lewis and Nash; Gratton, Toint, Sartenauer)
- “Preliminary” design / hi-fi models: min. $O(10^2-10^3)$ variables
 - Must rely on derivative-based optimization
 - In lower-dimensional problems, model management can rely on derivative-free optimization and data sampling models (e.g., Booker et al., numerous other efforts); Space Mapping (Bandler et al.) is another approach; similarity of trends in models important in 0-order approximations
- Assume black-box function evaluation
 - Many efforts in problem formulation
 - Simultaneous analysis and design methods not current focus, but discussion on models applies

Addressing tractability of high-fidelity models

- 1st order Approximation and Model Management Optimization (AMMO) (e.g., NMA & Lewis, AIAA-96-4101/02)
 - Replace local Taylor-series models in subproblems of NLP algorithms with available lower-fidelity models (heuristic use of lo-fi models long-standing in engineering)
 - No reason to assume that lo-fi model trends follow those of hi-fi model \Rightarrow impose local consistency conditions, i.e., assure local similarity of trends
 - AMMO can be imposed on any algorithm; usually faster than the basic algorithm because lo-fi models have better global properties than local Taylor-series models

AMMO vs. single-fidelity model optimization

Single-fidelity trust-region algorithms

- Do until convergence
 1. At x_k build **local models** (Taylor series) of the objective and constraints based on information computed by **hi-fi simulation**
 2. Compute a trial step by solving a subproblem based on **local hi-fi models**
 3. Check improvement in hi-fi responses and update iterates
- End do

Variable-fidelity (AMMO) algorithms

- Do until convergence
 1. At x_k select a model from a suite of available **lo-fi models** and **compute corrections based on hi-fi and lo-fi models** so that 1st order consistency holds
 2. Compute a trial step by solving a subproblem based on **corrected lo-fi models**, using standard techniques
 3. Check improvement in hi-fi responses and update iterates
- End do

AMMO: Convergence vs. Efficiency

- (Essentially) traditional trust-region convergence results apply
- Convergence analysis relies on enforcing local similarity of trends: if f_{HI} is a high-fidelity model and f_{LO} is a low-fidelity model, f^{corr} in optimization subproblem is required to be consistent to 1st order at each major iteration x_k :

$$f^{\text{corr}}(x_k) = f_{\text{HI}}(x_k) \quad \text{and} \quad \nabla f^{\text{corr}}(x_k) = \nabla f_{\text{HI}}(x_k)$$

- Exact consistency not needed, but easy to enforce
- Practical efficiency is problem/model dependent on
 - Global predictive properties of low-fidelity model
 - Data-fitting models – with sufficient sampling, good *global* predictive properties
 - Problem/model dependent for other models
 - Expense of low-fidelity model

Enforcing local consistency via corrections

- Additive: $f_{\text{HI}}(x) = f_{\text{LO}}(x) + a(x)$
- Multiplicative: $f_{\text{HI}}(x) = \beta(x) f_{\text{LO}}(x)$
- Approximating exact $a(x) = f_{\text{HI}}(x) - f_{\text{LO}}(x)$, $\beta(x) = f_{\text{HI}}(x) / f_{\text{LO}}(x)$ by linear (quadratic) Taylor series expansion about x_k guarantees 1st (2nd) order consistency. E.g., building

$$\beta_k(x) = \beta(x_k) + \nabla \beta(x_k)^T (x - x_k)$$

and setting $f_k^{\text{corr}}(x) = \beta_k(x) f_{\text{LO}}(x) \Rightarrow$ 1st order consistency at x_k (Haftka, 1991)

