Shape Optimization for Trailing Edge Noise Control August 7, 2002

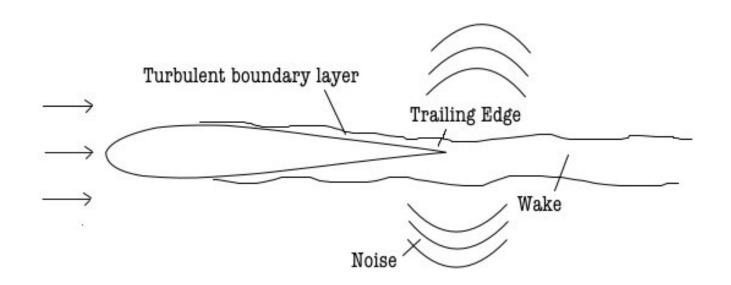
Alison L. Marsden

with
Meng Wang, Bijan Mohammadi, Parviz Moin
Supported by ONR





- Noise generated by flow past trailing edge of lifting surfaces
 - \square laminar flow
 - single tone from vortex shedding
 - □ turbulent flow
 - tonal and broadband noise



- Why Reduce Noise?
 - □ naval applications
 - ☐ aircraft and airframe noise
 - propeller noise

- Why Reduce Noise?
 - □ naval applications
 - ☐ aircraft and airframe noise
 - □ propeller noise
- Development of design methods for "real life" fluids problems
 - unsteadiness
 - □ turbulence

- Why Reduce Noise?
 - □ naval applications
 - ☐ aircraft and airframe noise
 - □ propeller noise
- Development of design methods for "real life" fluids problems
 - unsteadiness
 - □ turbulence
- Influence of surface shape on noise production

Objectives

- To develop a feasible method of shape optimization for trailing edge noise control
 - □ computationally affordable

Objectives

- To develop a feasible method of shape optimization for trailing edge noise control
 - □ computationally affordable
- Interface with existing Navier stokes code
 - □ demonstrate design of quiet trailing edge
 - □ 2-D unsteady laminar flow past small airfoil
 - ☐ Fully turbulent trailing edge flow

Noise Computation Methods

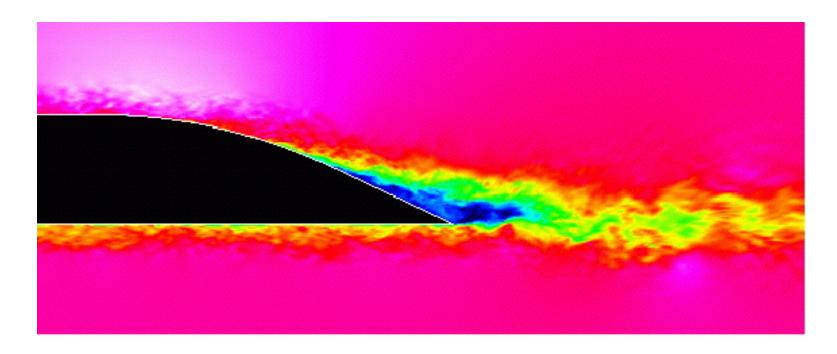
- Direct Numerical Simulation
 - □ Not suitable for low Mach number flows
 - \square Acoustic wavelength \gg flow scales
 - huge computational domain
 - \square acoustic energy \ll flow energy
 - need accurate numerics

Noise Computation Methods

- Direct Numerical Simulation
 - □ Not suitable for low Mach number flows
 - \square Acoustic wavelength \gg flow scales
 - huge computational domain
 - \square acoustic energy \ll flow energy
 - need accurate numerics
- Hybrid methods
 - □ good for small Mach number
 - ☐ Lighthill Analogy
 - ullet incompressible flow calculation o source term for wave equation
 - takes advantage of scale separation

Acoustic Computations

- Acurate simulation of trailing edge flow (Wang & Moin 2000)
 - ☐ Large eddy simulation
 - $\square Re = 2.15 \times 10^6, M = 0.09$
 - □ Comparison with experiments of Blake (1975)



Acoustic Computations

- Full Navier-Stokes solver
 - ☐ Sub-grid scale turbulence model
 - ☐ Curvilinear coordinates
- Expense estimate for one flow solution
 - ☐ Converged turbulence and noise statistics
 - □ 7 million mesh points
 - □ 10,000 SGI single processor hours
 - \square approximately 2 weeks using 32 processors!
- Need optimization method with minimum function evaluations!