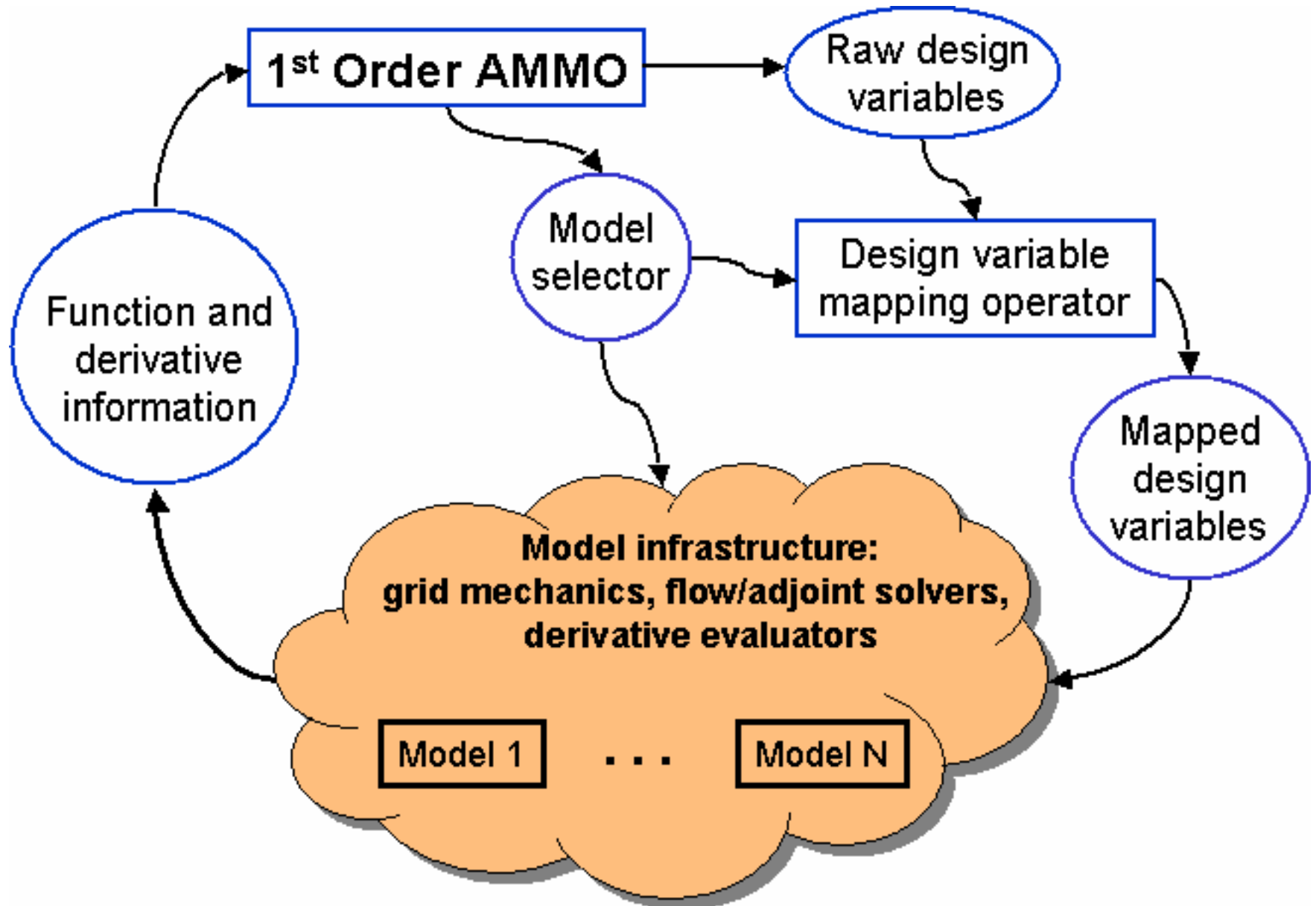
(Corrections can be mixed as necessary)

Computational experience

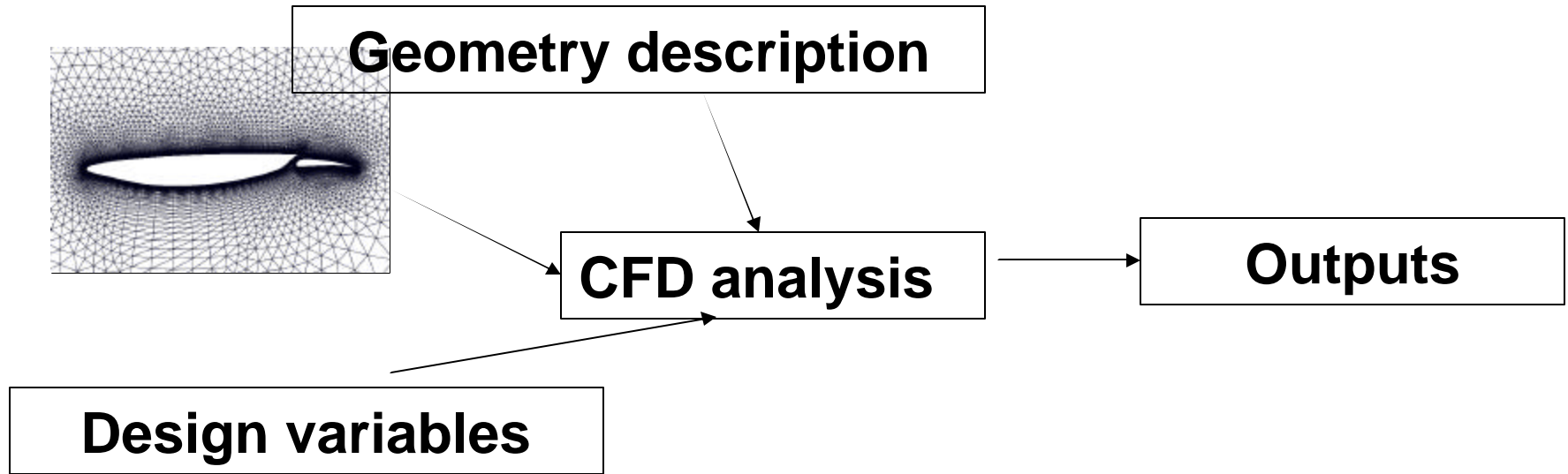
Several independent proofs of concept using AMMO for aerodynamic and hydrodynamic and MD design (e.g., Eldred, *et al*, Marduel *et al.*, Campana & Peri)

- Typical savings in hi-fi function evaluations from 3 to 7-fold
- Q: If mimicking local Taylor series approximations, why expect any savings compared to conventional derivative-based methods?
- A: Local corrections, but hope that corrected lo-fi model has better global behavior. So far, has held for CFD-based applications.
- At NASA LaRC:
 - AMMO imposed on several algorithms (SQP, Augmented Lagrangian, a multilevel method)
 - Example: aerodynamic design optimization...