Gradient based methods

- Gradient based methods
 - ☐ Direct
 - Compute gradients by "brute force"
 - Cost per iteration is \approx # parameters \times simulation cost
 - Expensive for many parameters
 - Not widely used

- Gradient based methods
 - ☐ Direct
 - Compute gradients by "brute force"
 - Cost per iteration is \approx # parameters \times simulation cost
 - Expensive for many parameters
 - Not widely used
 - ☐ Adjoint
 - Compute gradients by solving adjoint equation
 - Cost per iteration is $\approx 2 \times$ simulation cost
 - Need new ajoint solver for each flow solver
 - Data storage issues for unsteady flow
 - Used for aerodynamic design steady flows

- □ Incomplete Sensitivities (Mohammadi and Pironneau 2000)
 - New method
 - Demonstrated for simple cases
 - Compute gradients by approximation
 - Cost per iteration is \approx simulation cost
 - Portable and inexpensive

- Non-gradient based methods
 - ☐ Evolutionary Algorithms
 - Good for noisy cost functions
 - Numerical simulations always have some noise
 - Expense depends on number of parameters
 - ☐ EA with response surface method
 - Construct approximation of cost function during iterations
 - Reduced cost compared to other EA's

Gradient Evaluation

In general, cost function depends on geometry and state

$$\frac{dJ}{da_i} = \frac{\partial J}{\partial a_i} + \frac{\partial J}{\partial q_j} \frac{\partial q_j}{\partial a_i} + \frac{\partial J}{\partial U_k} \frac{\partial U_k}{\partial q_j} \frac{\partial q_j}{\partial a_i}$$

- $a_i = control variables$
- $q_i = geometric variables$
- $U_i = state (flow) variables$
- ☐ Classic methods are expensive, especially for unsteady flows
 - Direct computation
 - Adjoint method

Incomplete Sensitivities

■ Mohammadi and Pironneau (2000) suggest that if J is defined on a surface

$$\frac{dJ}{da_i} \approx \frac{\partial J}{\partial a_i} + \frac{\partial J}{\partial q_j} \frac{\partial q_j}{\partial a_i}$$

- Sensitivity to state negligible relative to geometric sensitivity
- ☐ No need to solve adjoint problem
- ☐ Independent of flow solver
- \square Computational cost \approx simulation cost

Optimization Procedure

□ Parameterize surface deformation (polynomials or splines)

$$\delta y = \sum_{i=1}^{n} a_i x^i, \quad a_i = \text{control parameters}$$

- ☐ Advance flow solver in time until statistically steady
- ☐ Evaluate the gradients until converged

$$\frac{dJ}{da_i} = \frac{J(a_i + \epsilon) - J(a_i)}{\epsilon}, \text{ and } \frac{\overline{dJ}}{\overline{da_i}} = \frac{1}{T} \int_0^T \frac{dJ}{da_i} dt$$

□ Calculate shape deformation with steepest descents

$$\delta a_i = -\lambda \frac{\overline{dJ}}{da_i}, \quad \delta y = \sum_{i=1}^n (a_i + \delta a_i) x^i$$

☐ Modify shape and generate new grid, repeat

Cost Function Definition

- Model Problem: Unsteady, laminar flow
 - □ 2-D Acoustically compact airfoil
 - Noise from unit span given by Curle's formula

$$\rho \approx \frac{M^3}{4\pi} \frac{x_i}{|\vec{x}|^2} \dot{D}_i(t - Mr)$$

$$\dot{D}_i = \frac{\partial}{\partial t} \int_{c} n_j p_{ij}(\vec{y}, t - Mr) d^2 \vec{y}, \qquad p_{ij} = p \delta_{ij} - \tau_{ij}$$

- ullet Total acoustic power $\propto \overline{\dot{D}_1^2} + \overline{\dot{D}_2^2}$
- ☐ Cost function is defined as

$$J = \overline{\left(\frac{\partial}{\partial t} \int_{S} n_{x} p(\vec{y}, t) dS\right)^{2}} + \overline{\left(\frac{\partial}{\partial t} \int_{S} n_{y} p(\vec{y}, t) dS\right)^{2}}$$