AMMO framework



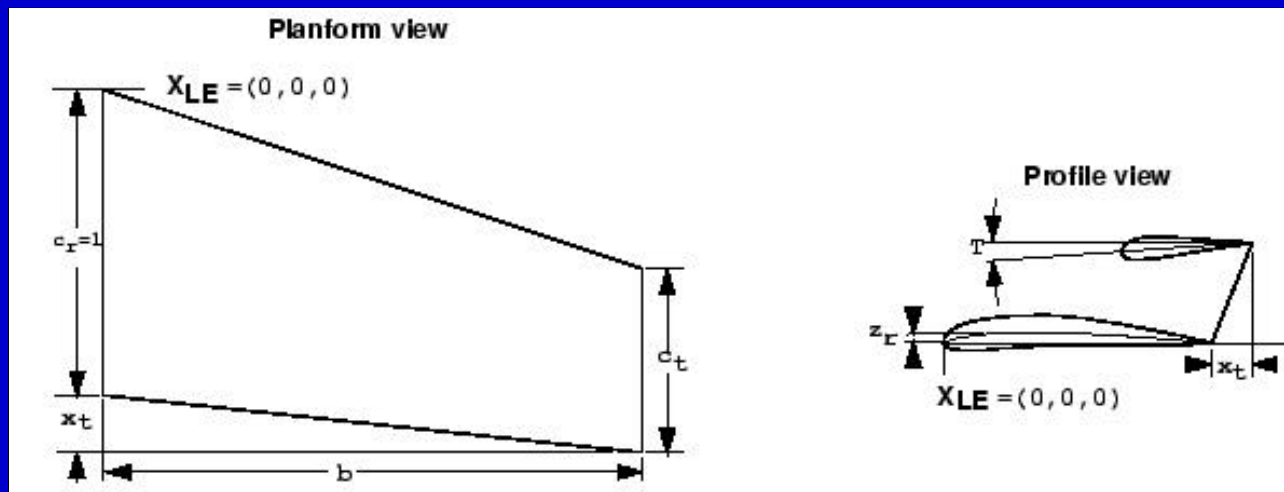
Example: aerodynamic shape optimization



- Minimize objectives (e.g., $-L/D$)
- subject to constraints on the moments

Summary of AMMO with variable resolution models:

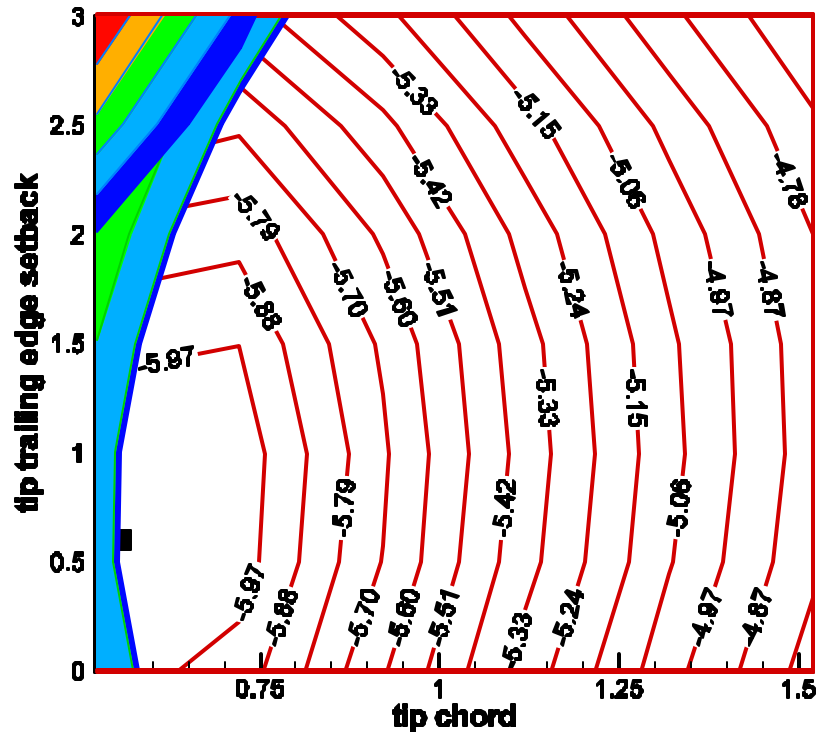
- Wing design: minimize some combination of lift and drag, subject to constraints on the moments; same equations (Euler), varying grid refinement



- Observations
 - If meshes were generated as proper subsets of one another, trends were similar
 - Functions computed on meshes that are not proper subsets of a mesh can result in large landscape variations

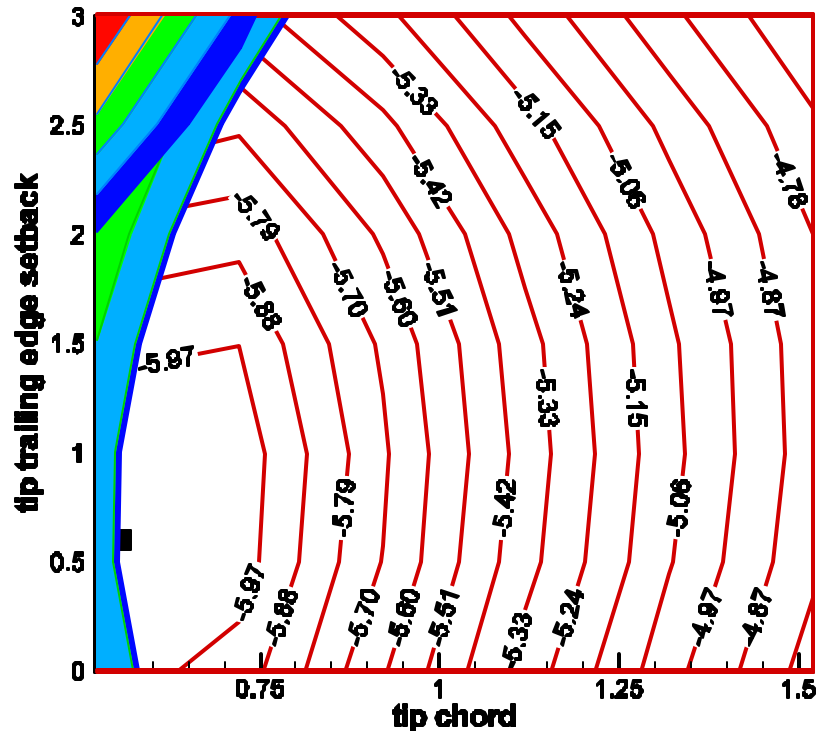
Favorable relationship between hi-fi & lo-fi model level sets