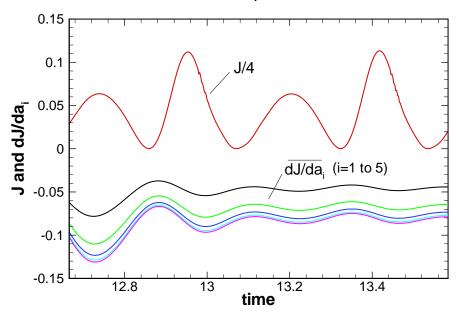
Model Problem: Setup

☐ Laminar flow over airfoil



- Initial T.E. tip angle 45 degrees
- Allow section of upper surface to deform (blue section)

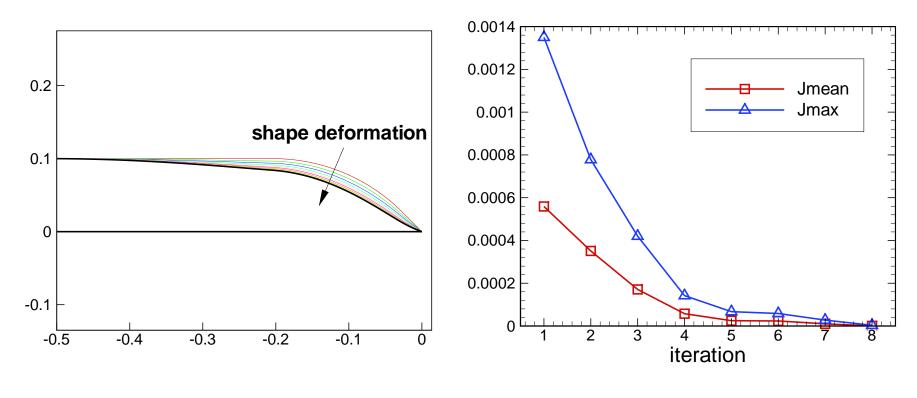
Time history of J and dJ/da; (Re=10,000, initial shape)