193x49x33 mesh, CL/CD, CLxS, CM

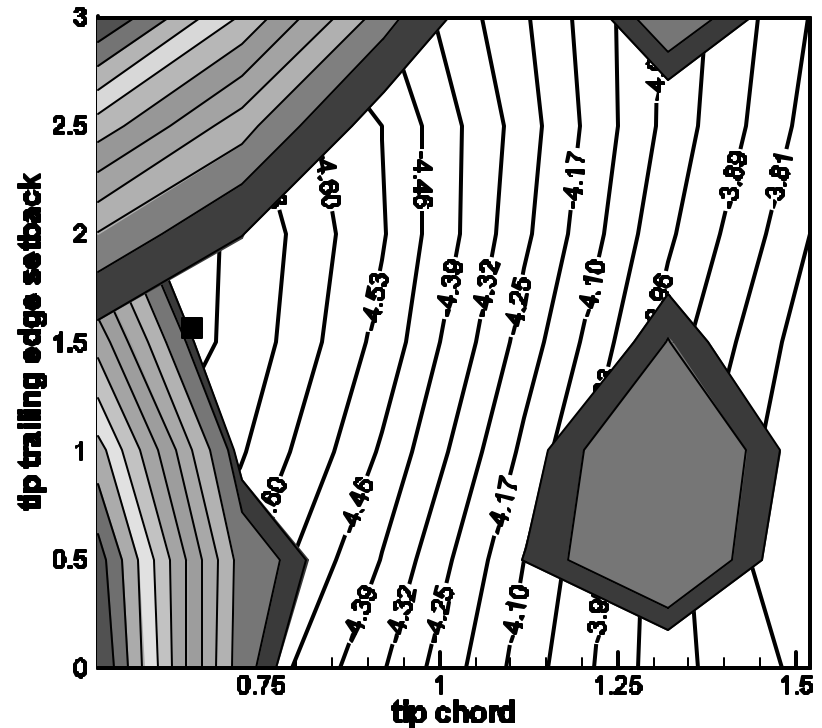


Less favorable relationship between hi-fi & lo-fi model level sets

193x49x33 mesh, CL/CD, CLxS, CM



97x25x17, cubic poly, CL/CD, CLxS, CM

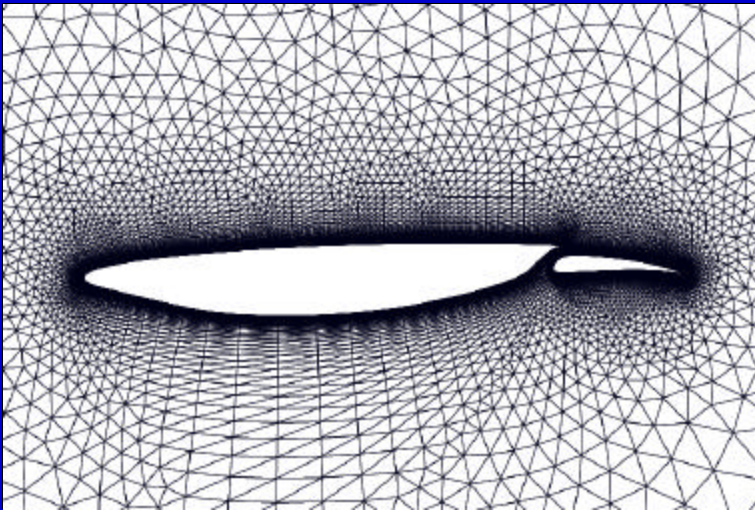


No impact on performance (subsonic, well-behaved problem);
typical savings in terms of hi-fi evaluations 3-4 times (no tuning
of algorithms)

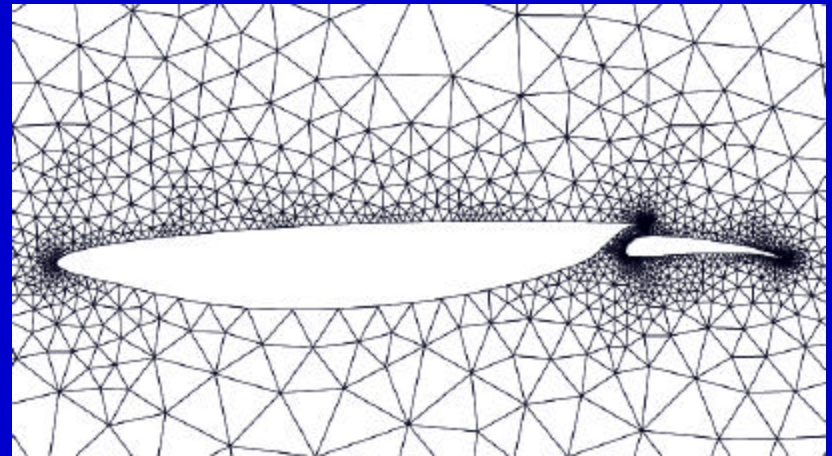
Summary of AMMO with variable resolution, variable-fidelity physics models

- Airfoil design; different equations (Navier-Stokes vs. Euler), varying grid refinement; posed as bound-constrained problem

Hi-fi grid

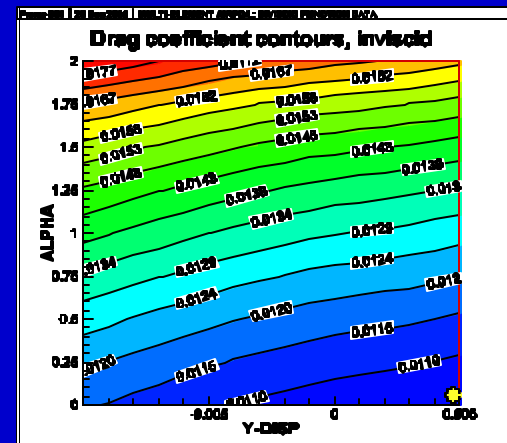
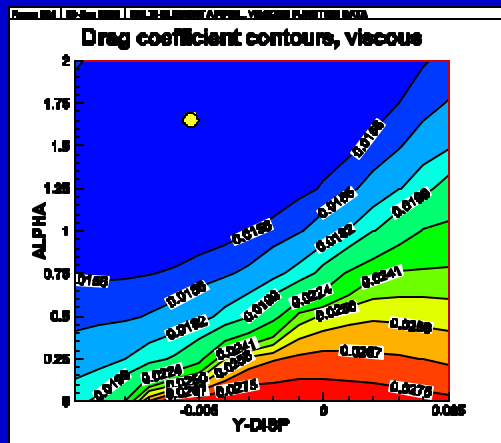
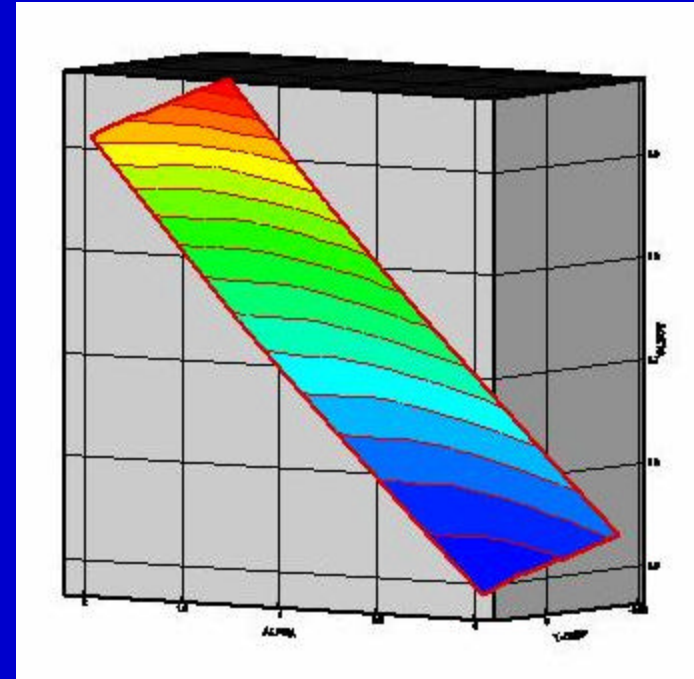
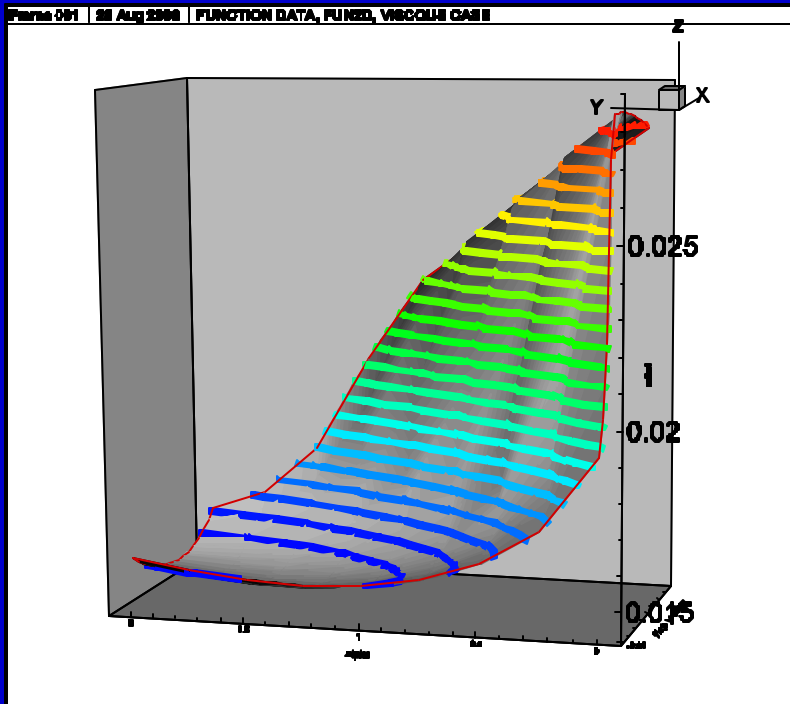


Lo-fi grid



- Trends in models of different physical fidelity can differ drastically

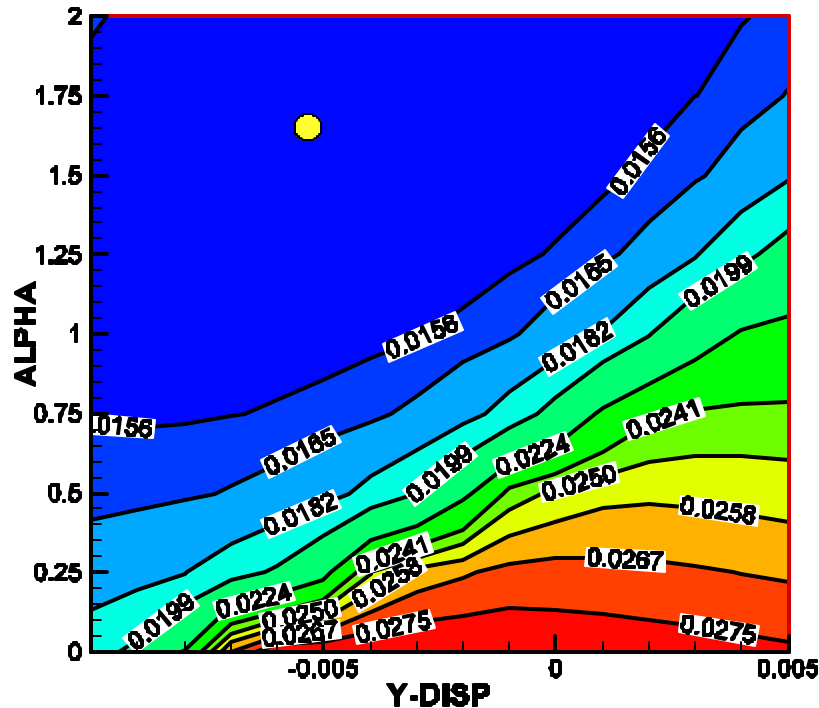
Dissimilar models hi-fi and lo-fi models (combination of lift and drag)