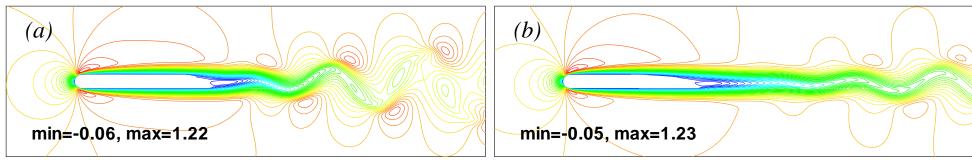


Model Problem: Re = 2,000

Shape Evolution

Cost Function Evolution



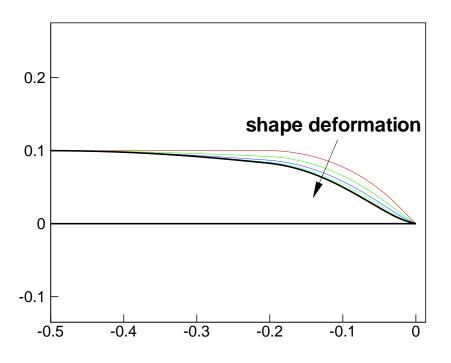


Initial velocity contours

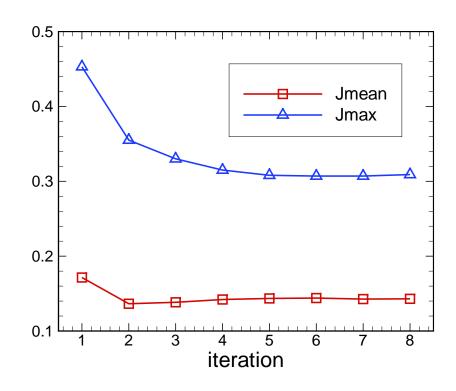
Final velocity contours

Model Problem: Re = 10,000

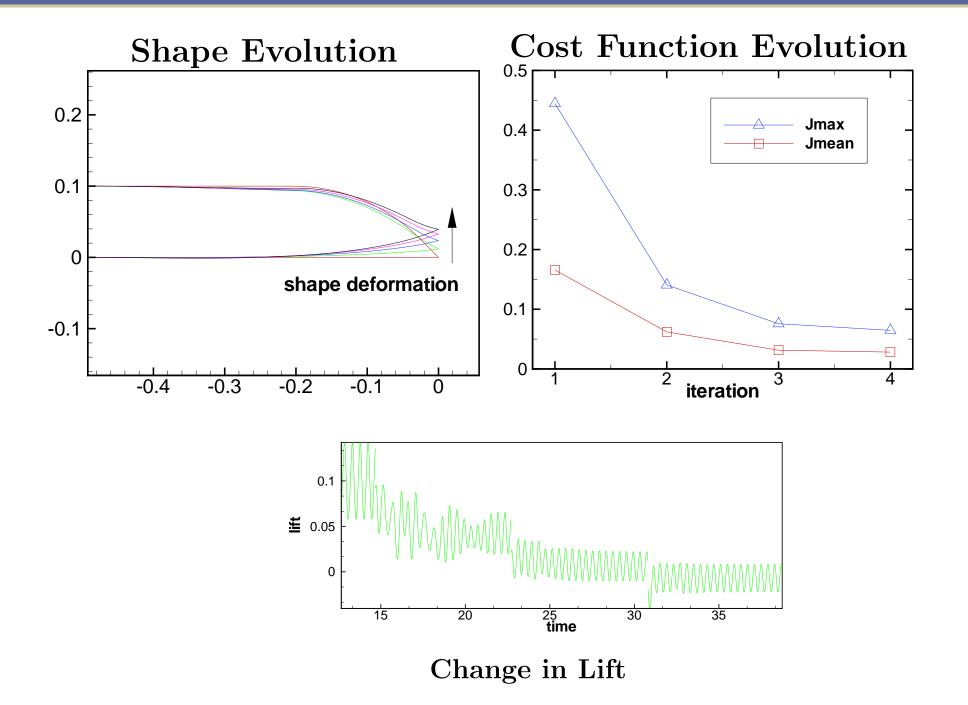
Shape Evolution



Cost Function Evolution

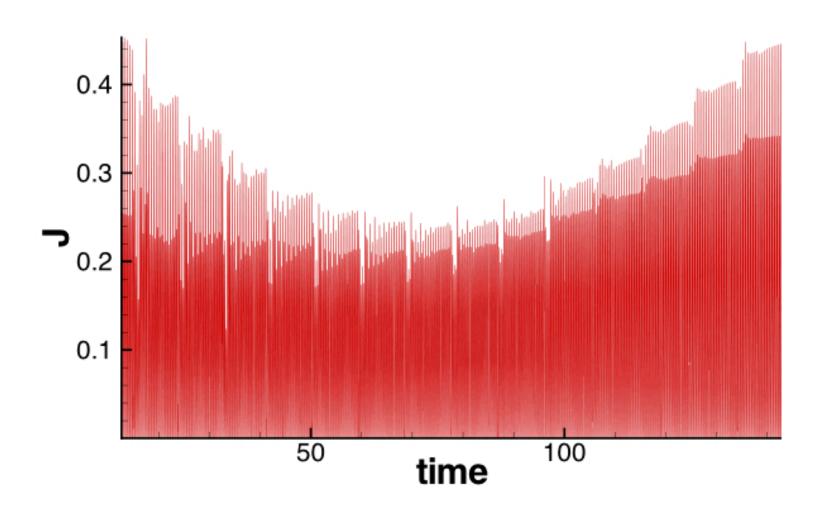


Both Sides: Re = 10,000

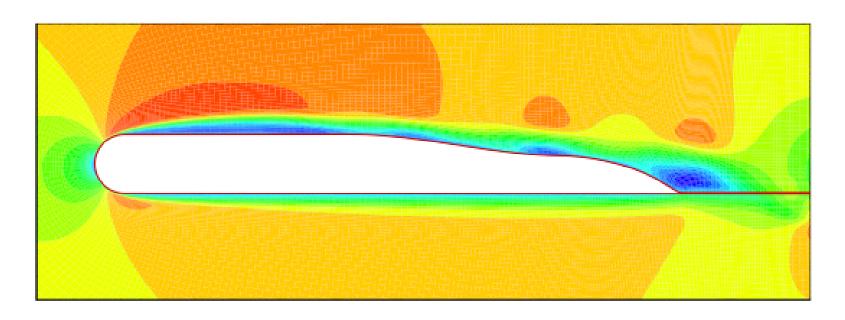


Assumption Breaks Down

Continue to iterate \rightarrow shape does not converge \rightarrow cost function increase!