Hi-fi vs. corrected lo-fi model

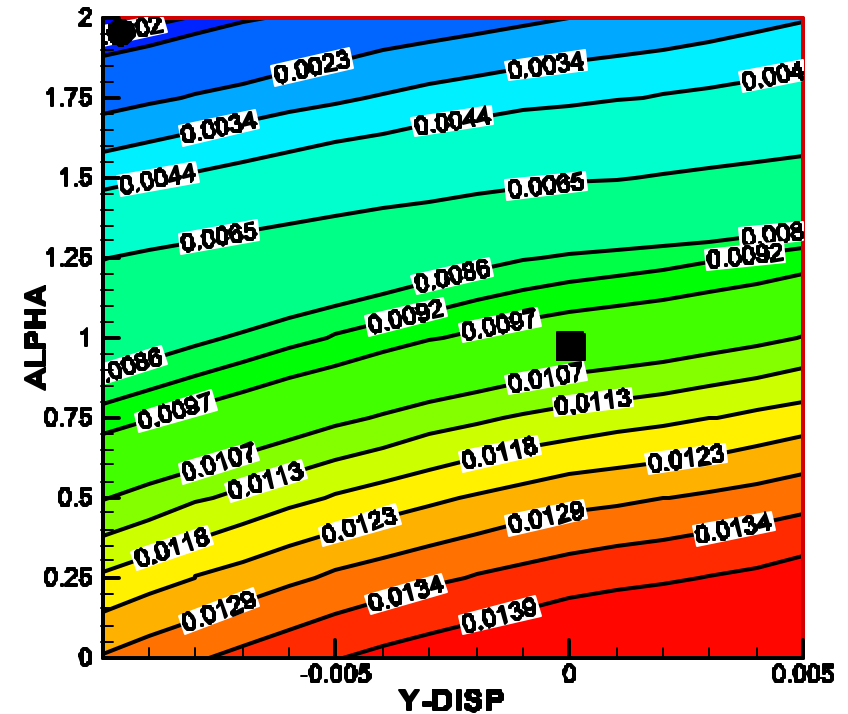
Frame 001 | 20 Sep 2000 | MULTI-ELEMENT AIRFOIL: VISCOUS FUNCTION DATA

Drag coefficient contours, viscous



Frame 001 | 31 Aug 2000 | MULTI-ELEMENT AIRFOIL: CORRECTED LO-FI DATA

Drag coefficient contours, corrected inviscid



First-order correction reversed trends

Efficiency depends on relative expense of low-fidelity model

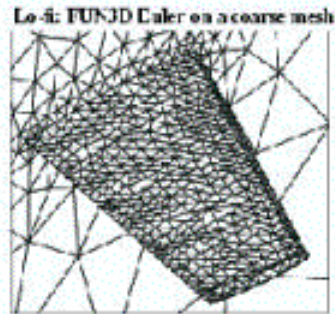
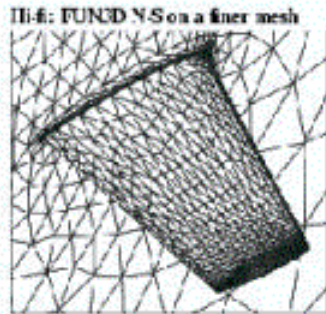
Example: 2D (multi-element airfoil) aerodynamic optimization problem;
time/hi-fi analysis / time/lo-fi analysis » 120

	hi-fi eval	lo-fi eval	total CPU time	factor
Optimization (PORT), 2 variables	14/13		» 12 hrs	
AMMO, 2 variables	3/3	19/9	» 2.41 hrs	» 5
Optimization (PORT), 84 variables	19/19		» 35 hrs	
AMMO, 84 variables	4/4	23/8	» 7.2 hrs	» 5

(functions/gradients)

Savings depend on relative expense of low-fidelity model, cont.

3D Aerodynamic Design with AMMO



$$\begin{aligned} \min_{\mathbf{x}} \quad & 5C_D^2 + \frac{1}{2}(C_L - 0.12303)^2 \\ \text{s.t.} \quad & \mathbf{x}_l \leq \mathbf{x} \leq \mathbf{x}_u \\ & \alpha_0 = 3.06^\circ, M_\infty = 0.84, Re = 5 \times 10^6 \end{aligned}$$

- Approximately 4-fold savings in terms of hi-fi function evaluations
- Only 2 time savings; lo-fi model also expensive
- Developing “optimal” lo-fi models; distribute computations via PVD-like approach (after Ferris & Mangasarian)

Distributing computation (following Ferris & Mangasarian)

- Current problem: $\text{minimize } f(x), \text{ s.t. } x \in B$
- Notation: for $x \in \mathbb{R}^n$, partitions are $x_l \in \mathbb{R}^{n_l}$, $l=1, \dots, p$ and n_l sum up to n
- Let l^* be a complement of l in $\{1, \dots, p\}$, $\mu_{l^*} \in \mathbb{R}^{p-1}$
- Let $d^k \in \mathbb{R}^n$ be an arbitrary direction, partitioned into n subsets and

$$D_{l^*}^k = \begin{pmatrix} d_1^k & & & & & \\ & \dots & & & & \\ & & d_{l-1}^k & & & \\ & & & d_{l+1}^k & & \\ & & & & \dots & \\ & & & & & d_p^k \end{pmatrix}^{n_l}$$

- $D_{l^*}^k$ and μ_{l^*} are used to form the “forget-me-not” term in subproblems

AMMO with PVD at a low-fidelity subproblem level

Given f_{HI} , x^0 , and $B^0=B^{\text{max}}$ (bound constraints)

Do until convergence

1. Choose f_{LO}^k and compute correction s.t. $f_{\text{corr}}^k(x^k)=f_{\text{HI}}(x^k)$,
 $\nabla f_{\text{corr}}^k(x^k)=\nabla f_{\text{HI}}(x^k)$
2. Solve approximately for s^k : $\min_s f_{\text{corr}}^k(x^k + s)$ s.t. $x^k + s \hat{I} B^k$:

Do until stopping criterion is satisfied{

Solve in parallel: $\min_{x_I, \mu_{I^*}} \varphi_I^k(x_I, \mu_{I^*}) \equiv f_{\text{corr}}^k(x_I, x_{I^*}^k + D_{I^*}^k \mu_{I^*})$
s.t. $(x_I, x_{I^*}^k + D_{I^*}^k \mu_{I^*}) \hat{I} B^k$,

resulting in $(y_I^k, \mu_{I^*}^k)$

Synchronize: Compute x^{k+1} s.t. $f(x^{k+1}) \leq \min_{(y_I^k, \mu_{I^*}^k)} \varphi_I^k$

$$s^k = x^{k+1} - x^k$$

3. Update the iterate and bounds based on the actual decrease in f_{HI} produced by s^k vs. the decrease predicted by f_{corr}^k

}

Comments

- Forget-me-not term distinguishes PVD from block-Jacobi and coordinate descent (secondary variables are fixed there)
- Allowing secondary variables to move improves robustness of the algorithm, as observed in computations by Ferris and Mangasarian
- The choice of d^k is arbitrary theoretically, but important in practice; one particular choice (F&M) is scaled $-\nabla f(x^k)$ for unconstrained problems
- Following Solodov, we use the projected gradient residual function
$$d^k = r(x^k), \text{ where } r(x) = x - P_B [x - \nabla f(x^k)]$$
- Solodov's convergence theory allows for sufficient decrease instead of global solutions for the subproblems \Rightarrow consequences for practical problems and parallelism

But point design is not enough

- One reason direct optimization is not used more widely for actual design is the lack of robustness in **point** optima
- Currently, much activity in uncertainty-based design; many approaches
 - Global uncertainty quantification
 - Incorporation into optimization
- In practice, in aerospace design, **multipoint** (robust) design = heuristic inverse design methods
 - Designers ignore “start with a dog” approaches
 - Design optimal airfoils for several flight conditions and average them
 - Average several target pressure distributions and design an airfoil to the resulting distribution
 - Etc.

Problem formulation

- Consider objective function $f : X \times Y \rightarrow \mathfrak{R}$
 $x \in X$ are design variables, controlled
 $y \in Y$ uncertainty variables, not controlled
- Ideally, find $x^* \in X$ s.t., $\forall y \in Y$
$$f(x^*;y) = f(x;y) \quad \forall x \in X$$
- Example: aerodynamic shape design
 - Minimize drag of a *manufactured* airfoil; y are errors in manufacturing
 - Design an airfoil or a wing with good performance over a range of speeds and angles of attack; y are M_∞ and α

Problem formulation

- Central problem of statistical decision making
- Relax impossible problem...
 - via minimax principle (e.g., Ferguson 1967):
 - $\min_{x \in X} \psi(x) \equiv \sup_{y \in Y} f(x; y)$
 - conservative; protect against worst-case scenario
 - via Bayes principle (Welch et al. 1990):
 - $\min_{x \in X} \psi(x) \equiv \int_Y f(x; y) p(y) dy$
 - p is a probability density function on Y
 - minimize average loss; can be customized via p

Example: airfoil shape design

- $y = M_\infty$ and $f(x; M_\infty)$ is, say, the drag coefficient, then we want to solve

$$\min_{x \in X} \psi(x) \equiv \int_{\text{range of } M_\infty} f(x; M_\infty) p(M_\infty) dM_\infty$$

- Here p is the weight function that quantifies the value placed on performance at various speeds
- Such formulations studied by Huyse, Li, and others

Difficulty

- Tractability in question even for problems of medium size
- Under investigation (NMA and Trosset)
 - Low-fidelity models for integration (AMMO-like)
 - A variety of surrogates (data-fitting models) for integration

Now in the works, e.g.,

- Making use of special problem / model structure
 - Tighter integration of adjoint-based adaptation for CFD into optimization logic
 - Optimal modeling strategies, e.g., using lo-fi models of different geometric description (e.g., grid-based vs. non-grid based models); must deal with different variable domains
- PVD
 - General constraints
 - Multidisciplinary/multiobjective application