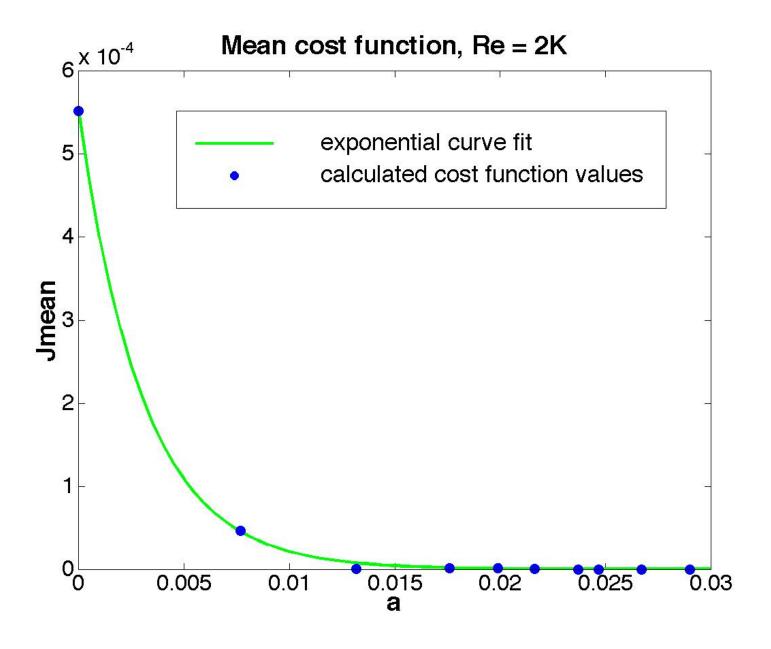


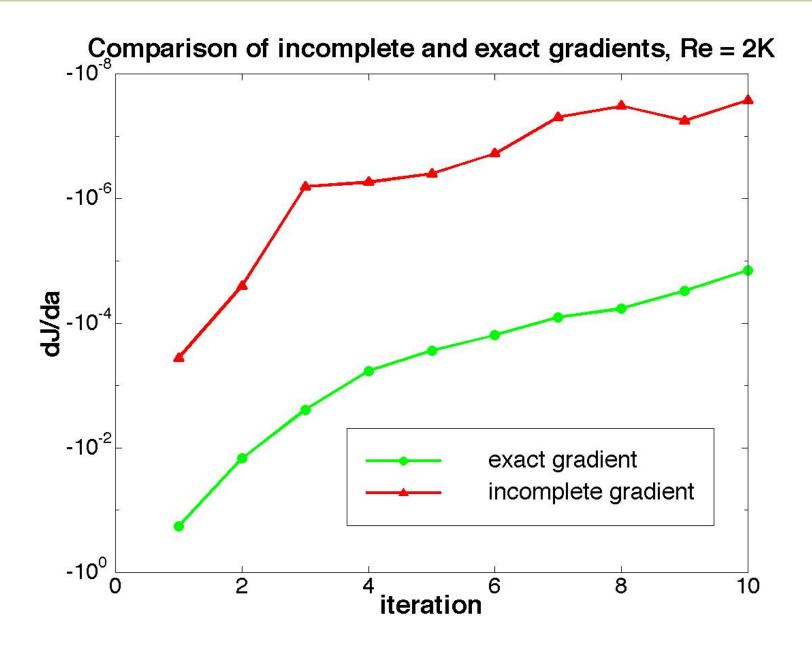
Assumption Breaks Down

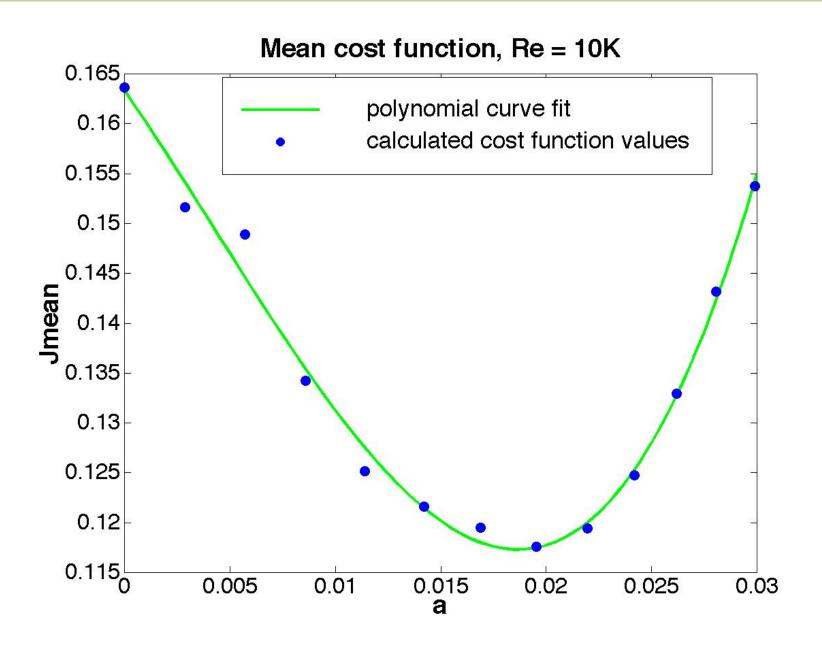


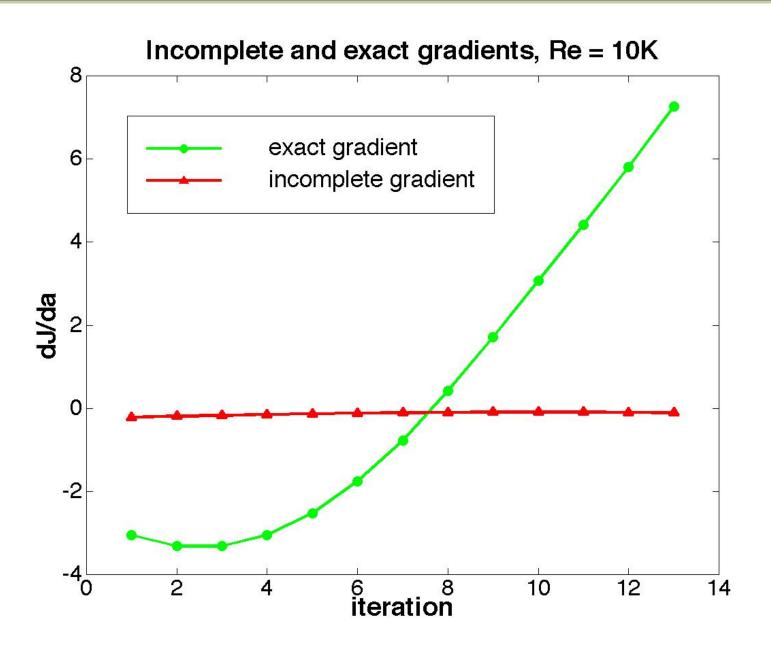
- Cost function increases when flow separates
- Gradient is wrong
 - ☐ Incomplete assumption invalid?

- Test validity of incomplete assumption
- With one spline case, compute exact gradients by "brute force"
 - ☐ Find exact gradient with finite difference
 - ☐ Convergence for exact gradient is difficult
 - integration of oscillatory cost function
 - ☐ Do curve fit of cost function vs. displacement
 - take derivatives of fit
 - ☐ Compare exact and incomplete gradients



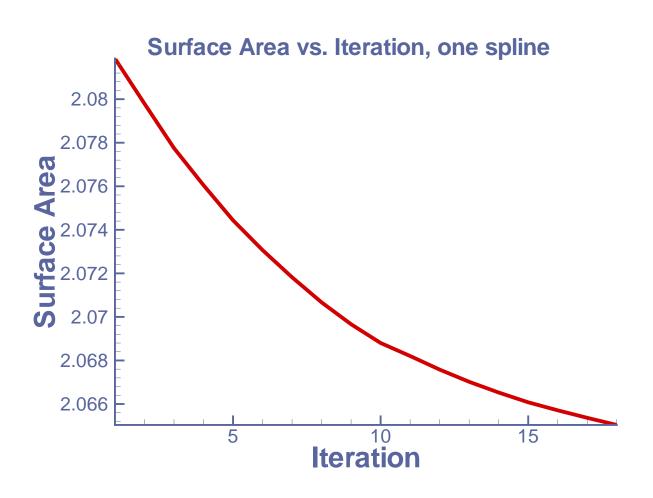






What is minimized?

- Incomplete assumption only accounts for geometry at each time step
- Method minimizes surface area?



Conclusions and Future Work

- No free lunch!
- Incomplete sensitivities assumption not valid for this case
- Choose new method
 - ☐ Adjoint
 - optimal control
 - suboptimal control
 - ☐ Evolutionary algorithm
 - Traditional method
 - Surface response method
 - ☐ Comparison of both?

Conclusions and Future Work

- **Extension to high** Re turbulent trailing edge flow
 - ☐ Cost function identification: define on surface
 - ☐ Total radiated power vs. frequency-weighted power
 - Low frequency noise propogates further
- Add constraints: lift, drag, thickness, volume, etc.